

# Temperature sensing with NTC circuit

## **Design Goals**

Temperature		Output Voltage		Supply		
T <sub>Min</sub>	T <sub>Max</sub>	V <sub>outMin</sub>	V <sub>outMax</sub>	$V_{dd}$	V <sub>ee</sub>	V <sub>ref</sub>
25 °C	50 °C	0.05V	3.25V	3.3V	0V	1.659V

#### **Design Description**

This temperature sensing circuit uses a resistor in series with a negative-temperature-coefficient (NTC) thermistor to form a voltage divider, which has the effect of producing an output voltage that is linear over temperature. The circuit uses an op amp in a non-inverting configuration with inverting reference to offset and gain the signal, which helps to utilize the full ADC resolution and increase measurement accuracy.



### **Design Notes**

- 1. Use the op amp in a linear operating region. Linear output swing is usually specified under the A<sub>OL</sub> test conditions.
- 2. The connection, Vin, is a positive temperature coefficient output voltage. To correct an NTC output voltage, switch the position of R<sub>1</sub> and the NTC thermistor.
- 3.  $R_1$  is chosen based on the temperature range and the NTC's value.
- 4. V<sub>ref</sub> can be created using a DAC or voltage divider. If a voltage divider is used the equivalent resistance of the voltage divider will influence the gain of the circuit.
- 5. Using high value resistors can degrade the phase margin of the amplifier and introduce additional noise in the circuit. It is recommended to use resistor values around 10 k $\Omega$  or less.
- 6. A capacitor placed in parallel with the feedback resistor will limit bandwidth, improve stability and help reduce noise.

TEXAS INSTRUMENTS

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## **Design Steps**

 $V_{out} = V_{dd} \star \frac{R_1}{R_{\text{NTC}} + R_1} \star \frac{R_2 + R_3}{R_2} - \frac{R_3}{R_2} \star V_{\text{ref}}$ 

1. Calculate the value of R<sub>1</sub> to produce a linear output voltage. Use the minimum and maximum values of the PTC to obtain a range of values for R<sub>1</sub>.

 $\mathsf{R}_{\mathsf{NTC\_max}} = \mathsf{R}_{\mathsf{NTC}\ @\ 25^\circ C} = 2.252 \ \mathsf{k}\Omega, \quad \mathsf{R}_{\mathsf{NTC\_min}} = \mathsf{R}_{\mathsf{NTC}\ @\ 50^\circ C} = 819.7 \ \Omega$ 

 $R_{1} = \sqrt{R_{\text{NTC } @25^{\circ}\text{C}} \times R_{\text{NTC } @50^{\circ}\text{C}}} = \sqrt{2.252 \text{ k}\Omega \times 819.7 \ \Omega} = 1.359 \text{ k}\Omega \approx 1.37 \text{ k}\Omega$ 

2. Calculate the input voltage range.

$$V_{inMin} = V_{dd} \times \frac{R_1}{R_{NTC_max} + R_1} = 3.3 \text{ V} \times \frac{1.37 \text{ }k\Omega}{2.252 \text{ }k\Omega + 1.37 \text{ }k\Omega} = 1.248 \text{ V}$$
$$V_{inMax} = V_{dd} \times \frac{R_1}{R_{NTC_min} + R_1} = 3.3 \text{ V} \times \frac{1.37 \text{ }k\Omega}{819.7 \Omega + 1.37 \text{ }k\Omega} = 2.065 \text{ V}$$

3. Calculate the gain required to produce the maximum output swing.

$$G_{ideal} = \frac{V_{outMax} - V_{outMin}}{V_{inMax} - V_{inMin}} = \frac{3.25 \, V - 0.05 \, V}{2.065 \, V - 1.248 \, V} = 3.917 \, \frac{V}{V}$$

4. Select  $R_2$  and calculate  $R_3$  to set the gain in Step 3.

$$\begin{split} & \text{Gain} = \frac{R_2 + R_3}{R_2} \\ & \text{R}_2 = 1 \text{ } k\Omega \quad (\text{Standard value}) \\ & \text{R}_3 = \text{R}_2 \times (\text{G}_{\text{ideal}} - 1) = 1 \text{ } k\Omega \times (3.917 \frac{\text{V}}{\text{V}} - 1) = 2.917 \text{ } k\Omega \end{split}$$

Choose  $R_3 = 2.87 \text{ k}\Omega$  (Standard value)

5. Calculate the actual gain based on standard values of  $\mathsf{R}_2$  and  $\mathsf{R}_3.$ 

$$G_{\text{actual}} = \frac{R_2 + R_3}{R_2} = \frac{1 \text{ k}\Omega + 2.87 \text{ k}\Omega}{1 \text{ k}\Omega} = 3.87 \frac{\text{V}}{\text{V}}$$

6. Calculate the output voltage swing based on the actual gain.

 $V_{out\_swing} = (V_{inMax} - V_{inMin}) \times G_{actual} = (2.065 \text{ V} - 1.248 \text{ V}) \times 3.87 \frac{\text{V}}{\text{V}} = 3.162 \text{ V}$ 

7. Calculate the maximum output voltage when the output voltage is symmetrical around mid-supply.

$$V_{outMax} = V_{mid-supply} + \frac{V_{out\_swing}}{2} = \frac{V_{dd} - V_{ee}}{2} + \frac{V_{out\_swing}}{2} = \frac{3.3 \, V - 0 \, V}{2} + \frac{3.162 \, V}{2} = 3.231 \, V$$

8. Calculate the reference voltage.

$$\begin{split} V_{\text{outMax}} &= V_{\text{inMax}} \star G_{\text{actual}} - \frac{R_3}{R_2} \star V_{\text{ref}} \\ 3.231 \text{ V} &= 2.065 \text{ V} \star 3.87 \frac{\text{V}}{\text{V}} - \frac{2.87 \text{ k}\Omega}{1 \text{ k}\Omega} \star V_{\text{ref}} \\ V_{\text{ref}} &= \frac{2.065 \text{ V} \star 3.87 \frac{\text{V}}{\text{V}} - 3.231 \text{ V}}{\frac{2.87 \text{ k}\Omega}{1 \text{ k}\Omega}} = 1.659 \text{ V} \end{split}$$

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**Design Simulations** 

**DC Transfer Results** 



AC Simulation Results



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# **References:**

- 1. Analog Engineer's Circuit Cookbooks
- 2. SPICE Simulation File SBOMAV6
- 3. TI Precision Labs

# Design Featured Op Amp:

TLV9002				
V <sub>cc</sub>	1.8 V to 5.5 V			
V <sub>inCM</sub>	Rail-to-rail			
V <sub>out</sub>	Rail-to-rail			
V <sub>os</sub>	1.5mV			
l <sub>q</sub>	0.06mA			
I <sub>b</sub>	5рА			
UGBW	1MHz			
SR	2V/µs			
#Channels	1, 2, 4			
http://www.ti.com/product/TLV9002				

# Design Alternate Op Amp:

OPA333				
V <sub>cc</sub>	1.8 V to 5.5 V			
V <sub>inCM</sub>	Rail-to-rail			
V <sub>out</sub>	Rail–to–rail			
V <sub>os</sub>	2μV			
l <sub>q</sub>	17μΑ			
I <sub>b</sub>	70pA			
UGBW	350kHz			
SR	0.16V/µs			
#Channels	1, 2, 4			
http://www.ti.com/product/OPA333				

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