

SPICE Op Amp Macromodels for Stability Analysis “Trust But Verify”

Tim Green, MGTS

Precision Linear Analog Applications

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Overview

There are only 2 things you need in an op amp macromodel to analyze stability problems:

Z_o

(AC open loop output impedance)

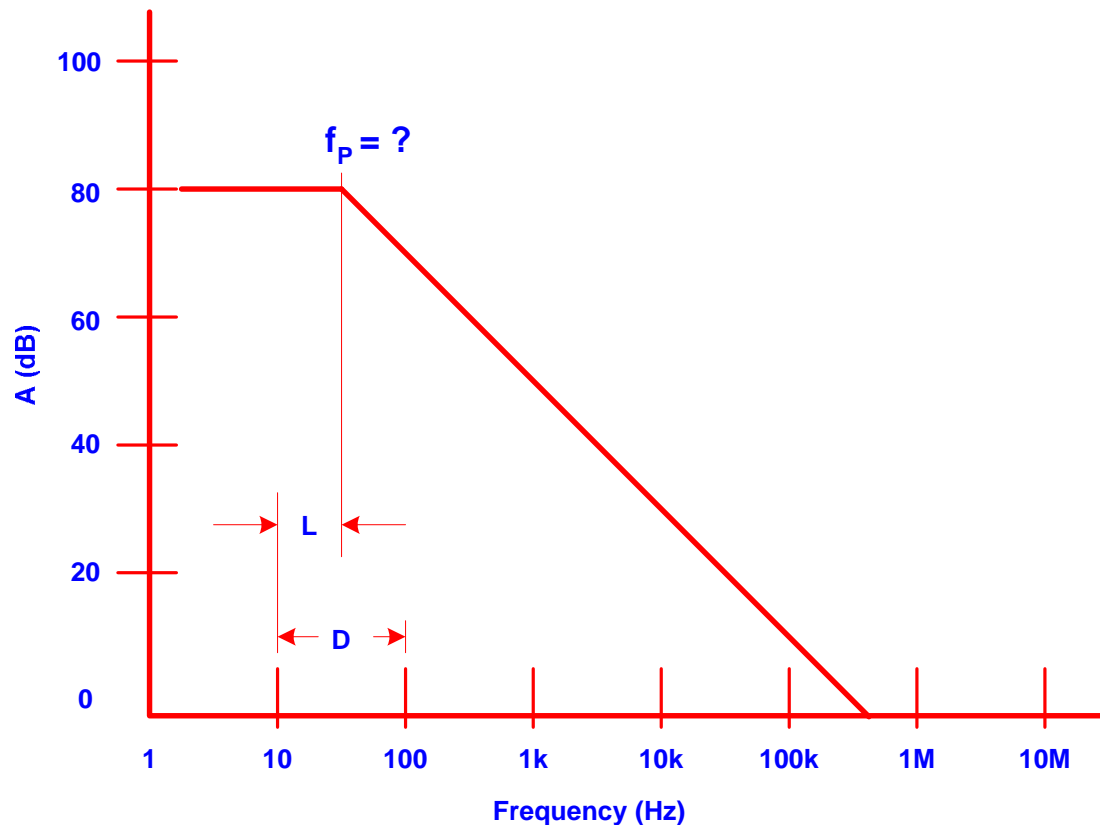
A_{ol}

(AC open loop gain)

Summary

- 1) Before any stability analysis is done check the SPICE op amp macromodel for proper Aol.
- 2) Before any stability analysis is done check the SPICE op amp macromodel for proper Zo (open loop output impedance).
- 2) Newer TI op amp datasheets give a Zo curve. Test in SPICE for Zo.
- 3) Older TI and competitor op amps usually have a Zout (closed loop output impedance curve). Test for Zout. If Zout is right Zo is right.
- 4) If op amp macromodel Zout or Zo does not match the datasheet build correct Aol and Zo from datasheet (use Aol and Zo or Zout curves. If Aol is correct you can just build an external Zo block

Log Scale Trick



Log Scale Trick ($f_p = ?$):

1) Given: $L = 1\text{cm}$; $D = 2\text{cm}$

2) $L/D = \text{Log}_{10}(f_p)$

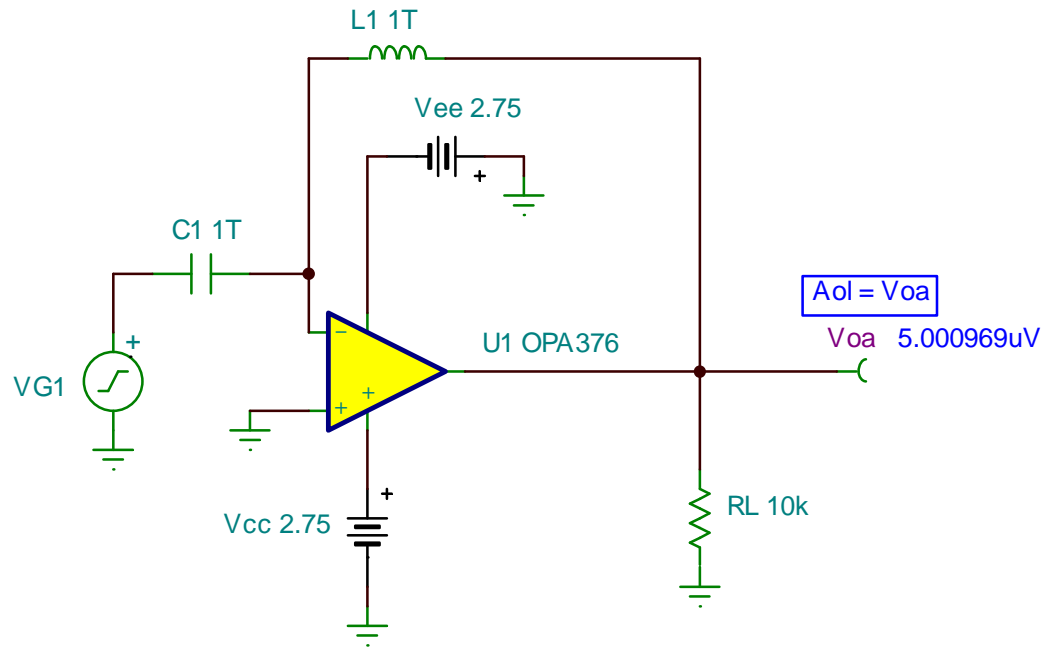
3) $f_p = \text{Log}_{10}^{-1}(L/D) = 10^{(L/D)}$
 $f_p = 10^{(L/D)} = 10^{(1\text{cm}/2\text{cm})} = 3.16$

4) Adjust for the decade range working within –
 10Hz-100Hz decade \hat{a}
 $f_p = 31.6\text{Hz}$

5) $L = \text{Log}_{10}(f_p') \times D$
 $L = \text{Log}_{10}(3.16) \times 2\text{cm} = 1\text{cm}$
 where $f_p' = f_p$ normalized to the
 1-10 decade range –
 $f_p = 31.6 \hat{a} f_p' = 3.16$

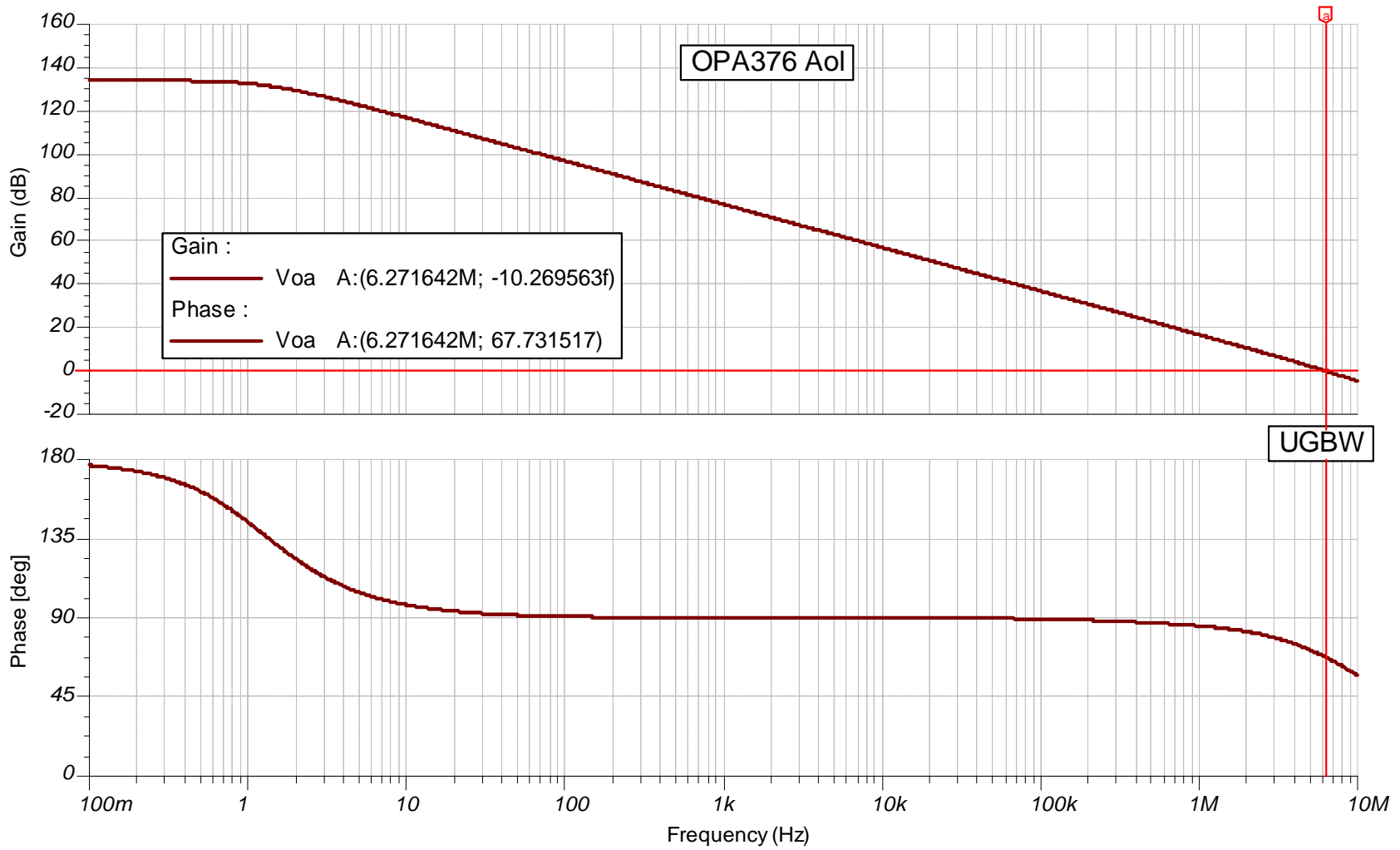
Analysis

Aol Test

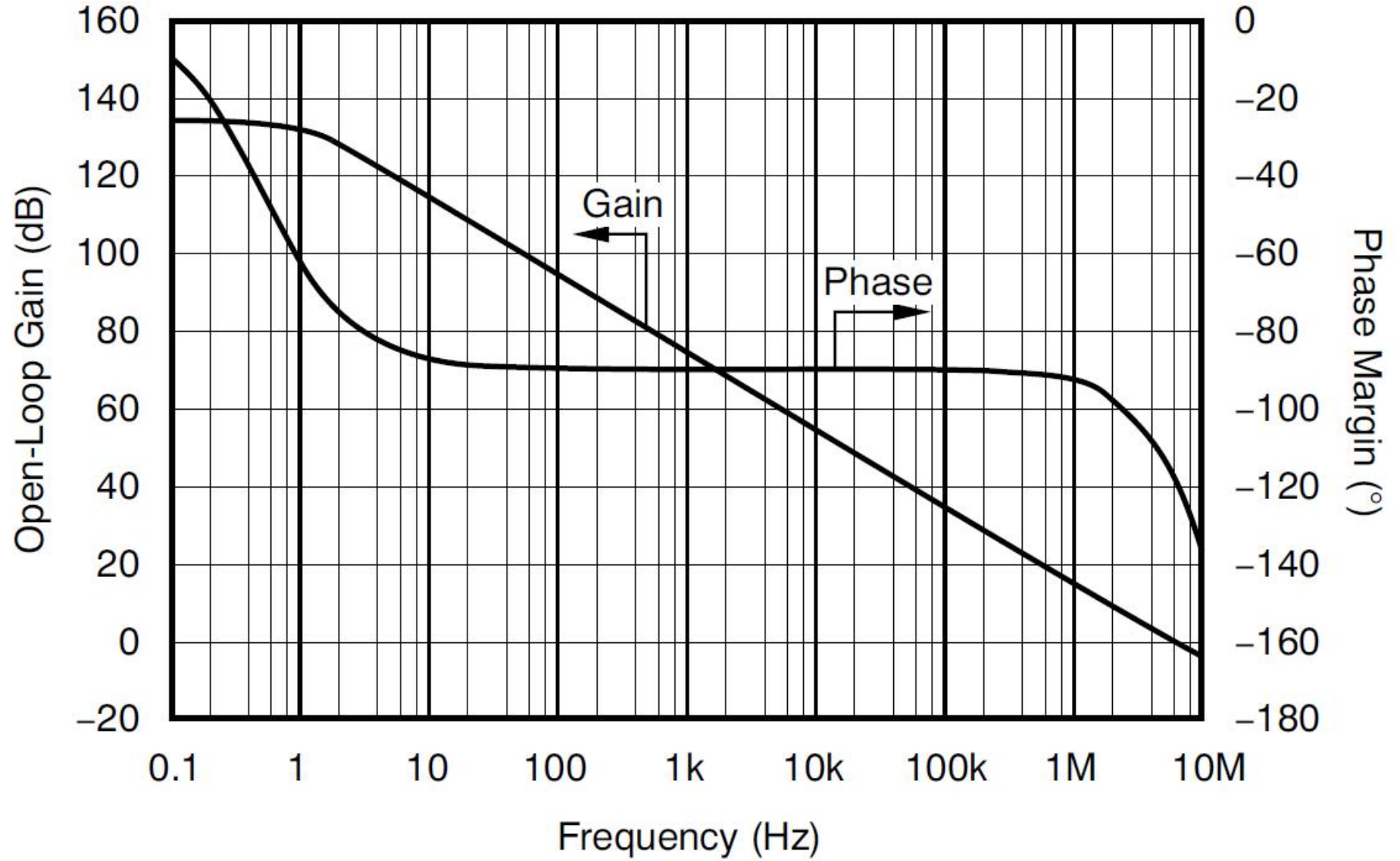


Note:
Check DC Operating Point first.
Op Amp must be in DC Linear region for AC Analysis to be valid.

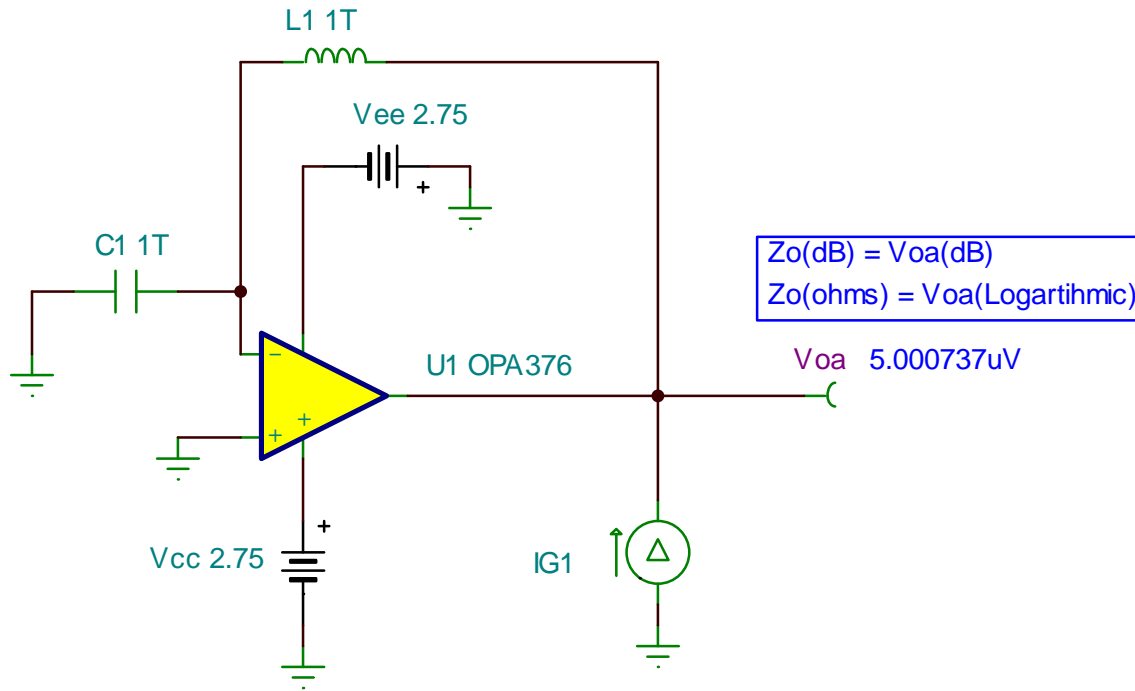
Aol Test



Aol Test



Zo Test

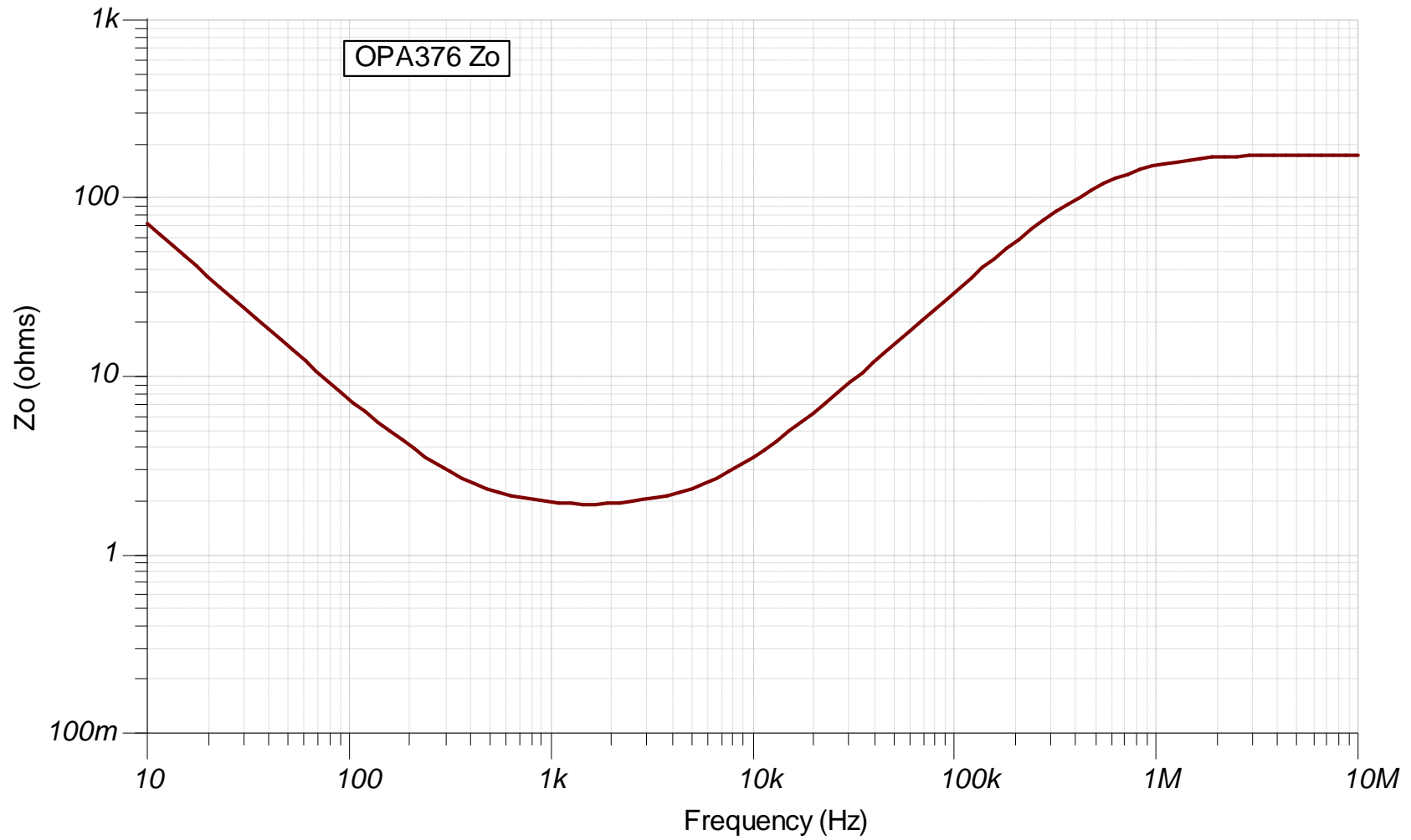


Note:
Check DC Operating Point first.
Op Amp must be in DC Linear region for AC Analysis to be valid.



OPA376 Zo.TSC

Zo Test



Zo Test

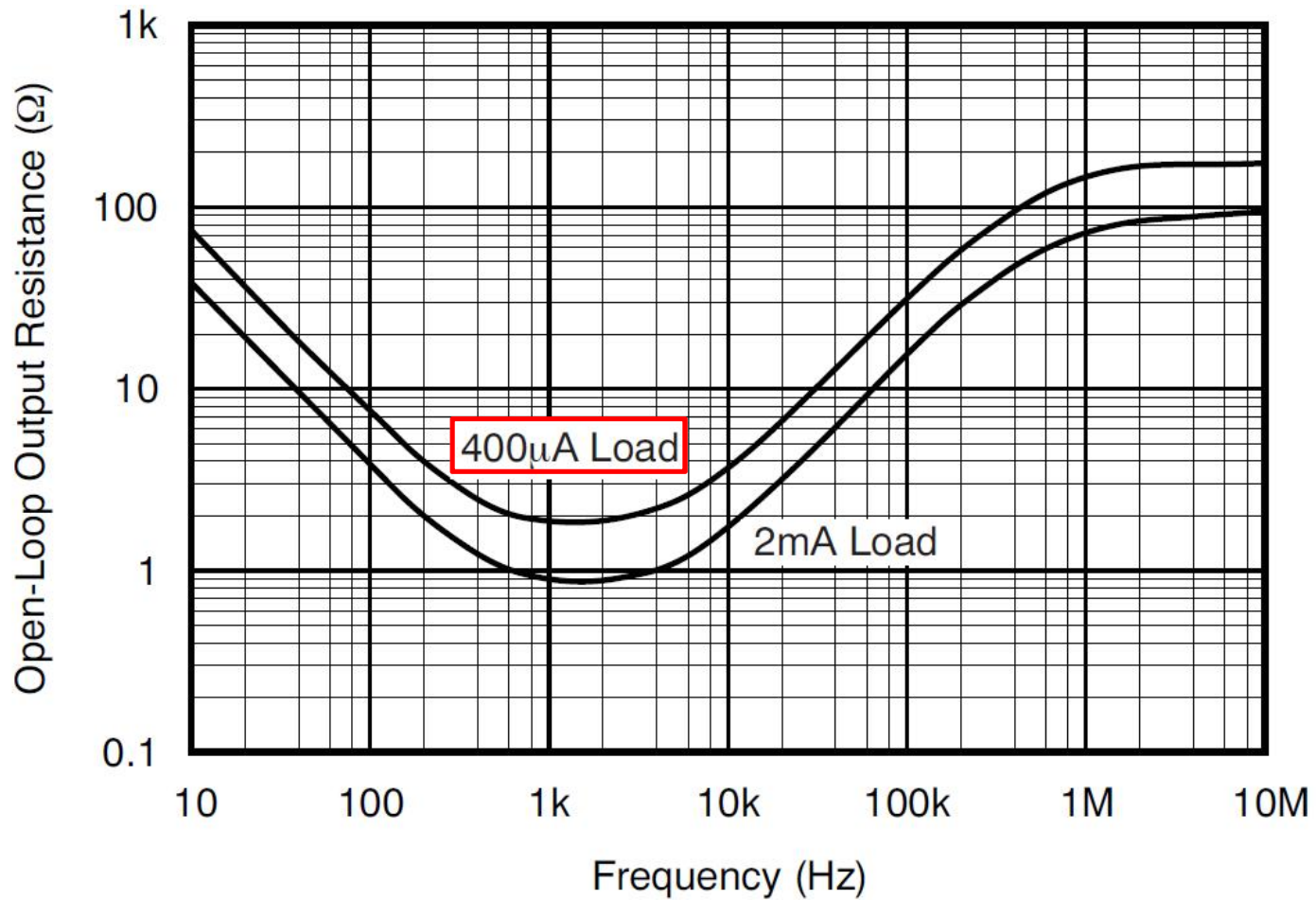
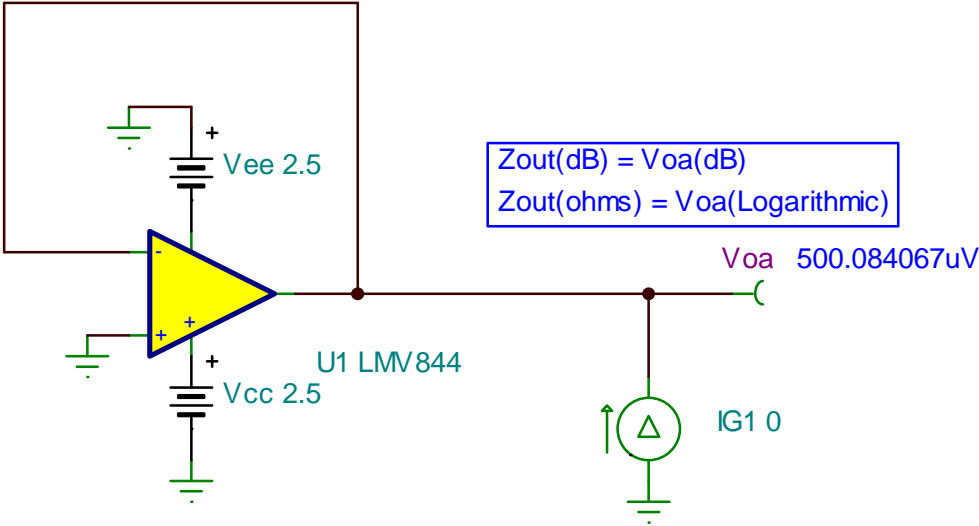


Figure 21. Open-Loop Output Resistance vs Frequency

Zout Test



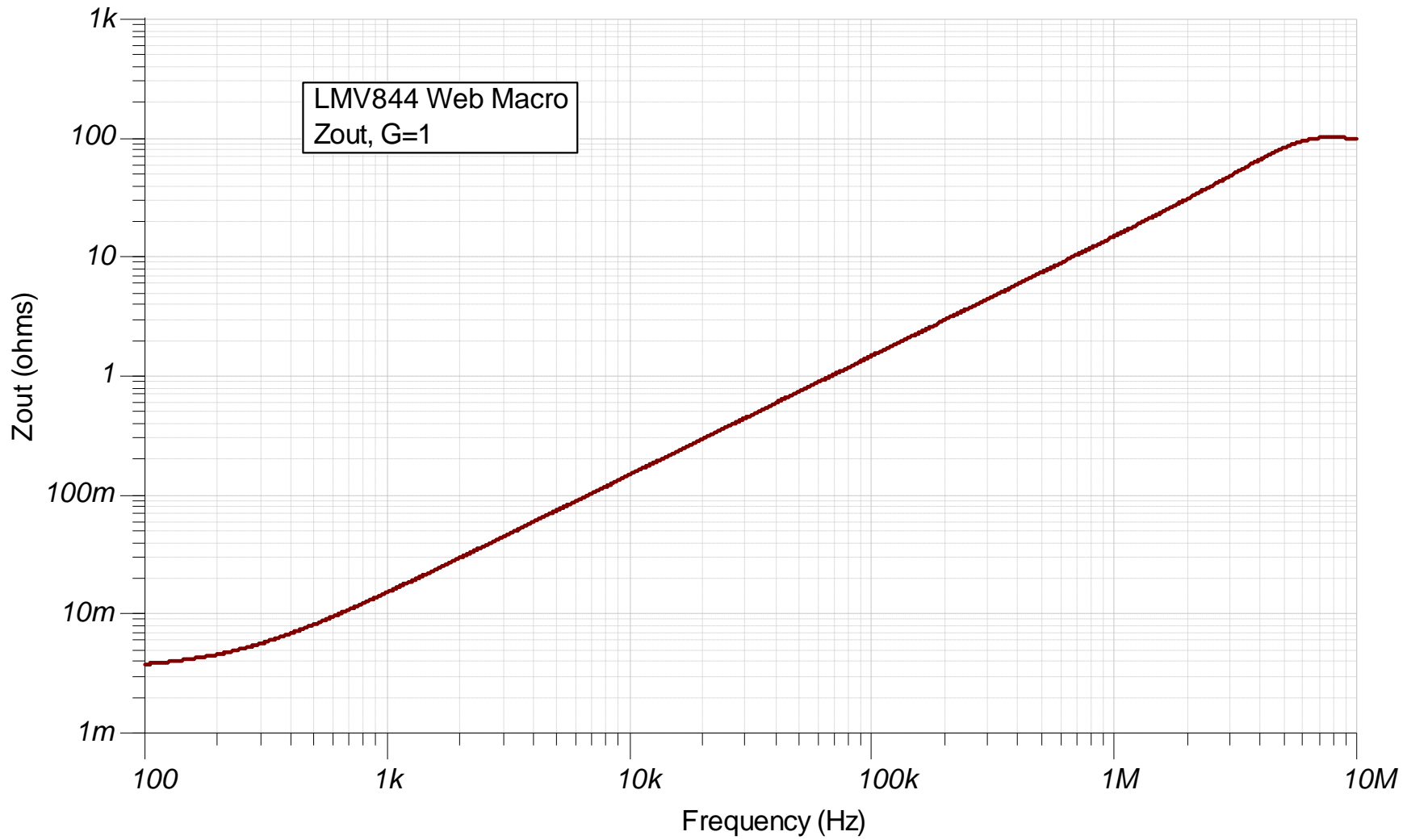
Note:
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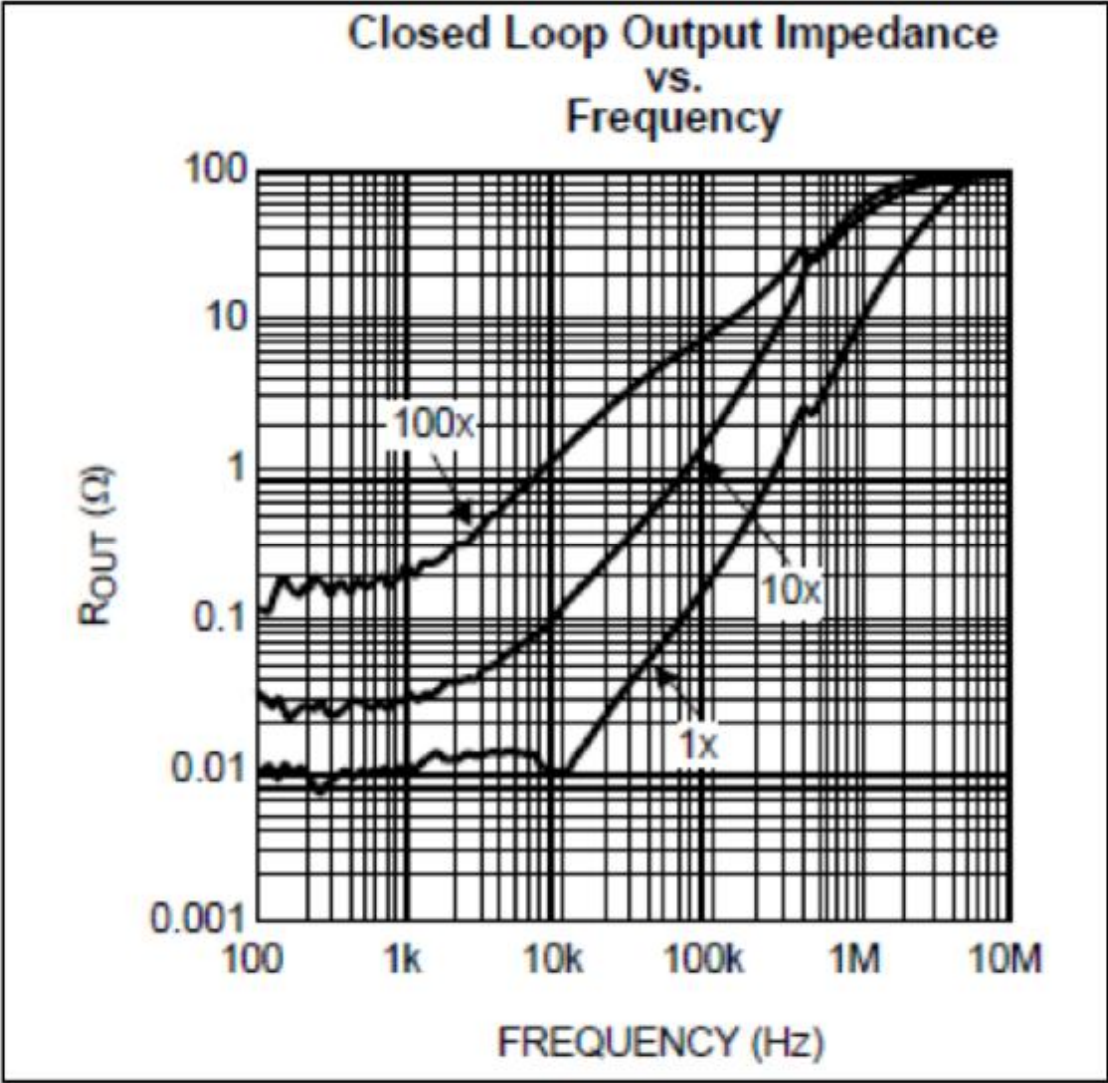
LMV844 Zout.TSC

Zout Test

Note Zout macromodel does NO MATCH datasheet - Contact Vendor to fix!!



Zout Test



Op Amp Output Impedance

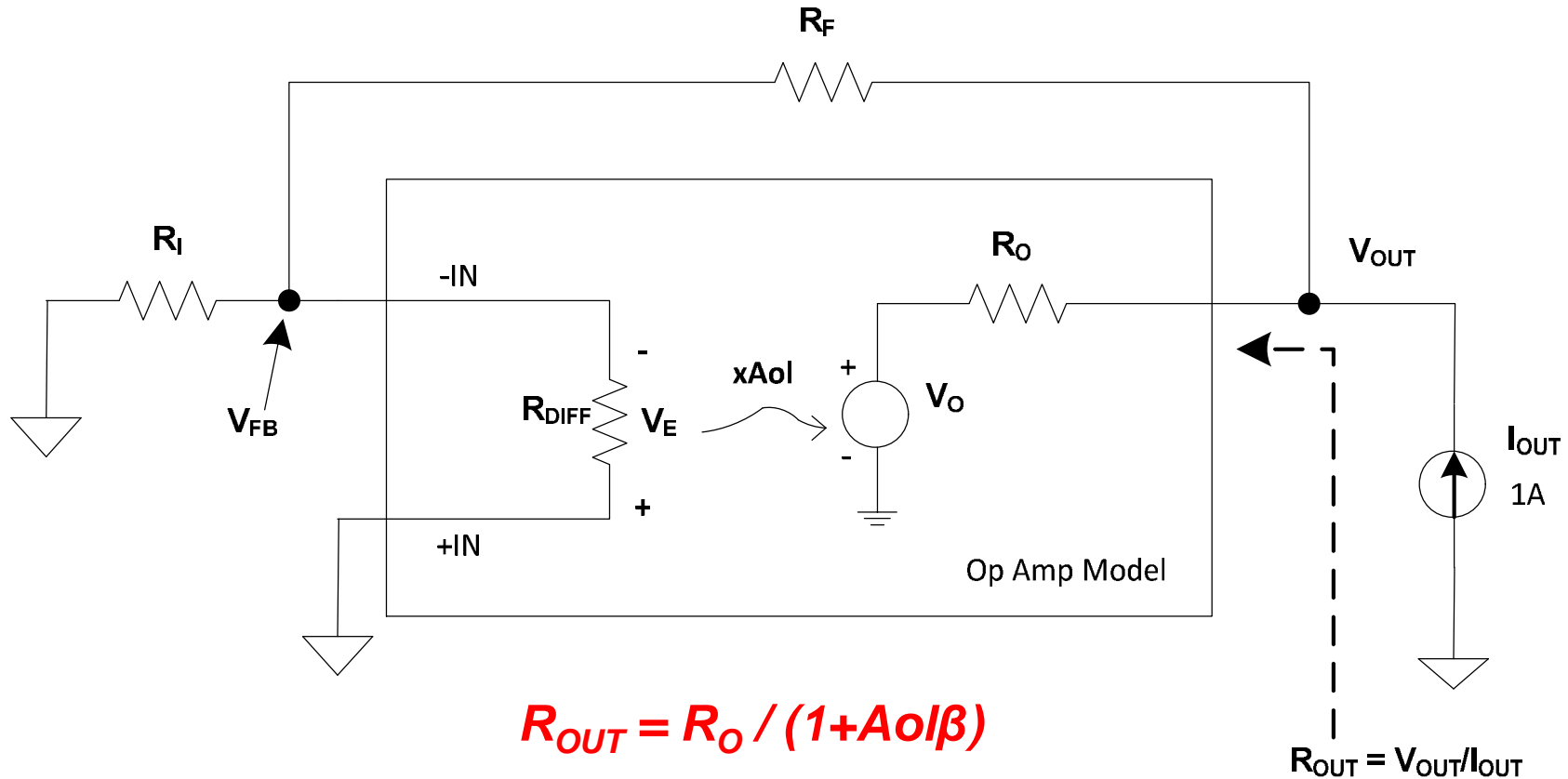
Open Loop (Z_o)
&
Closed Loop (Z_{OUT})

Op Amps and “Output Resistance”

Definition of Terms:

R_O = Op Amp **Open Loop** Output Resistance

R_{OUT} = Op Amp **Closed Loop** Output Resistance



Derivation of R_{OUT} (Closed Loop Output Resistance)

1) $\beta = V_{FB} / V_{OUT} = [V_{OUT} (R_I / \{R_F + R_I\})] / V_{OUT} = R_I / (R_F + R_I)$

2) $R_{OUT} = V_{OUT} / I_{OUT}$

3) $V_O = -V_E A_{ol}$

4) $V_E = V_{OUT} [R_I / (R_F + R_I)]$

5) $V_{OUT} = V_O + I_{OUT} R_O$

6) $V_{OUT} = -V_E A_{ol} + I_{OUT} R_O$ *Substitute 3) into 5) for V_O*

7) $V_{OUT} = -V_{OUT} [R_I / (R_F + R_I)] A_{ol} + I_{OUT} R_O$ *Substitute 4) into 6) for V_E*

8) $V_{OUT} + V_{OUT} [R_I / (R_F + R_I)] A_{ol} = I_{OUT} R_O$ *Rearrange 7) to get V_{OUT} terms on left*

9) $V_{OUT} = I_{OUT} R_O / \{1 + [R_I A_{ol} / (R_F + R_I)]\}$ *Divide in 8) to get V_{OUT} on left*

10) $R_{OUT} = V_{OUT} / I_{OUT} = [I_{OUT} R_O / \{1 + [R_I A_{ol} / (R_F + R_I)]\}] / I_{OUT}$

Divide both sides of 9) by I_{OUT} to get R_{OUT} [from 2)] on left

11) $R_{OUT} = R_O / (1 + A_{ol} \beta)$ *Substitute 1) into 10)*

$\longrightarrow R_{OUT} = R_O / (1 + A_{ol} \beta) \longleftarrow$

R_{OUT} vs R_O

$\emptyset R_O$ does *NOT* change when Closed Loop feedback is used

$\emptyset R_{OUT}$ is the effect of R_O , A_{ol} , and β controlling V_O

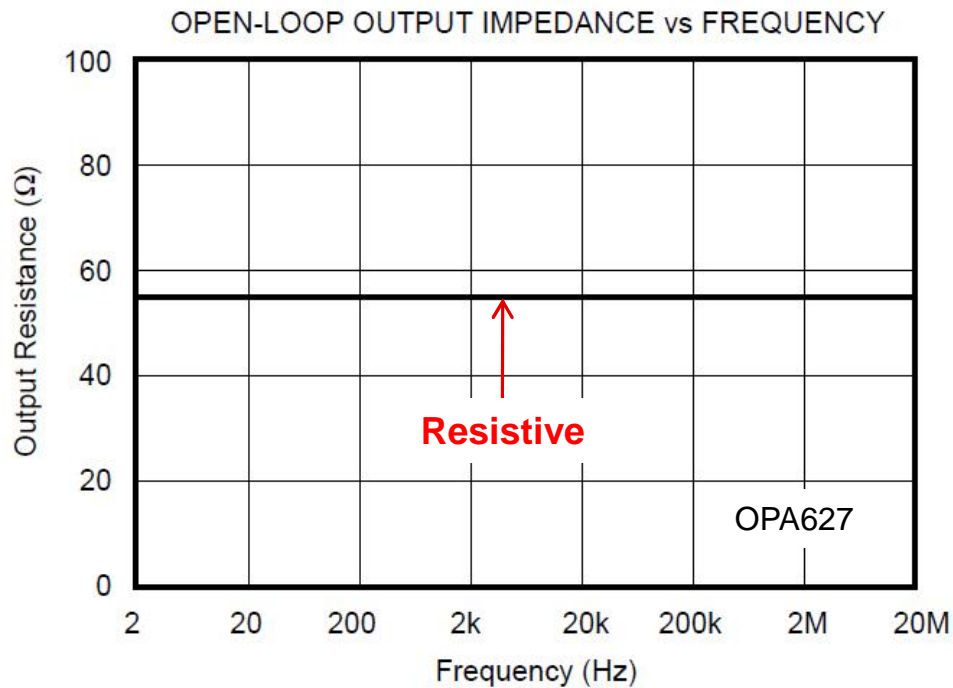
ü Closed Loop feedback (β) forces V_O to increase or decrease as needed to accommodate V_O loading

ü Closed Loop (β) increase or decrease in V_O appears at V_{OUT} as a reduction in R_O

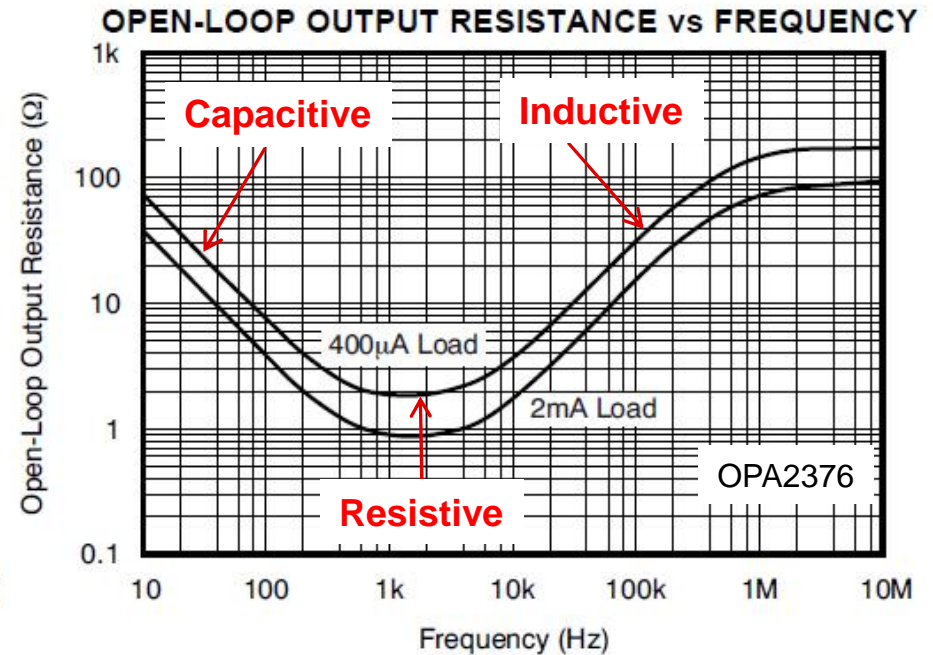
ü R_{OUT} increases as Loop Gain ($A_{ol}\beta$) decreases

When R_o is really Z_o !!

OPA627 has R_o

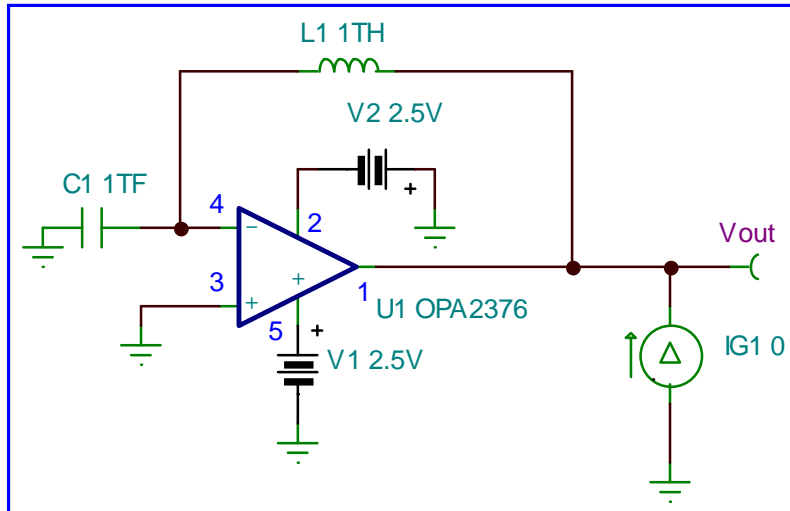


OPA2376 has Z_o

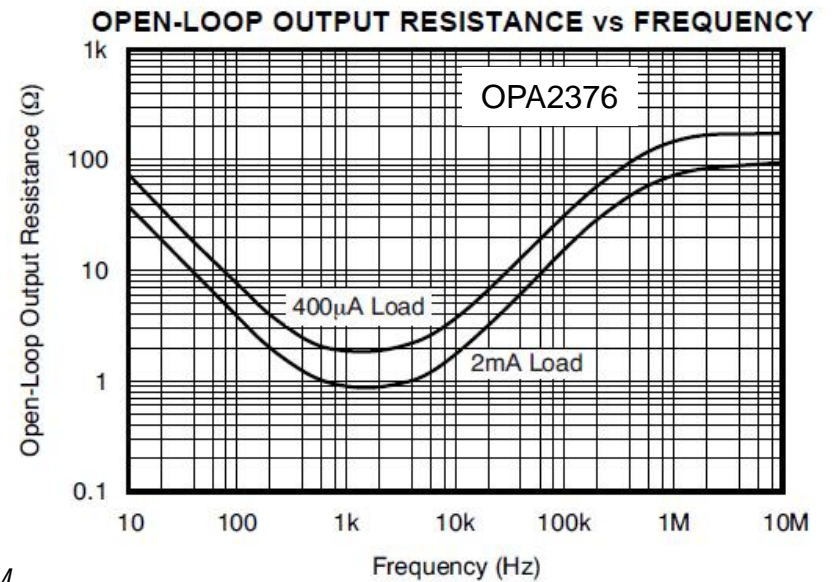
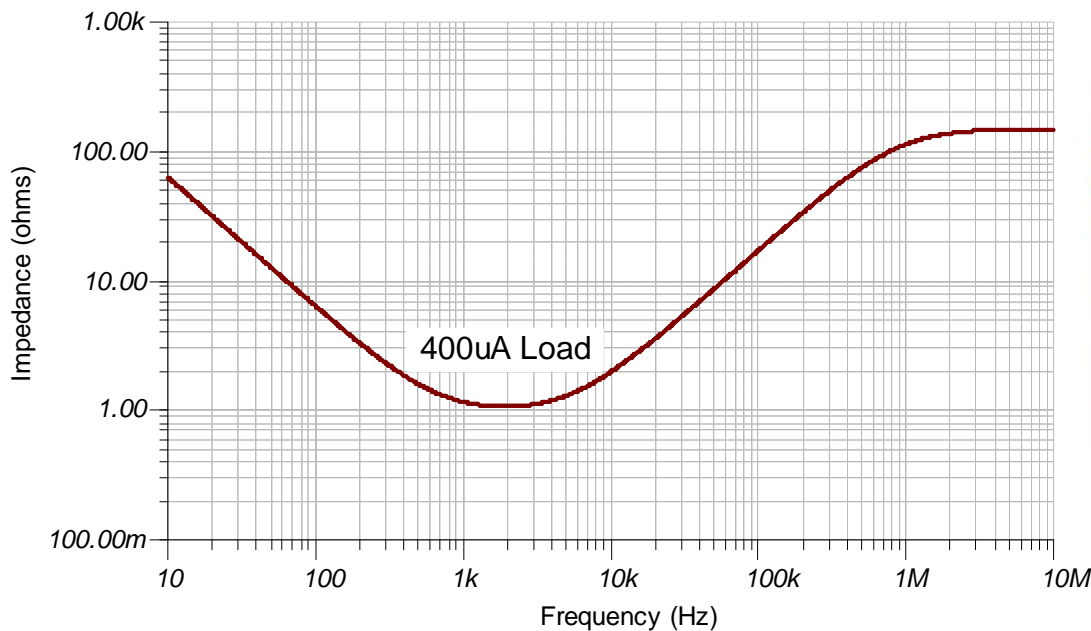


Note: Some op amps have Z_o characteristics other than pure resistance – consult data sheet / manufacturer

With Complex Z_o , Accurate Models are Key!



SPICE Test of Op Amp Macro Z_o :
 Run SPICE AC Analysis
 IG1 is AC Current Generator
 IG1DC Value = 0A for unloaded Z_o
 $Z_o = V_{out}$
 Convert V_{out} (dB) to V_{out} (Logarithmic)
 Z_{out} (ohms) = V_{out} (Logarithmic)



Some Data Sheets Specify Z_{OUT} **NOT** Z_o

R_{OUT} is Inverse of A_{ol} :

$$R_{OUT} = \frac{R_o}{1 + A_{ol}\beta}$$

$$R_{OUT} \propto \frac{1}{A_{ol}}$$

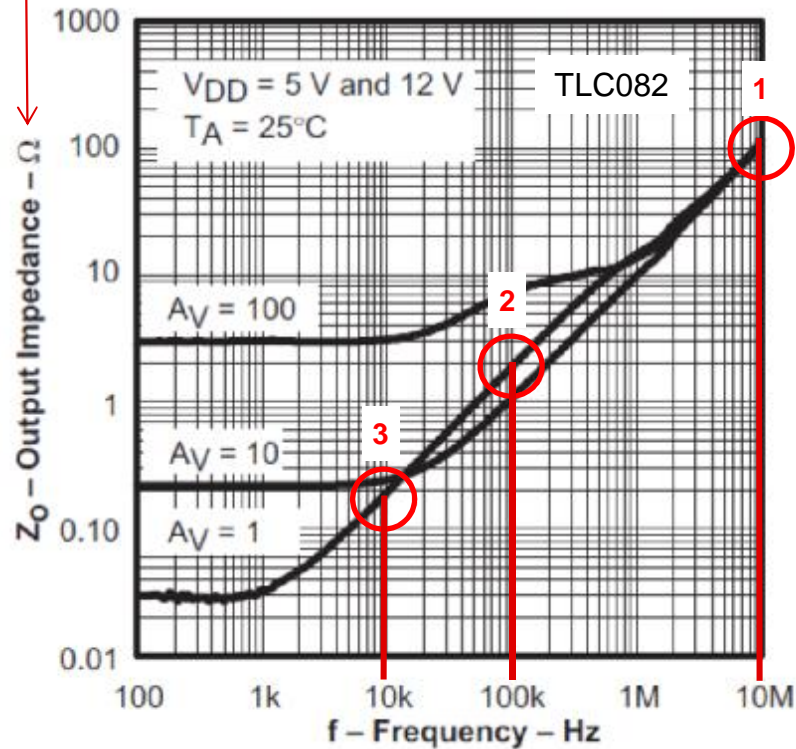
Recognize R_{OUT} instead of R_o :

R_{OUT} inversely proportional to A_{ol}

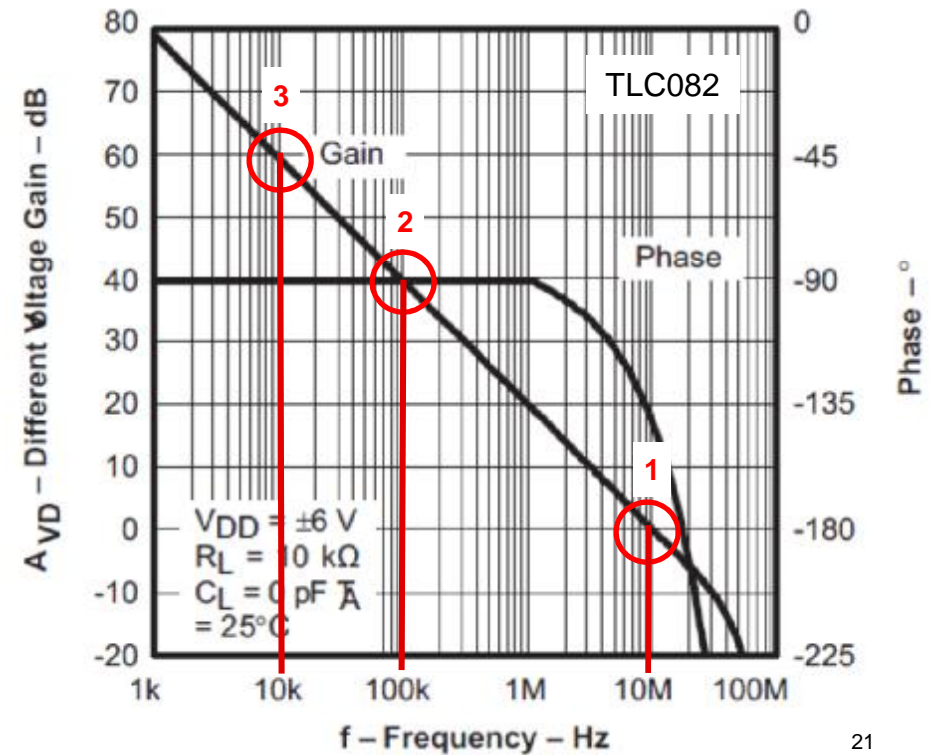
R_{OUT} typically $< 100\Omega$ at high frequency

This is really Z_{OUT} or R_{OUT} !

OUTPUT IMPEDANCE
VS
FREQUENCY



DIFFERENTIAL VOLTAGE GAIN AND
PHASE
VS
FREQUENCY



Some Data Sheets Specify Z_{OUT} *NOT* Z_O

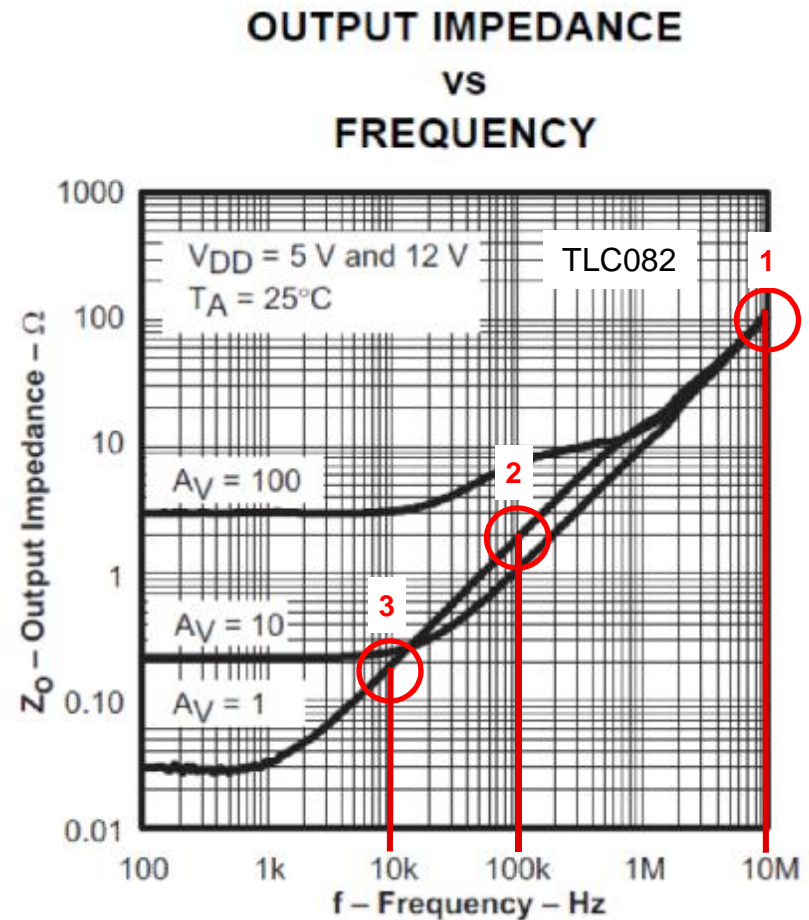
Point	frequency	Aol	$R_{OUT}(A_V=1)$ Datasheet	$R_{OUT}(A_V=1)$ Computed
-----	(Hz)	(dB)	(ohms)	(ohms)
1	10M	0	100	$R_O = 200$
2	100k	40	2	2
3	10k	60	0.2	0.2

Compute R_O from R_{OUT} where $Aol\beta = 1$ (0dB):

$R_{OUT} = 100\Omega$ for $A_V = 1$, $f = 10\text{MHz}$, $Aol\beta = 1$ (0dB)

$$R_{OUT} = \frac{R_O}{1 + Aol\beta}$$

$$100\Omega = \frac{R_O}{1+1} \rightarrow R_O = 200\Omega$$



Appendix: Op Amp Stability Reference

For detailed, definition-by-example of 10 different ways to stabilize op amps driving capacitive loads, and additional technical information on solving op amp stability problems, visit the Texas Instruments E2E Forum at:

http://e2e.ti.com/support/amplifiers/precision_amplifiers/w/design_notes/2645.solving-op-amp-stability-issues.aspx

Download Part 1, Part 2, Part 3, and Part 4.

For more in-depth learning about op amps and op amp stability look at TI Precision Labs at:
www.ti.com/precisionlabs

Analog Engineer's Pocket Reference

A “must-have” for every Board/System Design Engineer

Download: <http://www.ti.com/lstds/ti/amplifiers-linear/precision-amplifier-support-community.page#pocketref>

Buy Hardcopy: <https://store.ti.com/Search.aspx?k=pocket+reference&pt=-1>

All Embedded Schematics in this presentation can be run in the Free TINA_TI SPICE simulator available at:

<http://www.ti.com/tool/tina-ti>