







**[OPA561](https://www.ti.com/product/OPA561)**

[SBOS206F](https://www.ti.com/lit/pdf/SBOS206) – JANUARY 2001 – REVISED OCTOBER 2023

# **OPA561 High-Current, High-Speed Operational Amplifier**

## **1 Features**

<span id="page-0-0"></span>Texas

- 1.2‑A output current
- $12-V_{PP}$  output voltage

**INSTRUMENTS** 

- Wide power range
	- Single supply: 7 V to 15 V
	- Dual supply:  $\pm 3.5$  V to  $\pm 7.5$  V
- Fully protected
	- Thermal shutdown
	- Adjustable current limit
- Output disable control
- 17-MHz gain-bandwidth product
- 50-V/µs slew rate
- 1‑MHz full-power bandwidth
- Thermally enhanced HTSSOP-20 PowerPAD™ integrated circuit package
- Temperature range: 0°C to 125°C

# **2 Applications**

- Power-line communications
- Valve-actuator drivers
- Power supplies
- Test equipment
- Tec drivers
- Laser diode drivers

## **3 Description**

The OPA561 is a low-cost, high-current operational amplifier capable of driving up to 1.2-A pulses into reactive loads. This monolithic integrated circuit provides high reliability in demanding line-carrier communications, laser diode drivers, and motorcontrol applications. The high slew rate provides 1 MHz of full-power bandwidth and excellent linearity.

For design flexibility, the OPA561 operates from either a single supply in the range of 7 V to 15 V or dual power supplies of  $\pm 3.5$  V to  $\pm 7.5$  V. In single-supply operation, the input common-mode range extends below ground. At maximum output current, a wide output swing provides a 12  $V_{PP}$  capability with a nominal 15‑V supply.

The OPA561 is internally protected against overtemperature conditions and current overloads. In addition, the OPA561 is designed to provide an accurate, user-selected, current limit. The current limit can be adjusted from 0.2 A to 1.2 A with a lowpower resistor or potentiometer, or DAC (digital-toanalog converter). The high-speed characteristics of the current control loop provide accuracy, even under pulsed-load conditions.

The enable and status (E/S) pin performs two functions: the pin can be monitored to determine if the device is in thermal shutdown (active low), and can also be forced low to disable the output, thus disconnecting the load.

The OPA561 is available in a miniature HTSSOP-20 PowerPAD integrated circuit package. This surfacemount package is thermally enhanced and has a very low thermal resistance. Operation is specified over the industrial temperature range of 0°C to 125°C.

**Package Information**



(1) For more information, see [Section 10.](#page-21-0)

(2) The package size (length × width) is a nominal value and includes pins, where applicable.



**Pinout Diagram**





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## **4 Pin Configuration and Functions**



**Figure 4-1. PWP Package, 20-Pin HTSSOP (Top View)**

#### **Table 4-1. Pin Functions**



(1)  $I = input$ ,  $O = output$ ,  $G = ground$ ,  $P = power$ .

## <span id="page-3-0"></span>**5 Specifications**

## **5.1 Absolute Maximum Ratings**

over operating free-air temperature range (unless otherwise noted)<sup>(1)</sup>



(1) Operation outside the *Absolute Maximum Ratings* may cause permanent device damage. *Absolute Maximum Ratings* do not imply functional operation of the device at these or any other conditions beyond those listed under *Recommended Operating Conditions*. If used outside the *Recommended Operating Conditions* but within the *Absolute Maximum Ratings*, the device may not be fully functional, and this may affect device reliability, functionality, performance, and shorten the device lifetime.

#### **5.2 ESD Ratings**



(1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.

(2) JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.

## **5.3 Recommended Operating Conditions**

over operating free-air temperature range (unless otherwise noted)



#### **5.4 Thermal Information**



(1) For more information about traditional and new thermal metrics, see the *[Semiconductor and IC package thermal metrics](https://www.ti.com/lit/pdf/SPRA953)* application report.

## <span id="page-4-0"></span>**5.5 Electrical Characteristics**

at  $T_{\text{CASE}} = 25^{\circ}$ C, V<sub>S</sub> = 15 V, load connected to V/2, and E/S enabled (unless otherwise noted)

	<b>PARAMETER</b>	<b>TEST CONDITIONS</b>	<b>MIN</b>	<b>TYP</b>	<b>MAX</b>	<b>UNIT</b>	
	OFFSET VOLTAGE, V <sub>S</sub> = 12 V						
$V_{OS}$	Input offset voltage	$V_{CM} = 0 V$		$-3$	±20	mV	
$dV_{OS}/dT$	Input offset voltage vs temperature	$T_A = 0$ °C to 125°C		±50		µV/°C	
<b>PSRR</b>	Input Offset Voltage vs Power Supply	$V_{CM}$ = 0 V, V <sub>S</sub> = 7 V to 16 V		25	150	µV/V	
	<b>INPUT BIAS CURRENT(1)</b>						
l <sub>B</sub>	Input bias current	$V_{CM} = 0 V$		10	100	pA	
$I_{OS}$	Input offset current	$V_{CM} = 0 V$		10	100	pA	
<b>NOISE</b>							
$e_{n}$	Input voltage noise density	$f = 1$ kHz		83		$nV/\sqrt{Hz}$	
		$f = 10$ kHz		32			
		$f = 100$ kHz		14			
$I_{n}$	Current noise	$f = 1$ kHz		4		$fA/\sqrt{Hz}$	
	<b>INPUT VOLTAGE RANGE</b>						
$V_{CM}$	Common-mode voltage	Linear operation	$(V-) - 0.1$		$(V+) - 3$	$\vee$	
<b>CMRR</b>	Common-mode rejection ratio	$V_S$ = 15 V, V <sub>CM</sub> = (V-) - 0.1 V to (V+) – 3 V	70	80		dB	
<b>INPUT IMPEDANCE</b>							
	<b>Differential</b>			$1.8 \times 10^{11}$    10		$\Omega \parallel pF$	
	Common-mode			$1.8 \times 10^{11}$    18.5		$\Omega \parallel pF$	
<b>OPEN-LOOP GAIN</b>							
$A_{OL}$	Open-loop voltage Gain	$V_{O}$ = 10 $V_{PP}$ , R <sub>L</sub> = 5 Ω	80	100		dВ	
	<b>FREQUENCY RESPONSE</b>						
<b>GBW</b>	Gain-bandwidth product	$R_L = 5 \Omega$		17		MHz	
SR.	<b>Slew Rate</b>	$G = 1$ , 10-V step, $R_L = 5 \Omega$		50		$V/\mu s$	
	Full-power bandwidth	$G = +2$ , $V_{OUT} = 10 Vp-p$		1		MHz	
	Settling time: ±0.1%	$G = -1$ , 10-V step		1		μs	
THD+N	Total harmonic distortion + noise	f = 1 kHz, $R_1$ = 5 $\Omega$ , G = +2, V <sub>O</sub> = 10 V <sub>PP</sub>		0.02		$\%$	
		$f = 1$ MHz		3			
<b>OUTPUT</b>							
		Positive, $IO = 0.5 A$	$(V+) - 1$	$(V+) - 0.7$		$\vee$	
		Negative, $IO = -0.5 A$	$(V-) + 1$	$(V-) + 0.7$			
	Voltage output	Positive, $IO = 1$ A	$(V+) - 1.5$	$(V+) - 1.2$			
		Negative, $I_{O} = -1$ A	$(V-) + 1.5$	$(V-) + 1.2$			
	Maximum continuous current output, dc			1.2		A	
$Z_{O}$	Output impedance	$G = +2$ , $f = 100$ kHz		0.05		Ω	
	Output current limit Range			$±0.2$ to ±1.2		A	
	Current limit tolerance <sup>(2)</sup>	$R_{CL} = 2 k\Omega (I_{LIM} = \pm 1 A)$		±50		mA	
	Asymmetry	Comparing positive and negative limits		10		$\%$	
	Current limit overshoot <sup>(3)</sup>	V = 5-V pulse (200 ns $t_r$ ), G = +2		50		%	

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## <span id="page-5-0"></span>**5.5 Electrical Characteristics (continued)**

at  $T_{\text{CASE}}$  = 25°C,  $V_{\text{S}}$  = 15 V, load connected to V/2, and E/S enabled (unless otherwise noted)



(1) High-speed test at T<sub>J</sub> = +25°C.

(2) See text for more information on current limit accuracy.

(3) Transient load transition time must be  $\geq 200$  ns.

 $(4)$  402-k $\Omega$  pullup resistor to V+ can be used to permanently enable the OPA561.

<span id="page-6-0"></span>

## **5.6 Typical Characteristics**

at T $_{\mathsf{CASE}}$  = 25°C, V $_{\mathsf{S}}$  = 15 V, and E/S enabled (unless otherwise noted)



## **5.6 Typical Characteristics (continued)**

at  $T_{\text{CASE}}$  = 25°C,  $V_{\text{S}}$  = 15 V, and E/S enabled (unless otherwise noted)





at  $T_{\text{CASE}}$  = 25°C,  $V_{\text{S}}$  = 15 V, and E/S enabled (unless otherwise noted)





## <span id="page-9-0"></span>**6 Detailed Description**

## **6.1 Overview**

The OPA561 is a monolithic low-cost, high-current operational amplifier capable of driving up to 1.2 A pulses into reactive loads. The amplifier is designed to provide high slew rate, which results in 1-MHz full-power bandwidth and excellent linearity. The OPA561 operates from either a single supply in the range of 7 V to 15 V or dual power supplies of  $\pm 3.5$  V to  $\pm 7.5$  V for design flexibility.

## **6.2 Feature Description**

### **6.2.1 Adjustable Current Limit**

The OPA561 has an accurate, user-defined, current limit which can be set from 0.2 A to 1.2 A by controlling the input to the  $I_{LIM}$  pin. Unlike other designs that use a power resistor in series with the output current path, the OPA561 senses the load internally. This allows the current limit to be set with low-power components. In contrast, other designs require one or two expensive power resistors that can handle the full output current (1.2 A in this case).

#### *6.2.1.1 Current Limit Accuracy*

The OPA561 has separate circuits to monitor the positive and negative currents. Each output is compared to a single internal reference that is set by the external current limit resistor (or voltage). The OPA561 employs a patented circuit technique to achieve an accurate and stable current limit. The output current limit has an accuracy of up to 5% on the 1-A current limit. Due to internal matching limitations, the positive and negative current limits can be slightly different. However, the values are typically within 10% of each other.

#### *6.2.1.2 Setting the Current Limit*

Do not float the I<sub>LIM</sub> pin or damage to the device is possible. Connect I<sub>LIM</sub> directly to V− to program the maximum output current limit, typically 1.2 A. The simplest method for adjusting the current limit ( $I_{LIM}$ ) uses a resistor or potentiometer connected between the ILIM pin and V− according to the following equation:

$$
I_{LIM} = \left(\frac{1.2V}{R_{CL} + 10k\Omega}\right) \times 10,000\tag{1}
$$

This external resistor determines a small internal current which sets the desired output current limit. Alternatively, the output current limit can be set by applying a voltage to the  $I_{LIM}$  pin. Figure 6-1 shows a simplified schematic of the OPA561 current limit.



**Figure 6-1. Adjustable Current Limit — Resistor Method** 

<span id="page-10-0"></span>

#### **6.2.2 Enable-Status (E/S) Pin**

The enable-status (E/S) pin provides two unique functions:

- 1. Output disable by forcing the pin LOW
- 2. Thermal shutdown indication by monitoring the voltage level at the pin

One or both of these functions can be used on the same device. For normal operation (output enabled), pull the E/S pin high (at least 2 V greater than V−). A small-value capacitor can be connected between the E/S pin and V− for noisy applications. To enable the OPA561 permanently, tie the E/S pin to V+ through a 402‑kΩ pullup resistor.

#### *6.2.2.1 Output Disable*

The shutdown pin is referenced to the negative supply (V−). Therefore, shutdown operation is slightly different in single-supply and dual-supply applications. In single-supply operation, V− typically equals common ground. Therefore, the shutdown logic signal and the OPA561's shutdown pin are referenced to the same potential. In this configuration, the logic pin and the OPA561 enable can simply be tied together. Shutdown occurs for voltage levels of < 0.8 V. The OPA561 is enabled at logic levels > 2 V. In dual-supply operation, the logic pin is still referenced to a logic ground. However, the shutdown pin of the OPA561 is still referenced to V−. To shutdown the OPA561, the voltage level of the logic signal needs to be level shifted using an optocoupler, as shown in Figure 6-2. wever, the shutdown pin of the logic signal needs to be<br>
(a)  $+5V$  (b) HCT or TTL In



**Figure 6-2. Shutdown Configuration for Dual Supplies**

To disable the output, the E/S pin is pulled LOW, to no greater than 0.8 V above V−. This function can be used to conserve power during idle periods. The typical time required to shut down the output is 50 ns. To return the output to an enabled state, the E/S pin can be pulled to at least 2.0 V above V−. Typically, the output is enabled within 3 μs. Note that pulling the E/S pin HIGH (output enabled) does not disable the internal thermal shutdown.



#### *6.2.2.2 Maintaining Microcontroller Compatibility*

Not all microcontrollers output the same logic state after power-up or reset. 8051-type microcontrollers, for example, output logic-high levels on the ports, whereas other models power up with logic low levels after reset. In [Figure 6-2,](#page-10-0) configuration (a) the shutdown signal is applied on the cathode side of the photodiode within the optocoupler. A high logic level causes the OPA561 to be enabled, and a low logic level shuts down the OPA561. In [Figure 6-2](#page-10-0), configuration (b), with the logic signal applied on the anode side, a high level causes the OPA561 to shut down, and a low level enables the op amp.

#### **6.2.3 Overcurrent Flag**

The OPA561 features an overcurrent status flag (CLS, pin 9) that can be monitored to see if the load exceeds the current limit. The output signal of the overcurrent limit flag is compatible to standard logic. The CLS signal is referenced to V−. A voltage level less than (V−) + 0.8 V indicates normal operation, and a level greater than (V−) + 2 V indicates that the OPA561 is current limited. The flag remains high as long as the output of the OPA561 current limited. At very low signal frequencies (typically < 1 kHz), both the upper (sourcing current) and lower (sinking current) current limits are monitored. At frequencies > 1 kHz, as a result of internal circuit limitations, the flag output signal for the upper current limit becomes delayed and shortened. The flag signal for the lower current limit is unaffected by this behavior. As the signal frequency increases further, only the lower current limit (sinking current) is output on pin 9.

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## **7 Application and Implementation**

#### **Note**

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes, as well as validating and testing their design implementation to confirm system functionality.

## **7.1 Application Information**

Figure 7-1 shows the OPA561 connected as a basic noninverting amplifier. However, the OPA561 can be used in virtually any op amp configuration. Reinforce power supply terminals with low series impedance capacitors. The technique of using a ceramic and tantalum type in parallel is recommended. Low series impedance power supply wiring is recommended.



#### **Figure 7-1. Basic Circuit Connections**

#### **7.1.1 Output Stage Compensation**

The complex load impedances common in power op amp applications can cause output stage instability. For normal operation, output compensation circuitry is typically not required. However, if the OPA561 is intended to be driven into current limit, implementing an R/C network (snubber) is recommended. A snubber circuit also helps to enhance stability when driving large capacitive loads (> 1000 pF) or inductive loads (motors, loads separated from the amplifier by long cables). Typically,  $3 \Omega$  to 10  $\Omega$  in series with 0.01 µF to 0.1 µF is adequate. Varying the component values can help with challenging load conditions.



#### <span id="page-13-0"></span>**7.1.2 Output Protection**

Reactive and EMF-generation loads can return load current to the amplifier, causing the output voltage to exceed the power-supply voltage. This damaging condition can be avoided with clamp diodes from the output terminal to the power supplies, as shown in Figure 7-2. Schottky rectifier diodes with a 3 A or greater continuous rating are recommended.



**Figure 7-2. Output Protection Diode**

#### **7.1.3 Thermal Protection**

The OPA561 has thermal sensing circuitry that helps protect the amplifier from exceeding temperature limits. Power dissipated in the OPA561 causes the junction temperature to rise. Internal thermal shutdown circuitry shuts down the output when the die temperature reaches approximately 160°C, resetting when the die has cooled to approximately 140°C. Depending on load and signal conditions, the thermal protection circuit can cycle on and off. This cycling limits the dissipation of the amplifier, but can have an undesirable effect on the load. Any tendency to activate the thermal protection circuit indicates excessive power dissipation or an inadequate heat sink. For reliable, long-term, continuous operation, limit the junction temperature to 125°C, maximum. To estimate the margin of safety in a complete design (including heat sink), increase the ambient temperature until the thermal protection is triggered. Use worst-case loading and signal conditions. For good, long-term reliability, set the thermal protection to trigger at more than 35°C greater than the maximum expected ambient condition of your application. This configuration produces a junction temperature of 125°C at the maximum expected ambient condition. The internal protection circuitry of the OPA561 is designed to protect against overload conditions, and is not intended to replace a proper heat sink. Continuously running the OPA561 into thermal shutdown can degrade reliability. The E/S pin can be monitored to determine if shutdown has occurred. During normal operation the voltage on the E/S pin is typically greater than (V−) + 2 V. During shutdown, the voltage drops to less than (V−) + 0.8 V.

<span id="page-14-0"></span>

(2)

#### **7.1.4 Power Dissipation**

Power dissipation depends on power supply, signal, and load conditions. For DC signals, power dissipation is equal to the product of output current times the voltage across the conducting output transistor. Dissipation with ac signals is lower. The *[Power Amplifier Stress and Power Handling Limitations](https://www.ti.com/lit/pdf/SBOA022)* application bulletin explains how to calculate or measure power dissipation with unusual signals and loads, and can be downloaded from www.ti.com.

### **7.1.5 Heat-Sink Area**

The relationship between thermal resistance and power dissipation can be expressed as:

$$
\theta_{JA} = \frac{T_J - T_A}{P_D}
$$

Where:

- $T_J$  = Junction temperature (°C)
- $T_A$  = Ambient temperature (°C)
- $\theta_{JA}$  = Junction-to-ambient thermal resistance (°C/W)
- $P_D$  = Power dissipation (W)

Calculate the appropriate power dissipation to determine required heat-sink area. At the same time, consider the relationship between power dissipation and thermal resistance to minimize shutdown conditions and allow for proper long-term operation (junction temperature of 125 °C). After the heat-sink area has been selected, verify proper thermal protection by testing worst-case load conditions. For applications with limited board size, refer to Figure 7-3 for the approximate thermal resistance relative to heat-sink area. Increasing heat-sink area beyond 2 in<sup>2</sup> provides little improvement in thermal resistance. To achieve the 32 °C/W stated in the *Electrical Characteristics*, a copper plane size of 9 in<sup>2</sup> was used. The HTSSOP-20 PowerPAD integrated circuit package is a good choice for continuous power levels from 2 W to 4 W, depending on ambient temperature and heat-sink area. Higher power levels can be achieved in applications with a low on-off duty cycle, such as remote meter reading.



**Figure 7-3. Thermal Resistance vs Circuit Board Copper Area**



#### **7.1.6 Amplifier Mounting**

#### *7.1.6.1 What is the PowerPAD™ Integrated Circuit Package?*

The OPA561 uses the HTSSOP-20 PowerPAD integrated circuit package, a thermally enhanced, standard-size IC package designed to eliminate the use of bulky heat sinks and slugs traditionally used in thermal packages. This package can be easily mounted using standard PCB assembly techniques, and can be removed and replaced using standard repair procedures.

The PowerPAD package is designed so that the leadframe die pad (or thermal pad) is exposed on the bottom of the IC, as shown in Figure 7-4. This provides an extremely low thermal resistance  $(\theta_{\text{JC}})$  path between the or the lot, as shown in Figure 7-4. This provides an extremely low themal resistance ( $\sigma_{JC}$ ) path between the die and the exterior of the package. The thermal pad on the bottom of the IC must be soldered directly to the PCB, using the PCB as a heat sink. In addition, through the use of thermal vias, the thermal pad can be directly<br>
connected to a ground plane or special heat sink structure designed into the PCB.<br>
Leadframe (Copper Alloy) connected to a ground plane or special heat sink structure designed into the PCB.



**Figure 7-4. Section View of a PowerPAD Package**

Soldering the thermal pad to the PCB is always recommended, even with applications that have low power dissipation. Soldering provides the necessary connection between the leadframe die and the PCB. Connect the thermal pad to the most negative supply of the device.



#### *7.1.6.2 PowerPAD™ Integrated Circuit Package Assembly Process*

- 1. Prepare the PCB with a top-side etch pattern, as shown in the attached *Thermal Land Pattern* mechanical drawing. Use etch for the leads as well as etch for the thermal land.
- 2. Place the recommended number of holes (or thermal vias) in the area of the thermal pad as shown on the attached *Land Pattern* mechanical. Use holes that are 13 mils in diameter. Keep the holes small so that solder wicking through the holes is not a problem during reflow.
- 3. Best practice is to place a small number of the holes under the package and outside the thermal pad area. These holes provide additional heat path between the copper land and ground plane and are 25 mils in diameter. The holes can be larger because the holes are not in the area to be soldered, so wicking is not a problem.
- 4. Connect all holes, including those within the thermal pad area and outside the pad area, to the internal ground plane or other internal copper plane.
- 5. When connecting these holes to the ground plane, do not use the typical web or spoke via connection methodology; see Figure 7-5. Web connections have a high thermal resistance that is useful for slowing the heat transfer during soldering operations. This heat-transfer slowing makes the soldering of vias that have plane connections easier. However, in this application, low thermal resistance is desired for the most efficient heat transfer. Therefore, connect the holes under the PowerPAD package to the internal ground plane with a complete connection around the entire circumference of the plated through hole.
- 6. On the top-side solder mask, leave exposed the terminals of the package and the thermal pad area. On the thermal pad area, leave the 13 mil holes exposed. Cover the larger 25 mil holes outside the thermal pad area with solder mask.
- 7. Apply solder paste to the exposed thermal pad area and all of the package pins.
- 8. With these preparatory steps in place, the PowerPAD IC package is simply placed in position and run through the solder reflow operation, as with any standard surface-mount component. This procedure results in a part that is properly installed.

For detailed information on the PowerPAD IC package, including thermal modeling considerations and repair procedures, see the *[PowerPAD Thermally Enhanced Package](https://www.ti.com/lit/pdf/SLMA002)* technical brief, available at www.ti.com.



**Figure 7-5. Via Connection**



## <span id="page-17-0"></span>**7.2 Typical Application**

## **7.2.1 Laser Diode Driver**

The high output current and low supply of the OPA561 makes this device a good candidate for driving laser diodes and thermoelectric coolers. Figure 7-6 shows the OPA561 configured as a laser diode driver.



**Figure 7-6. Laser Diode Driver**

#### **7.2.2 Programmable Power Supply**

Figure 7-7 shows the OPA561 configured with the [MSP430](https://www.ti.com/product/MSP430)™ MCU, [REF3030](https://www.ti.com/product/REF3030), and [DAC7513](https://www.ti.com/product/DAC7513) as a space-saving, low-cost, programmable power-supply design. This design features low-voltage operation, small-size packages, (DAC7513 in SOT23-8, REF3030 in SOT23-3) and low cost. *I*ICU, REF3030, and<br>tures low-voltage op<br>R<sub>1</sub> R<sub>F</sub> R<sub>F</sub>







#### **7.2.3 Power-Line Communication Modem**



**Figure 7-8. Power-Line Communication Driver**

The OPA561 is an excellent choice to drive ac power lines for low-speed communication applications. The device provides an easily implemented, reliable option that is superior to discrete power transistor circuits. Advantages include:

- 1. Fully integrated device
- 2. Integrated shutdown circuitry for send-and-receive switching
- 3. Thermal shutdown
- 4. Adjustable current limit
- 5. Shutdown flag
- 6. Power savings
- 7. Small PowerPAD integrated circuit package

Typically such a system consists of a microcontroller, a modem IC and the power-line interface circuitry. See Figure 7-8 for the half-duplex power line communication system.

The system uses a synchronous FSK-modem, capable of 600-baud and 1200-baud data rates, and supports two different FSK channels in the 60‑kHz to 80‑kHz range. A microcontroller such as the [MSP430](https://www.ti.com/product/MSP430)™ MCU is used to control the modem IC.

The OPA561 analog interface circuitry drives the FSK modem signals on the ac power line. The circuitry filters the transmit signal (ATO) from the ST7536 to suppress the 2nd-harmonic distortion of the transmit signal. The circuitry also amplifies the ATO signal and provides the very low output impedance necessary to properly drive the line. The impedance of a typical power line at 70-kHz ranges from 1 Ω to 100 Ω. The OPA561 is an excellent choice for this type of load. The transformer provides isolation and additional filtering. C9 prevents 50‑Hz to 60‑Hz current from flowing in the transformer. Choose this capacitor carefully for proper voltage rating and safety characteristics.

The receive input signal is amplified (G = 100) and applied to the modem IC. The OPA561 is disabled in receive mode to avoid loading the line.



#### <span id="page-19-0"></span>**7.3 Power Supply Recommendations**

The OPA561 operates from single (7 V to 15 V) or dual (±3.5 V to ±7.5 V) supplies with excellent performance. Power-supply voltages do not need to be equal. For example, the positive supply can be set to 10 V with the negative supply at –5 V, or vice-versa. Most behaviors remain unchanged throughout the operating voltage range. Parameters that vary significantly with operating voltage are shown in the *Typical Characteristics*.

## **7.4 Layout**

#### **7.4.1 Layout Guidelines**

The OPA561 is a high-speed power amplifier that requires proper layout for best performance. Figure 7-9 shows an example of proper layout.

Keep power-supply leads as short as possible, which keeps inductance low and resistive losses at a minimum. A minimum 18-gauge wire thickness is recommended for power-supply leads. Use a wire length < 8 inches.

Proper power-supply bypassing with low-ESR capacitors is essential to achieve good performance. A parallel combination of small ceramic (around 100 nF) and larger (47 μF) nonceramic bypass capacitors provide low impedance over a wide frequency range. Place bypass capacitors as close as practical to the power-supply pins of the OPA561.

Keep PCB traces conducting high currents, such as from output to load or from the power-supply connector to the power-supply pins of the OPA561, as wide and as short as possible. This guideline helps keep inductance low and resistive losses to a minimum.

The holes in the landing pattern for the OPA561 are for the thermal vias that connect the thermal pad of the OPA561 to the heat sink area on the printed circuit board (see attached *Land Pattern* mechanical drawing). The additional larger vias further enhance the heat conduction into the heat-sink area. All traces conducting high currents are very wide for lowest inductance and minimal resistive losses. The negative supply (V−) pin on the OPA561 is connected through the thermal pad. This connection allows for maximum trace width for VOUT and the positive power supply  $(V+)$ .

#### **7.4.2 Layout Example**



**Figure 7-9. OPA561 Example Layout**

<span id="page-20-0"></span>

## **8 Device and Documentation Support**

TI offers an extensive line of development tools. Tools and software to evaluate the performance of the device, generate code, and develop solutions are listed below.

#### **8.1 Device Support**

#### **8.1.1 Third-Party Products Disclaimer**

TI'S PUBLICATION OF INFORMATION REGARDING THIRD-PARTY PRODUCTS OR SERVICES DOES NOT CONSTITUTE AN ENDORSEMENT REGARDING THE SUITABILITY OF SUCH PRODUCTS OR SERVICES OR A WARRANTY, REPRESENTATION OR ENDORSEMENT OF SUCH PRODUCTS OR SERVICES, EITHER ALONE OR IN COMBINATION WITH ANY TI PRODUCT OR SERVICE.

#### **8.2 Receiving Notification of Documentation Updates**

To receive notification of documentation updates, navigate to the device product folder on [ti.com.](https://www.ti.com) Click on *Notifications* to register and receive a weekly digest of any product information that has changed. For change details, review the revision history included in any revised document.

#### **8.3 Support Resources**

TI E2E™ [support forums](https://e2e.ti.com) are an engineer's go-to source for fast, verified answers and design help — straight from the experts. Search existing answers or ask your own question to get the quick design help you need.

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#### **8.4 Trademarks**

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#### **8.5 Electrostatic Discharge Caution**



This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

#### **8.6 Glossary**

[TI Glossary](https://www.ti.com/lit/pdf/SLYZ022) This glossary lists and explains terms, acronyms, and definitions.



## <span id="page-21-0"></span>**9 Revision History**

NOTE: Page numbers for previous revisions may differ from page numbers in the current version.



## **10 Mechanical, Packaging, and Orderable Information**

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

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