-
- Adopted configuration
• 4-wire LVDT with sensitivity ~ 105mV/V/I
• Differential analog gain x3.2 on the excit **Adopted configuration**
• 4-wire LVDT with sensitivity ~ 105mV/V/mm @ f_excitation = 5kHz, FS = ±5mm
• Differential analog gain x3.2 on the excitation (I verified that its noise is negligible)
• Excitation settings on PGA9 **Adopted configuration**
• 4-wire LVDT with sensitivity ~ 105mV/V/mm @ f_excitation = 5kHz, FS = ±5mm
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• Excitation settings on PGA Adopted configuration
• 4-wire LVDT with sensitivity ~ 105mV/V/mn
• Differential analog gain x3.2 on the excitati
• Excitation settings on PGA970:
• Amplitude = 300mV;
• Frequency = 5kHz **opted configuration**
-wire LVDT with sensitivity ~ 105mV/V/mm @ f_
Differential analog gain x3.2 on the excitation (I v
ixcitation settings on PGA970:
• Amplitude = 300mV;
• Frequency = 5kHz
• Waveform gain = 1.67 V/V
- -
	- Frequency = 5kHz
	-
- **opted configuration**
• wire LVDT with sensitivity ~ 105mV/V/mm @ f_excitation
Differential analog gain x3.2 on the excitation (I verified th
• xcitation settings on PGA970:
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• Differential analog gain x3.2 on the excitation (I verified th

• Excitation settings on PGA970:

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ixcitation settings on PGA970:

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he resulting amplitude on the primary inductor of

with oscillos • Amplitude = 300mV;
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he resulting amplitude on the primary induce
with oscilloscope)
9emodulator settings on PGA970:
• V_CM enabled = 1V
• ADC gain = 1V/V
• BPF at 5kHz with B • Waveform gain = 1.67 V/V

The resulting amplitude on the primary indue

with oscilloscope)

Demodulator settings on PGA970:

• V_CM enabled = 1V

• ADC gain = 1V/V

• BPF at 5kHz with BW = 500Hz

• LPF BW = 500Hz

• T_r
- -
	- ADC gain $= 1 \text{V/V}$
	-
	- LPF BW $=$ 500Hz
	-
	- DAC SIN $NDS1 = 0$
	-

Measurements

- Measurements
• Every 128us the PGA microcontroller enters an interrupt and saves demod 1 data (24-
bit amplitude, 32-bits sine and cosine). Those data are transferred serially to an
external uC using the COMBUF **easurements**
Every 128us the PGA microcontroller enters an interrupt and saves demod 1 data (24-
bit amplitude, 32-bits sine and cosine). Those data are transferred serially to an
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I read a com **easurements**
Every 128us the PGA microcontroller enters an int
bit amplitude, 32-bits sine and cosine). Those data
external uC using the COMBUF
I read a complete data set from the COMBUF ever
communication protocol betwee **Measurements**
• Every 128us the PGA microcontroller enters an interrupt and saves demod 1 data (2
bit amplitude, 32-bits sine and cosine). Those data are transferred serially to an
external uC using the COMBUF
• I read a **easurements**
Every 128us the PGA microcontroller enters an interrupt and saves demod 1 data (24-
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bit amplitude, 32-bits sine and cosine). Those data are transferred serially to an

external uC using the COMBUF

• I read a complete d **Example 12 For a long time interval to analyzing the data for an interval to an external uC using the COMBUF** enters an interrupt and saves demod 1 data (24-
bit amplitude, 32-bits sine and cosine). Those data are transfe
- Every 128us the PGA microcontroller enters an interrupt and saves demod 1 data (24-
bit amplitude, 32-bits sine and cosine). Those data are transferred serially to an
external uC using the COMBUF
• I read a complete data bit amplitude, 32-bits sine and cosine). Those data are transferred serially to an
external uC using the COMBUF
I read a complete data set from the COMBUF every 10ms (limited by the
communication protocol between uC and PC
-
-

Measured cosine (since DAC_SIN_NDS2 = WAVEFORM TABLE LEN the phase demodulator measures cos(phase))
Data coming from the phase demodulator are expressed in bins. The scale factor between bins and Volts is unknown
exerce

It is clear that the phase measurement is much more noisy than the amplitude measurement (the noise on sine and
cosine is two orders of magnitude higher than the amplitude noise).
It follows that if a calculate the amplit It is clear that the phase measurement is much more noisy than the amplitude measurement (the noise
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It follows that if a calculate the amplitude as $\sqrt{\sin$

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It is clear that the phase measurement is much more noisy than the amples cosine is two orders of magnitude higher than the amplitude noise).
It follows that if a calculate the amplitude as $\sqrt{\sin^2 + \cos^2}$ I get much hight It is clear that the phase measurement is much more noisy than the amplitude measurement (the noise on sine and
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It follows that if a calculate the amplitude as $\sqrt{\sin^2 + \cos^2}$ I get much higher noise compared with the amplitude noise
In addition, I can calculate if It follows that if a calculate the amplitude as $\sqrt{\sin^2 + \cos^2 1}$ get much higher noise compared with the amplitude noise
In addition, I can calculate if there is a scale factor between amplitude calculated by the amplitud In addition, I can calculate if there is a scale factor between amplitude calculated by the amplitude demodulator and
amplitude extracted starting from sine and cosine values.
This case the scale factor between amplitude In addition, I can calculate if there is a scale factor between amplitude calculated by the amplitude demodulator
amplitude extracted starting from sine and cosine values.
This case the scale factor between amplitude and As shown before the cosine is very noisy and in addition it has a small average value when the constrained in the cosine extracted starting from sine and cosine value.
This case the scale factor between amplitude and phas Ethis case the scale factor between amplitude and phase demodulator seems $\sqrt{1039.3^2 + 625.45^2}/1660.27 = 0.73$
This case the scale factor between amplitude and phase demodulator seems $\sqrt{1039.3^2 + 625.45^2}/1660.27 = 0.73$ rms case the scale ractor between ampintude and phase demodulard of orot understand why this value.
Am I doing some mistake in my considerations?
Starting from sine and cosine it is also possible to extract the phas
Since Starting from sine and cosine it is also possible to extract the phase as arctan(sin/cos)
Since sine and cosine are affected by a high percentage noise also the phase will be extremely noisy. Even worse, the
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Since sine and cosine are affected by a high percentage noise also the phase will be extremely noisy. Even worse, the
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Here you find a comparison b l also tried the same measurement at different positions of the LVDT and I noticed that the mean values of sine and
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extracted starting from the same digitalized inputs
Is there a smart way to extract phase
-
-
- Phase noise is a problem in my application when the LVDT approaches the center position. I do not understand why noise is so high, since both amplitude and phase are extracted starting from the same digitalized inputs
• Phase noise is a problem in my application when the LVD1 approaches the center
position. I do not understand why noise is so high, since both amplitude and phase are
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Is there a smart way to extract phase starting from the PGA970, which permits to
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Why does the scale factor seem to change at different LVDT pos