

From LM3481 TI application note

$$L_M(V_{IN}) = \frac{V_{IN}^2 \times \eta}{K_L \times P_O \times f_s} \times \frac{V_{OUT}^2 \times N_{ps}^2}{(V_{IN} + V_{OUT} \times N_{ps})^2}$$

where

- P_O is output power
- f_s is flyback converter frequency

Table 2. Design Specifications

PARAMETER	EXAMPLE VALUE
Vin min	5 VDC
Vin max	32 VDC
Vout	12 VDC
Iout	2 max
Target switching frequency	130 kHz

Setting $f_s = 130$ kHz, $K_L = 0.2$ and $\eta = 0.85$, the curve of L_m and V_{in} relationship could be derived as shown in Figure 9. Choose $L_m = 12$ μ H.

$$N_{ps} = \frac{V_{IN_min}}{V_{OUT}} \times \frac{D_{max}}{1-D_{max}} = \frac{5 \times 0.7}{12 \times (1-0.7)} \approx 1 \quad (23)$$

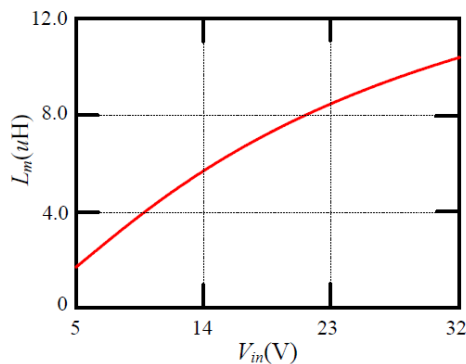


Figure 9. The Curve of Lm and Vin Relationship

$$Vin_min := 5 \text{ V} \quad Vin_max := 32 \text{ V} \quad Iout := 2 \text{ A} \quad Nps := 1 \quad Kl := 0.2$$

$$Vout := 12 \text{ V} \quad Po := Vout \cdot Iout \quad Po = 24 \text{ W} \quad n := 0.85 \quad fs := 130 \text{ kHz}$$

$$Lm_min := \frac{Vin_min^2 \cdot n}{Kl \cdot Po \cdot fs} \cdot \frac{Vout^2 \cdot Nps^2}{(Vin_min + Vout \cdot Nps)^2} \quad Lm_min = 16.968 \text{ } \mu\text{H} \quad @5Vin$$

$$Lm_max := \frac{Vin_max^2 \cdot n}{Kl \cdot Po \cdot fs} \cdot \frac{Vout^2 \cdot Nps^2}{(Vin_max + Vout \cdot Nps)^2} \quad Lm_max = 103.751 \text{ } \mu\text{H} \quad @32Vin$$

Calculated inductance values are not matching with the Figure 9. To be checked with TI supplier