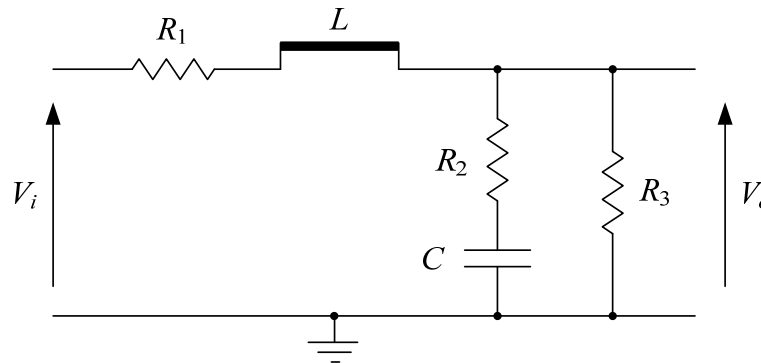


Design Example - 1

Step 1: Determine the plant transfer function



$$\begin{aligned}L &= 0.9 \mu\text{H} \\C &= 471 \mu\text{F} \\R_1 &= 2.2 \text{ m}\Omega \\R_2 &= 0.6 \text{ m}\Omega \\R_3 &= 1 \Omega\end{aligned}$$

The switching frequency is 1 MHz.

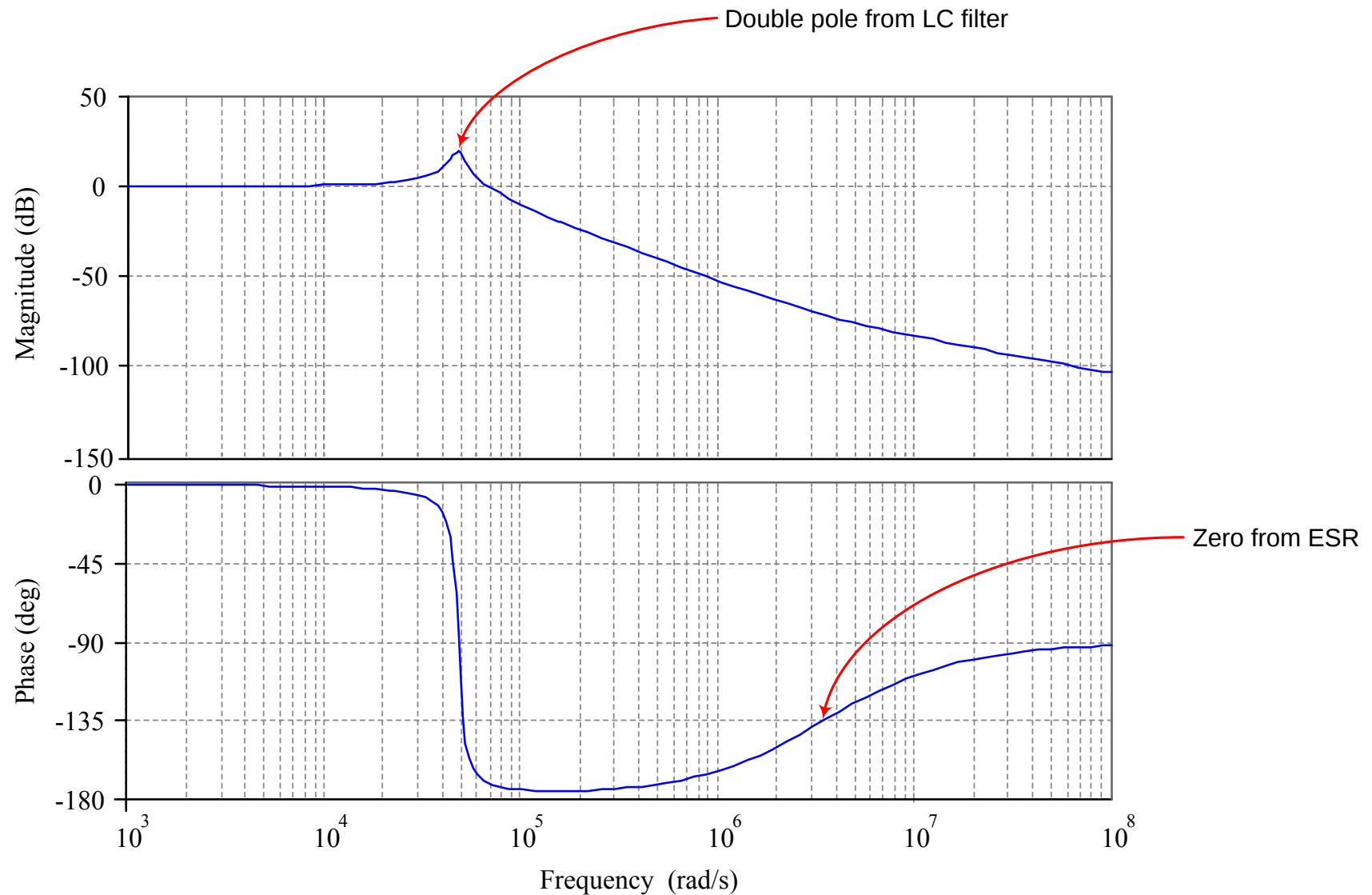
In Continuous Conduction Mode (CCM) the buck output stage has transfer function

$$G(s) = \frac{sCR_2R_3 + R_3}{s^2LC(R_2 + R_3) + s(CR_1(R_2 + R_3) + CR_2R_3 + L) + (R_1 + R_3)}$$

Inserting the passive component values for the workshop board, we obtain

$$G(s) = \frac{2.826 \times 10^{-7} s + 1}{4.252 \times 10^{-10} s^2 + 2.219 \times 10^{-6} s + 1.002}$$

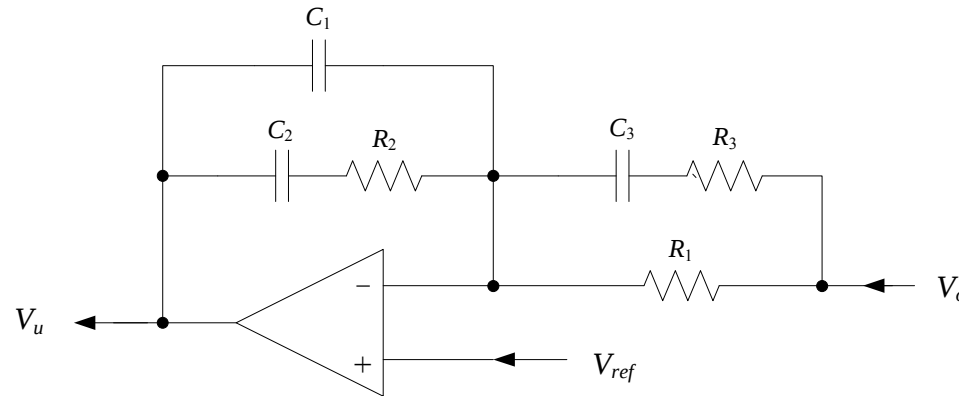
Design Example - 1a



The plant frequency response exhibits a well-defined peak in the magnitude curve from the LC filter, and a high-frequency zero from ESR of the output capacitor.

Design Example - 2

Step 2: Design the analog compensator



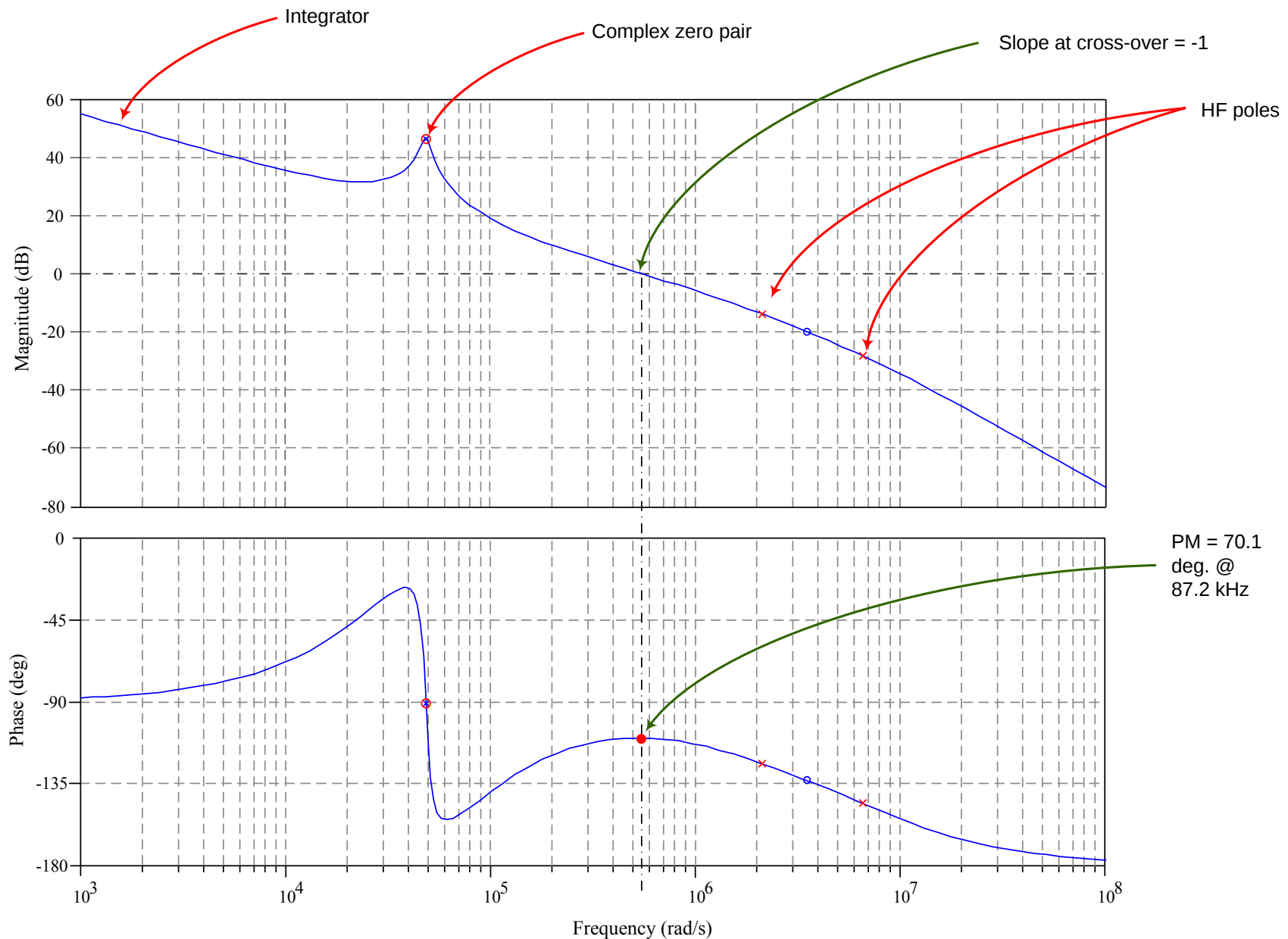
The transfer function of the classical type III compensator is

$$F(s) = \frac{R_1 + R_3}{R_1 R_3 C_1} \frac{\left(s + \frac{1}{R_2 C_2}\right) \left(s + \frac{1}{(R_1 + R_3) C_3}\right)}{s \left(s + \frac{C_1 + C_2}{R_2 C_1 C_2}\right) \left(s + \frac{1}{R_3 C_3}\right)}$$

Pole & zero frequencies are selected using any of the established design techniques.

$$F(s) = A_s \frac{(s + \omega_{z1})(s + \omega_{z2})}{s(s + \omega_{p1})(s + \omega_{p2})}$$

Design Example - 2a



Frequency response plot of open loop with analogue compensator.

Design Example - 3

Step 3: Transform the compensator into discrete time

$$F(s) = A_s \frac{(s + \omega_{z1})(s + \omega_{z2})}{s(s + \omega_{p1})(s + \omega_{p2})}$$

The digital transfer function can be formed using a Tustin transformation: $s \leftarrow \frac{2}{T} \frac{z-1}{z+1}$

$$F(z) = A_s \frac{\left(\frac{2}{T} \frac{z-1}{z+1} + \omega_{z1} \right) \left(\frac{2}{T} \frac{z-1}{z+1} + \omega_{z2} \right)}{\frac{2}{T} \frac{z-1}{z+1} \left(\frac{2}{T} \frac{z-1}{z+1} + \omega_{p1} \right) \left(\frac{2}{T} \frac{z-1}{z+1} + \omega_{p2} \right)}$$

The 0Hz gains of the transfer functions must be matched: $|F(s)|_{s=0} = |F(z)|_{z=1}$

After some algebra, we arrive at the third order digital transfer function

$$F(z) = \frac{b_0 + b_1 z^{-1} + b_2 z^{-2} + b_3 z^{-3}}{1 + a_1 z^{-1} + a_2 z^{-2} + a_3 z^{-3}}$$

Design Example - 3a

Using the Tustin method, we have transformed a transfer function in s to one in z.

$$F(s) = \frac{\omega_{p1}}{s} \frac{\left(\frac{s}{\omega_{z1}} + 1\right)\left(\frac{s}{\omega_{z2}} + 1\right)}{\left(\frac{s}{\omega_{p2}} + 1\right)\left(\frac{s}{\omega_{p3}} + 1\right)} \quad \Rightarrow \quad F(z) = \frac{b_0 + b_1 z^{-1} + b_2 z^{-2} + b_3 z^{-3}}{1 + a_1 z^{-1} + a_2 z^{-2} + a_3 z^{-3}}$$

After a lot of algebra, the coefficients turn out to be:

$$a_1 = -\frac{-12 + T^2 \omega_{p2} \omega_{p3} - 2T(\omega_{p2} + \omega_{p3})}{(2 + T\omega_{p2})(2 + T\omega_{p3})}$$

$$a_2 = -\frac{12 + T^2 \omega_{p2} \omega_{p3} - 2T(\omega_{p2} + \omega_{p3})}{(2 + T\omega_{p2})(2 + T\omega_{p3})}$$

$$a_3 = -\frac{(-2 + T\omega_{p2})(-2 + T\omega_{p3})}{(2 + T\omega_{p2})(2 + T\omega_{p3})}$$

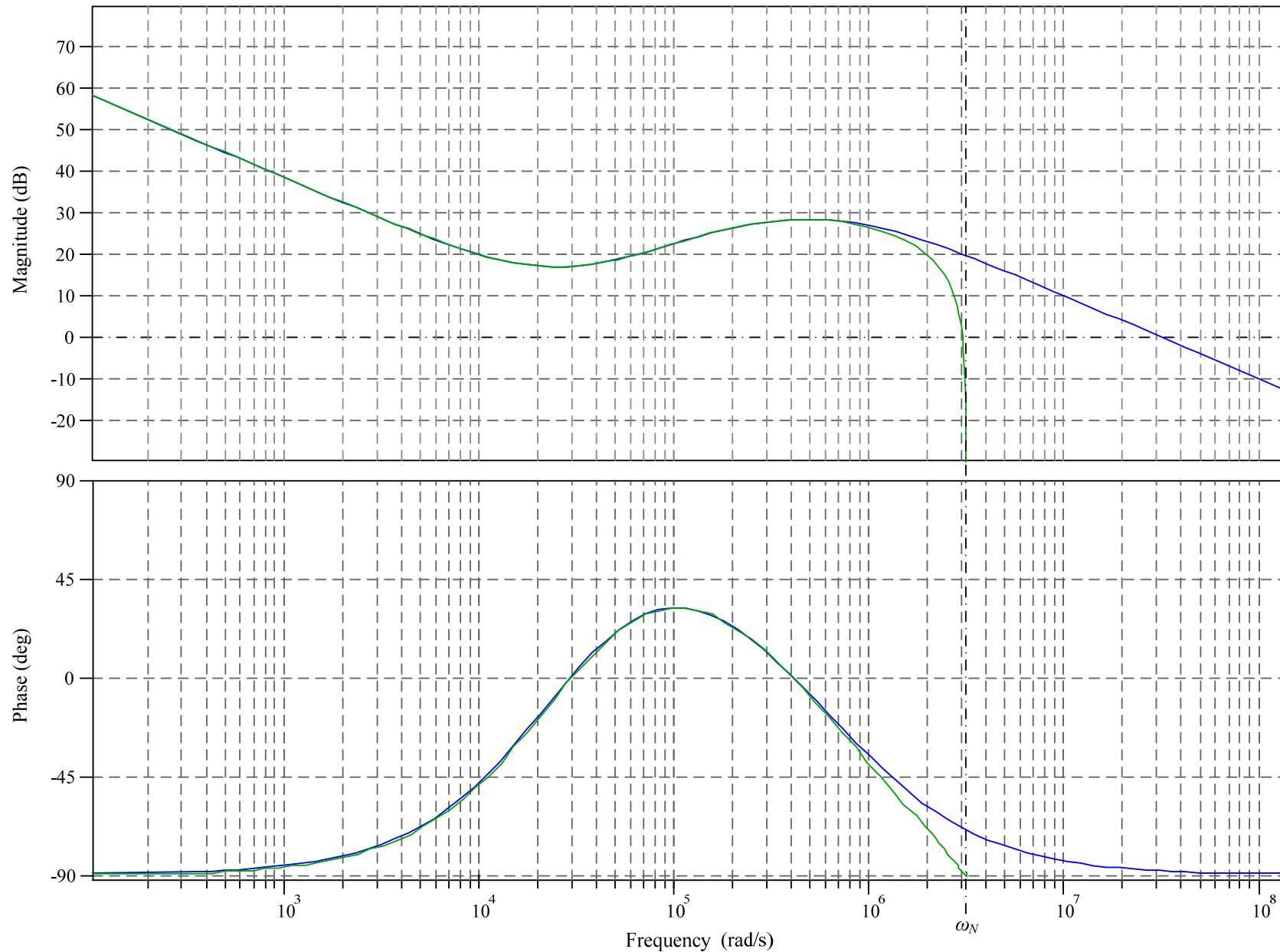
$$b_0 = \frac{T\omega_{p1}\omega_{p2}\omega_{p3}(2 + T\omega_{z1})(2 + T\omega_{z1})}{2\omega_{z1}\omega_{z2}(2 + T\omega_{p2})(2 + T\omega_{p3})}$$

$$b_1 = \frac{T\omega_{p1}\omega_{p2}\omega_{p3}(-4 + 3T^2\omega_{z1}\omega_{z2} + 2T(\omega_{z1} + \omega_{z2}))}{2\omega_{z1}\omega_{z2}(2 + T\omega_{p2})(2 + T\omega_{p3})}$$

$$b_2 = \frac{T\omega_{p1}\omega_{p2}\omega_{p3}(-4 + 3T^2\omega_{z1}\omega_{z2} - 2T(\omega_{z1} + \omega_{z2}))}{2\omega_{z1}\omega_{z2}(2 + T\omega_{p2})(2 + T\omega_{p3})}$$

$$b_3 = \frac{T\omega_{p1}\omega_{p2}\omega_{p3}(-2 + T\omega_{z1})(-2 + T\omega_{z2})}{2\omega_{z1}\omega_{z2}(2 + T\omega_{p2})(2 + T\omega_{p3})}$$

Design Example - 3b



Frequency response comparison of analogue (blue) and digital (green) compensators. $f_s = 1\text{MHz}$.

Design Example - 4

Step 4: Determine the difference equation for the compensator

Normalizing to the highest power of z in the denominator

$$F(z) = \frac{u(z)}{e(z)} = \frac{b_0 + b_1 z^{-1} + b_2 z^{-2} + b_3 z^{-3}}{1 + a_1 z^{-1} + a_2 z^{-2} + a_3 z^{-3}}$$

$$u(z) = b_0 e(z) + b_1 z^{-1} e(z) + b_2 z^{-2} e(z) + b_3 z^{-3} e(z) - a_1 z^{-1} u(z) - a_2 z^{-2} u(z) - a_3 z^{-3} u(z)$$

To find the difference equation, we simply apply the shifting property of the z transform

$$\mathcal{Z}\{f(k-n)\} = z^{-n} f(z)$$

$$u(k) = b_0 e(k) + b_1 e(k-1) + b_2 e(k-2) + b_3 e(k-3) - a_1 u(k-1) - a_2 u(k-2) - a_3 u(k-3)$$

All that remains is to code and test the controller algorithm.