

# Control of Electrical Drives

## Equation set & model salient PM?

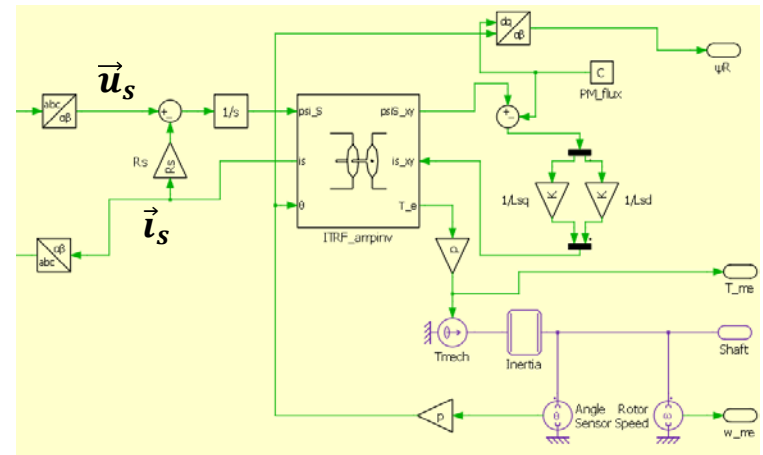
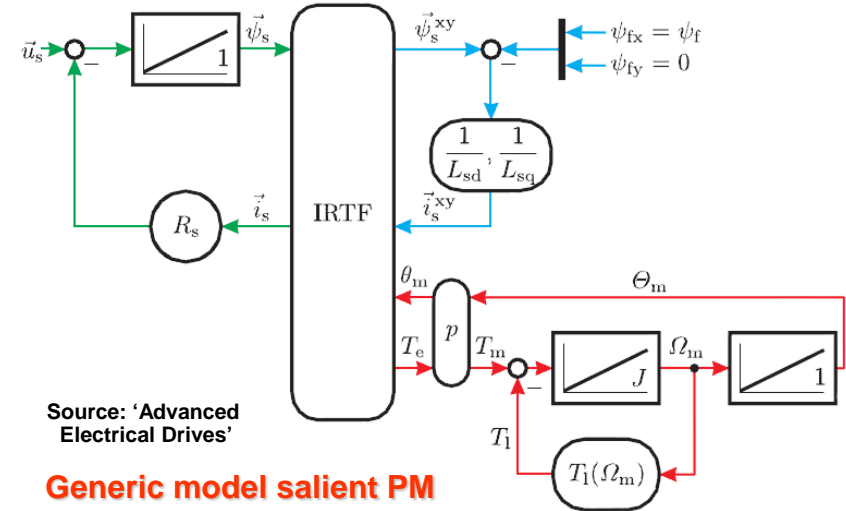
Equation set for 'p' pole pair machine :

- Terminal :  $\vec{u}_s = \vec{i}_s R_s + \frac{d\vec{\psi}_s}{dt}$
- Flux (x):  $\psi_{sx} = i_{sx} L_{sd} + \psi_f$
- Flux (y):  $\psi_{sy} = i_{sy} L_{sq}$
- Torque :  $T_e = \frac{3}{2} (\vec{\psi}_s \times \vec{i})$
- Mechanical:  $T_m - T_l = J \frac{d\Omega_m}{dt}$
- Rotational:  $\Omega_m = \frac{d\theta_m}{dt}$
- Pole pair related:  $T_m = pT_e$ ,  $\theta_m = p\Theta_m$

With permanent magnet flux :  $\psi_f$  and mechanical shaft speed  $\Omega_m$

Generic model based on above equation set uses:

- Voltage vector as input
- Dynamic model of mechanical side
- IRTF model
- Load torque module:  $T_l(\Omega_m)$



## Current controller?

# Field weakening control for non-salient PM machines

Moved from day 2

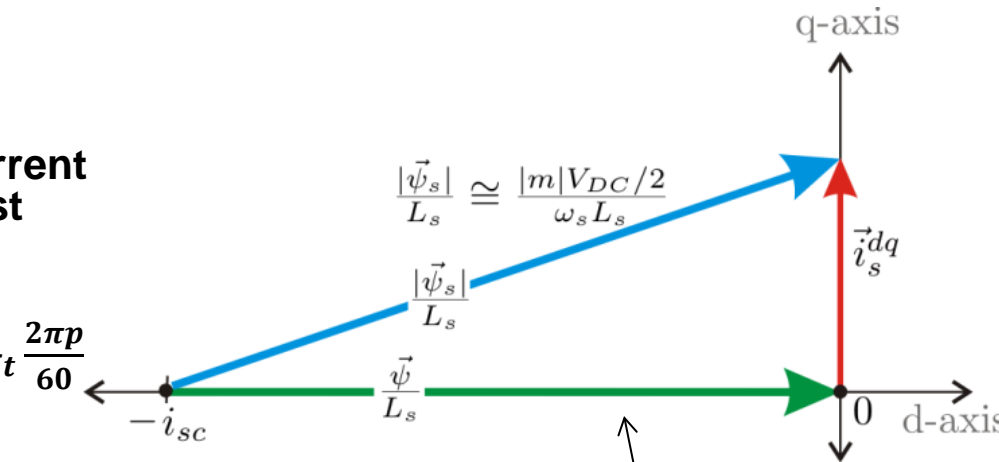
Recall basic motor equations:

$\vec{\psi}_s = \psi + L_s \vec{i}_s$ , which can be written as:  $\frac{\vec{\psi}_s}{L_s} = i_{sc} + \vec{i}_s$  with,  $i_{sc} = \frac{\psi}{L_s}$ ; PM short-circuit current

$\vec{u}_s = j\omega_s \vec{\psi}_s + R_s \vec{i}_s$ , if we ignore  $R_s \vec{i}_s$  for simplicity, then the stator flux amplitude can be written as  $\psi_s \sim \frac{m u_{DC}/2}{\omega_s}$ , using  $u_s = \frac{m u_{DC}}{2}$

## Representation in d,q diagram

- Example given with  $i_{sd} = 0$
- Modulation index  $|m|$  controlled by current controller, if speed increases,  $|m|$  must increase to maintain same stator flux value for given d,q current values
- Electrical speed is equal to  $\omega_s = n_{shaft} \frac{2\pi p}{60}$



Absolute value of modulation index  $|m|$  is limited by current controller.

We need to reduce length of stator flux vector if this condition is met and speed needs to be further increased

# Field weakening control for PM

Moved from day 2

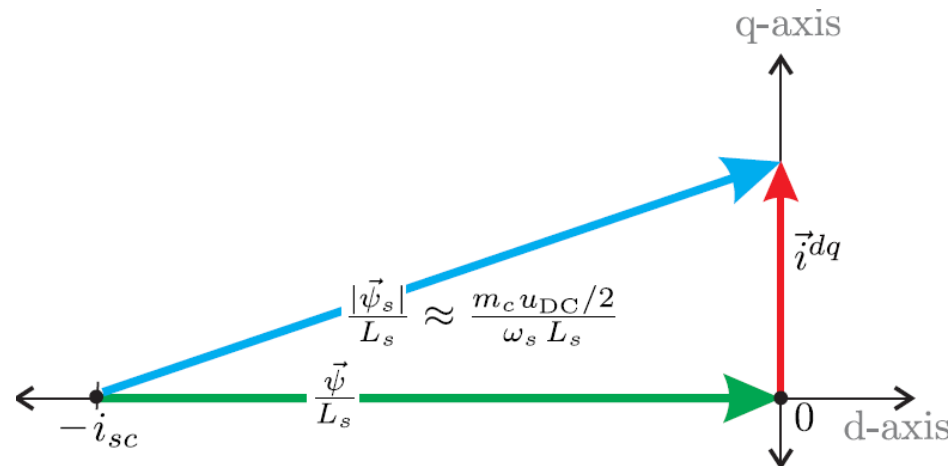
What is the operating speed which can be reached WITHOUT field weakening control?:

The estimate for the speed  $\omega_{sLim}$ , with  $i_{sd} = 0$ , can be found using Pythagoras and the d,q diagram namely

$$\left(\frac{m_c u_{DC}/2}{\omega_{sLim} L_s}\right)^2 = (i_{sc})^2 + (i_{sq})^2$$

which gives

$$n_{shLim} = \left(\frac{15}{\pi p L_s}\right) \frac{m_c u_{DC}}{\sqrt{(i_{sc})^2 + (i_{sq})^2}}$$



- A numerical example using the Teknic motor with :  $i_{sc} = 35.7$  A,  $i_{sq} = 2.6$  A,  $p = 4$ ,  $u_{DC} = 24$  V,  $L_s = 180.0$   $\mu$ H and current controller modulation index of  $m_c=1$  gives a theoretical maximum achievable shaft speed (without field weakening) of  $n_{shLim} = 4450$  rpm

How can we extend this speed range?