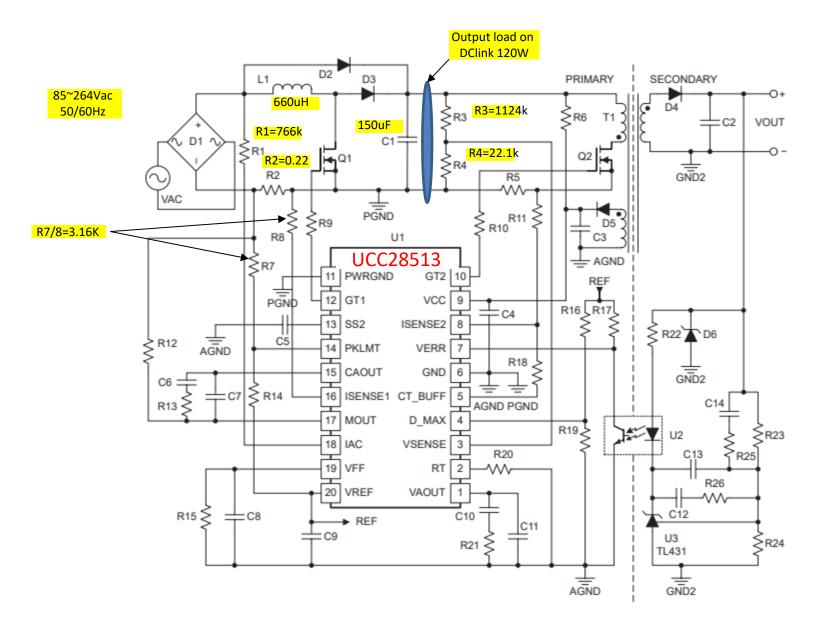
UCC28513 questions, Alex W., 11/17/2022

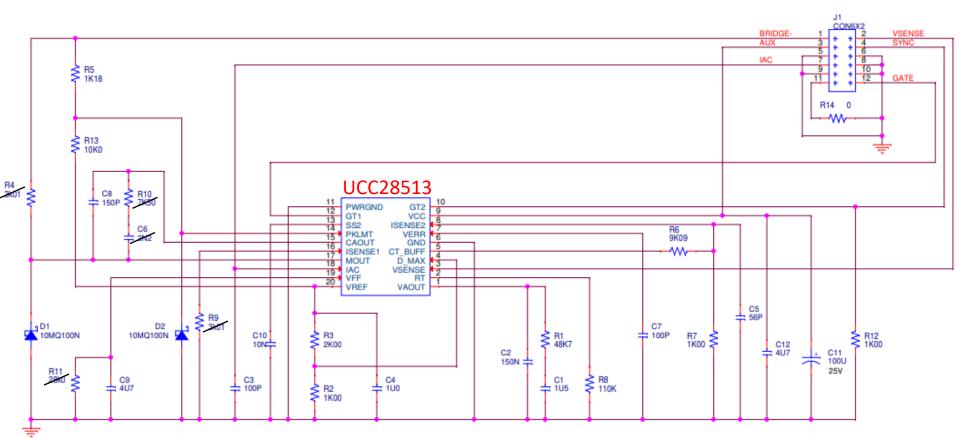
- The boost stage design is based on UCC28513. The PFC stage works well up to 200-220Vac input. Above this voltage range there are significant distortions at the points where sinusoidal input voltage reaches to its positive and negative peaks
- Output voltage is 385Vac
- Input voltage range is 85-264Vac; 50/60Hz
- The load on DC link output is 120W max
- Boost stage switching frequency is 277kHz
- Verified that the Vcc aux supply and Vref are stable
- Observed that the AC ripple on DC link goes up at around 200Vac but not sure it this is the reason or the result
- Observed that the duty cycle is about 70% at the peak sine wave at 85Vac but drops down to ~15% at the peaks of 220Vac at which point I start get distortions on the input current.
- The provided test results are at ~30W output power. It was observed that changing the load did not affect the behavior at around 220Vac.

# <u>Questions:</u>

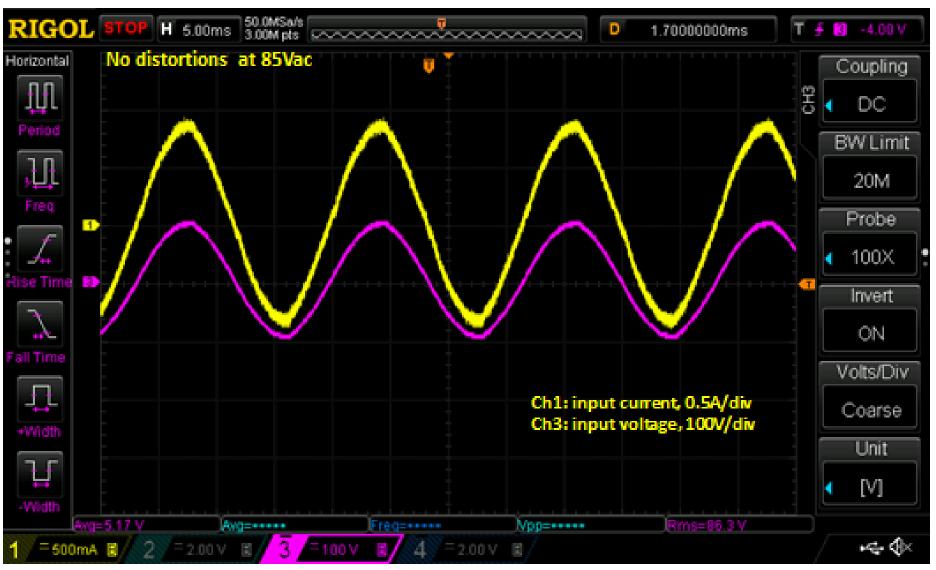
- 1. Based on the design values, what could potentially cause the distortions at the peak of sine waves at and above ~ 200Vac?
- 2. Fig. 36 on data sheet talks about max capacitance vs min duty cycle. What capacitor is referred in Fig 36?

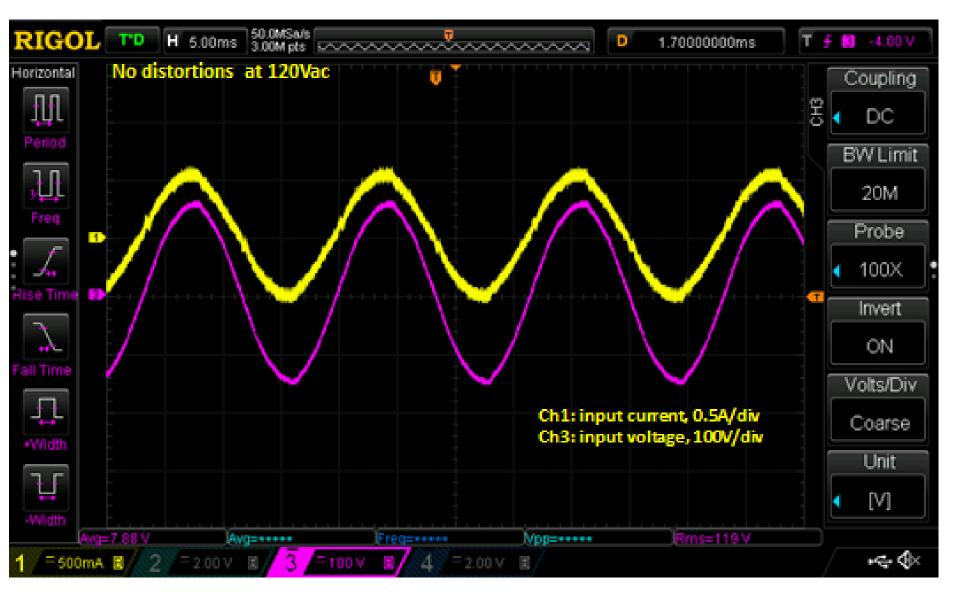


RefDes on data sheet	RefDes in design	values	
R1	R47+R50	766K	
R2	R43	0.22	
R8/R12	R4/R9	3.16K	
R3	R44+R49	1124K	
R4	R60	22.1k	
C1	C32	150uF	
L1	L2	660uH	
R13	R10	15.8K	
C6	C6	680pF	
С7	C8	150pF	
R15	R11	30.1K	
C8	С9	4.7uF	
C10	C1	1.5uF	
C11	C2	150nF	
R21	R1	48.7K	
R14	R13	10K	
R7	R5	1.18K	
С9	C4	1uF	

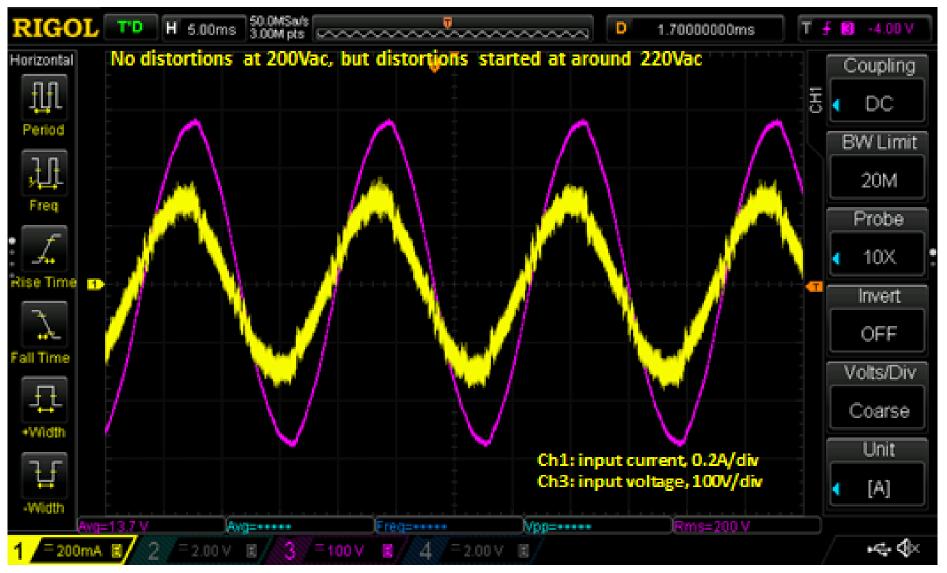


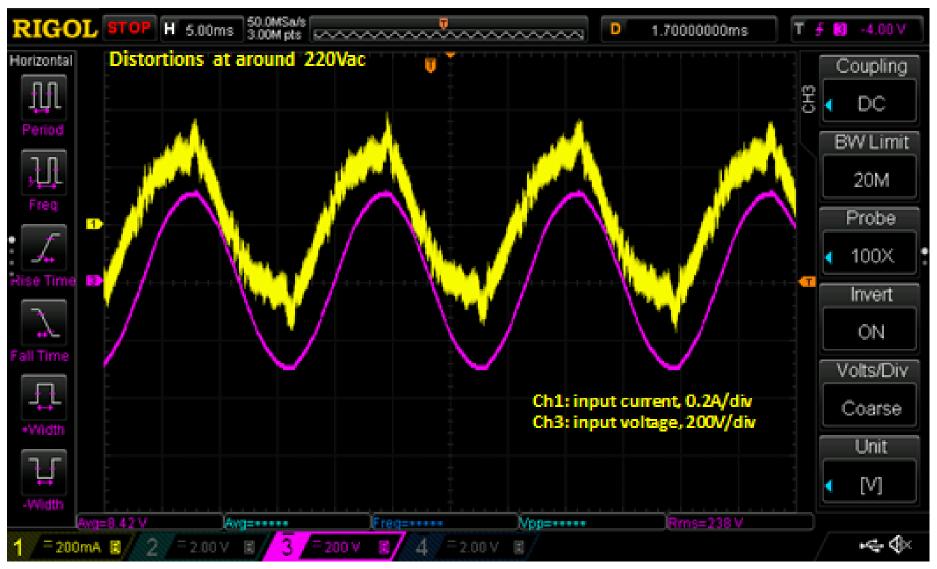
RefDes on data sheet	RefDes in design	values	
R8/R12	R4/R9	3.16K	
R13	R10	15.8K	
C6	C6	680pF	
R15 R11		30.1K	



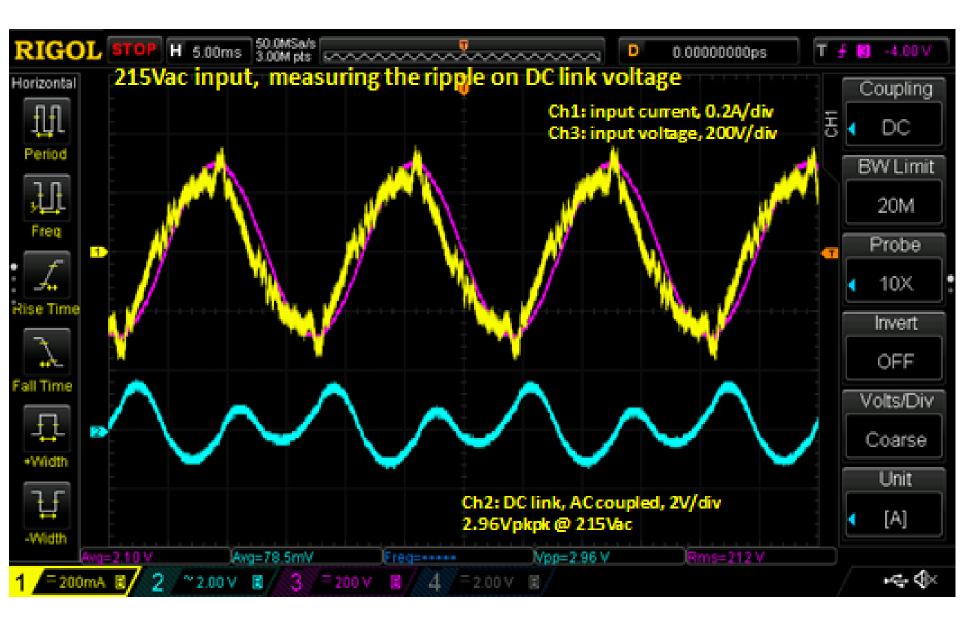


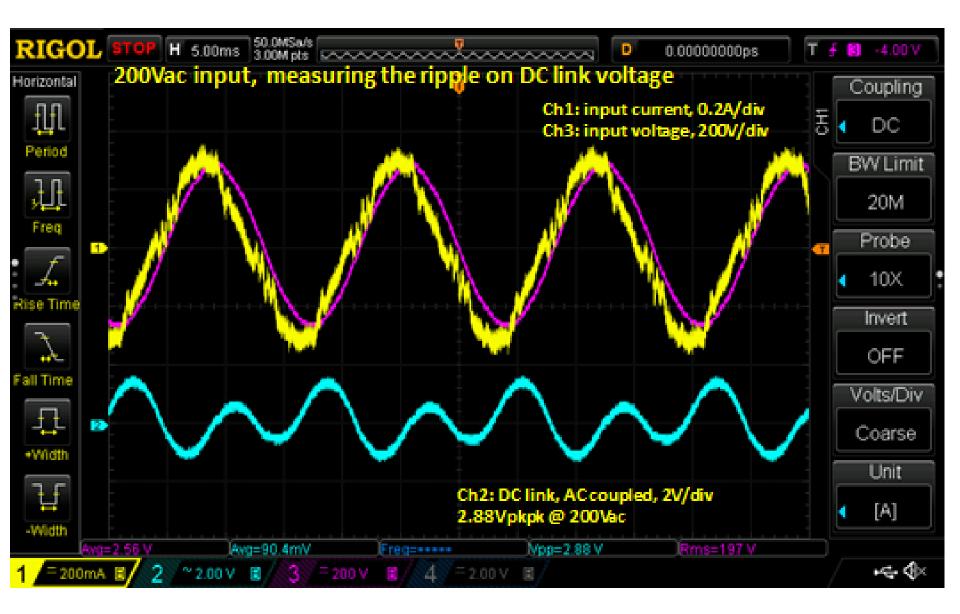
# No distortions at 200Vac input, displacement between current and voltage is probably caused by the input capacitors on EMI filter



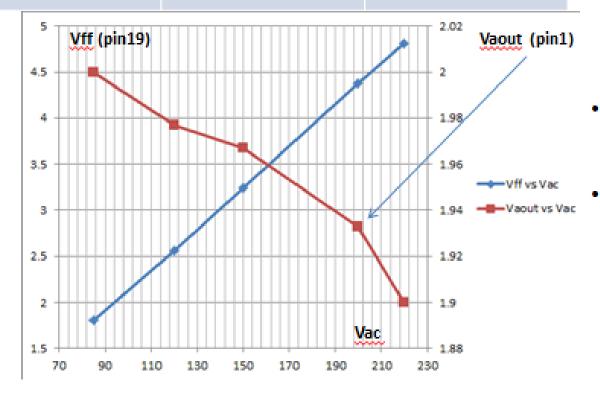








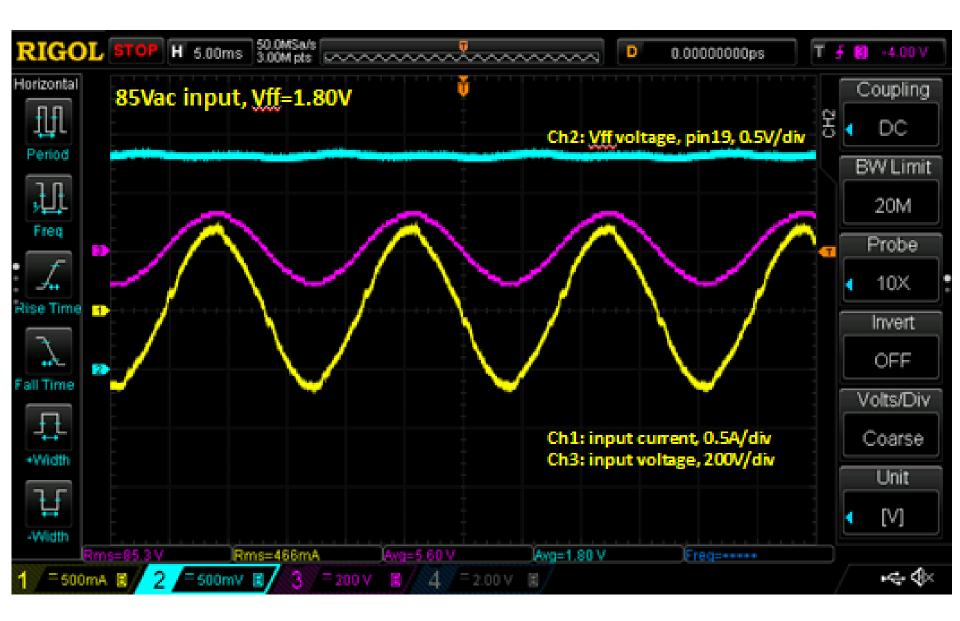
Input voltage ( <u>Vrms</u> )	Vff on pin19 w/ DiffProbe (Vdc)	Vaout on pin1 w/ DVM (Vdc)	0 < i (t) < 500 A
85	1.80	2.000	$0 \le i_{IAC}(t) \le 500 \mu\text{A},$
120	2.56	1.977	$0 \leq V_{VAOUT}(t) \leq 5 V,$
150	3.24	1.967	$1.4 \text{ V} \le \text{V}_{\text{VFF}} \le \text{V}_{\text{VREF}} - 1.4 \text{ V}$
200	4.38	1.933	VFF VICEF
220	4.81	1.900	

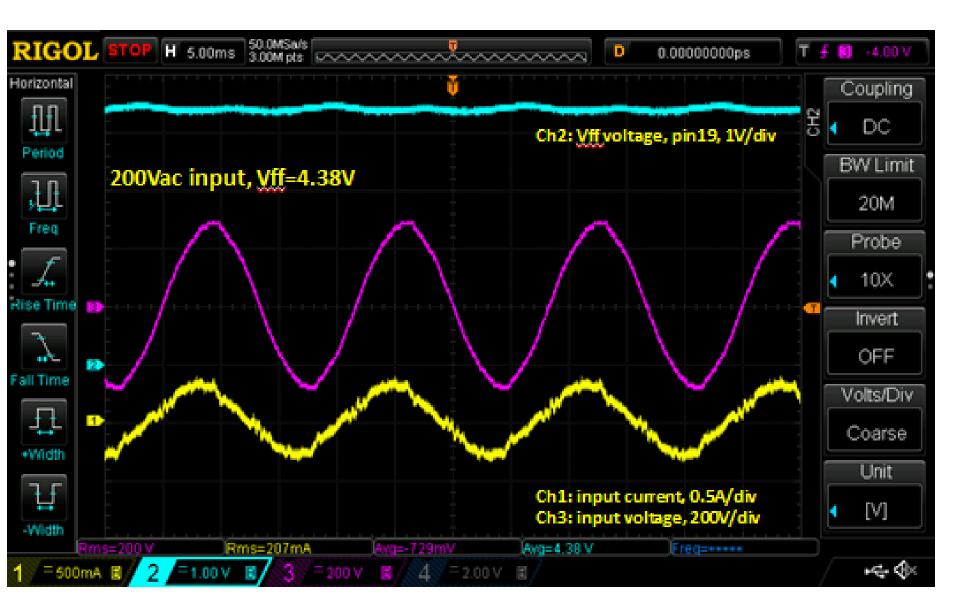


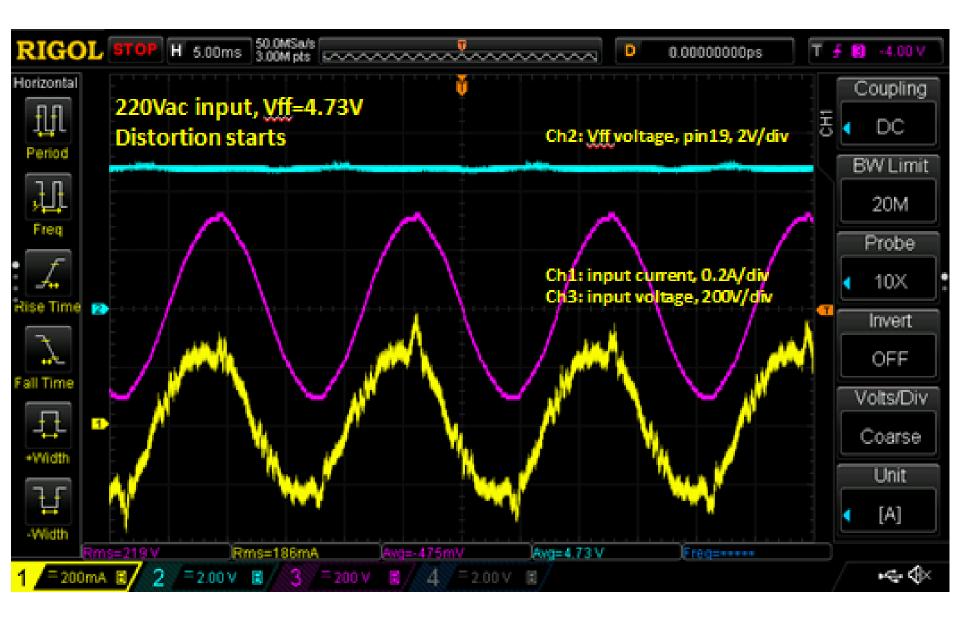
- Vff increases proportionally and <u>Vaout</u> drops inversely as Vac increases.
- Vaout seems to start low at 2V and not varying within its full range of 0-5V

12

65

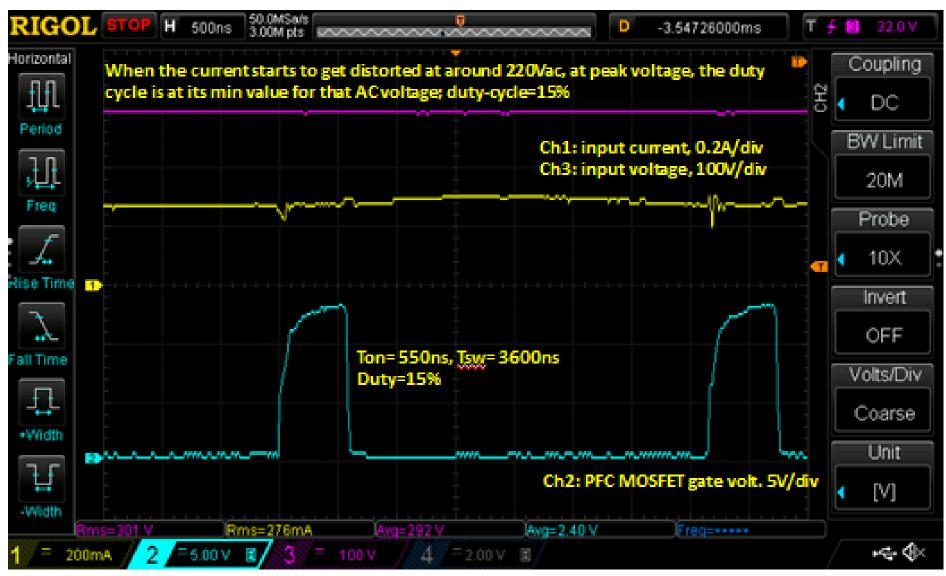






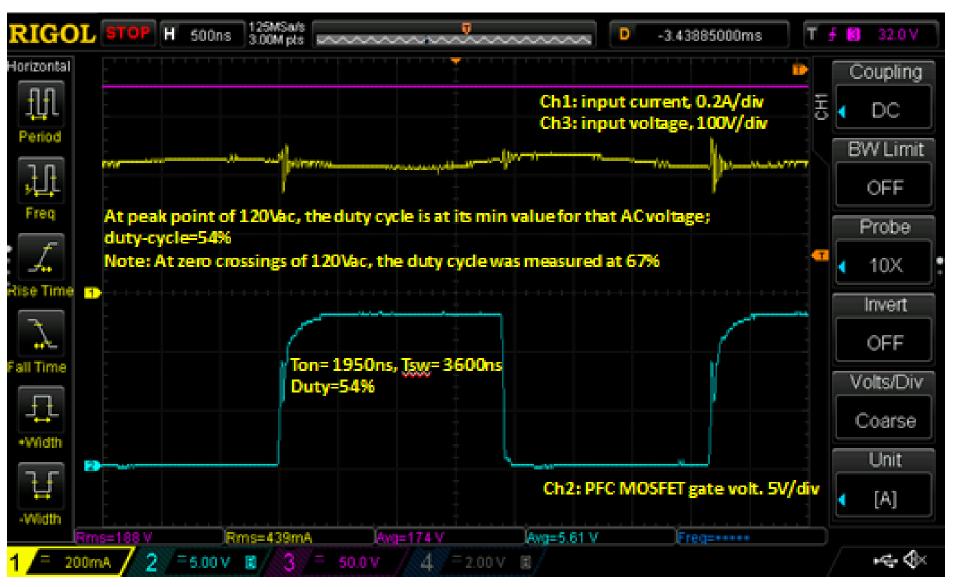
### UCC28513 questions to TI, Alex W., 11/17/2022

At the peak of sinewaves when distortion starts, the duty cycle of boost MOSFET is about 15%



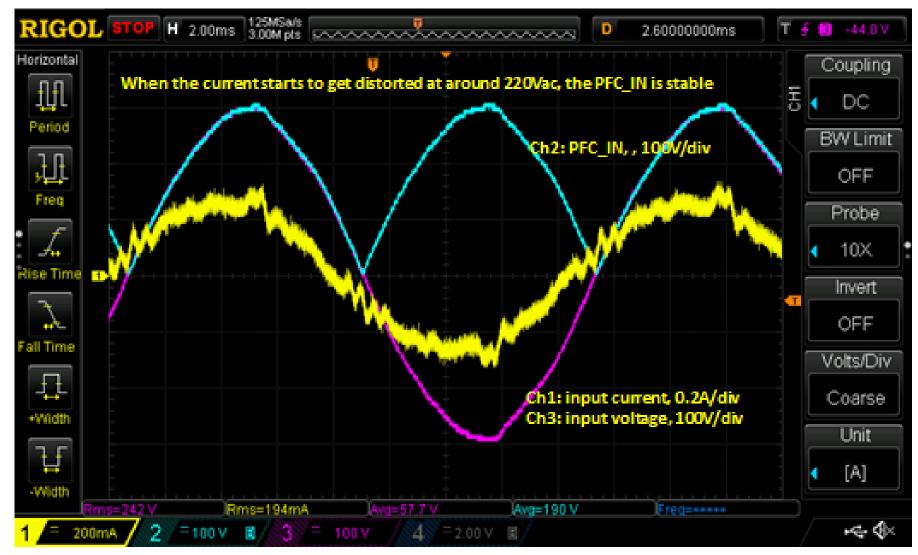
# UCC28513 questions to TI, Alex W., 11/17/2022

#### At the peak of sinewaves at 120Vac, the duty cycle of boost MOSFET is about 54%

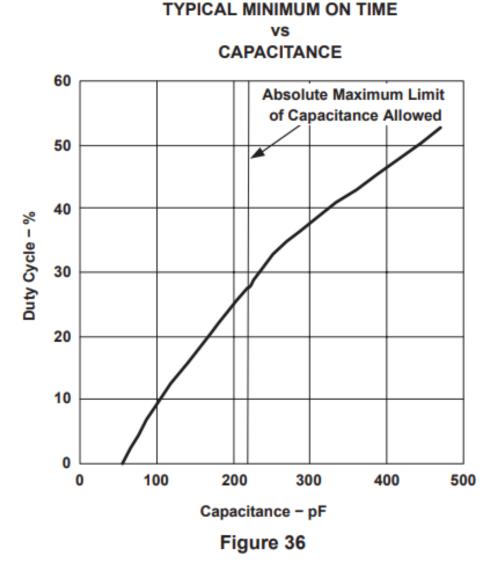


# UCC28513 questions to TI, Alex W., 11/17/2022

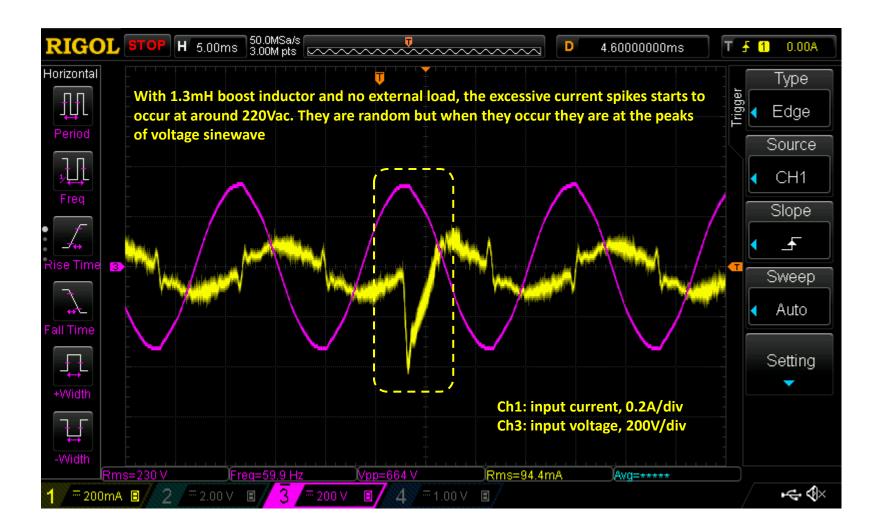
#### At 220Vac when distortions starts, the rectified input voltage (used for Vff) is shown below

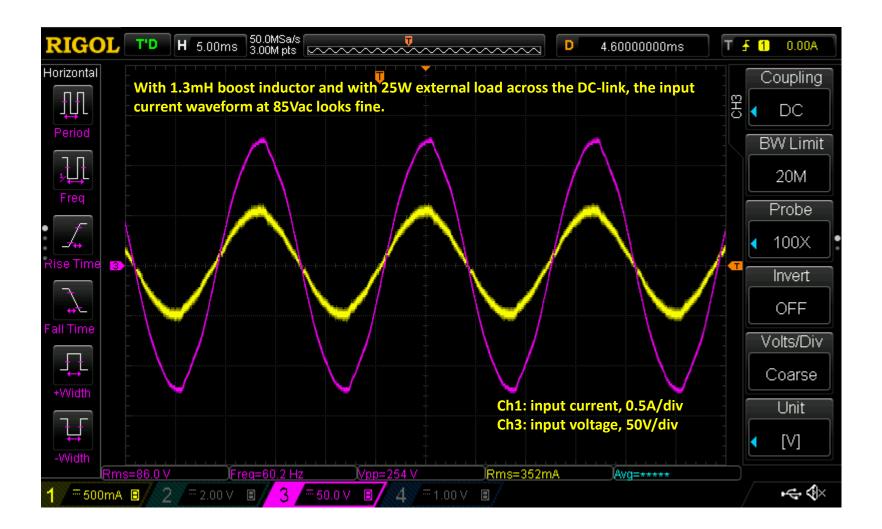


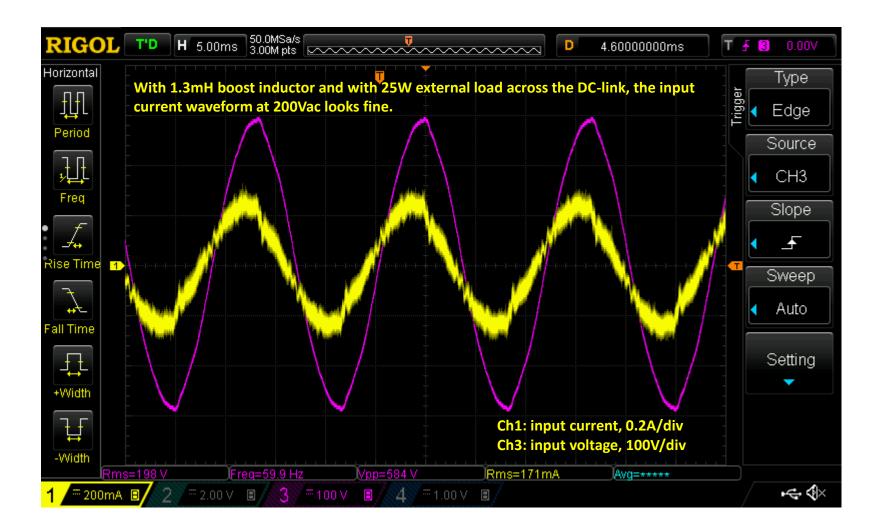
Referring to Fig 36 in the data sheet of UCC28513DW, what specific capacitor controls the min duty cycle?



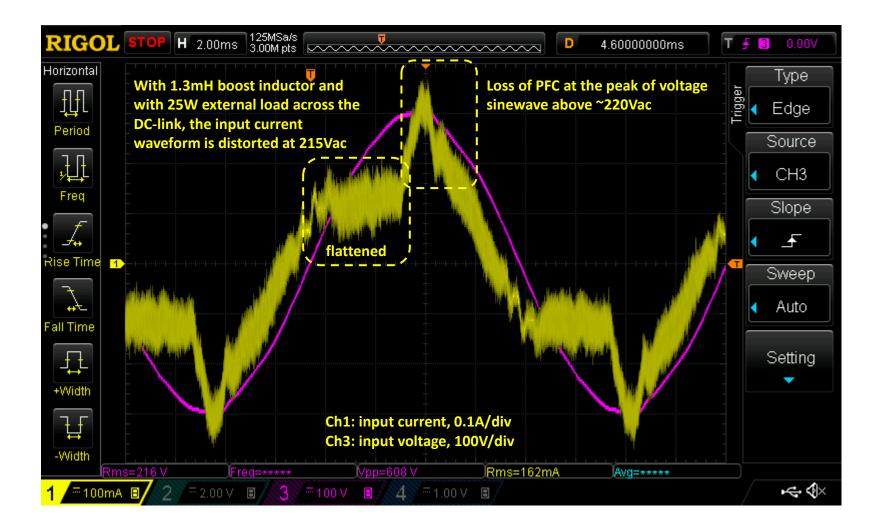
Note: The capacitor on Isense2 affects the min duty cycle on GATE2 output, PFC is on GATE1 output



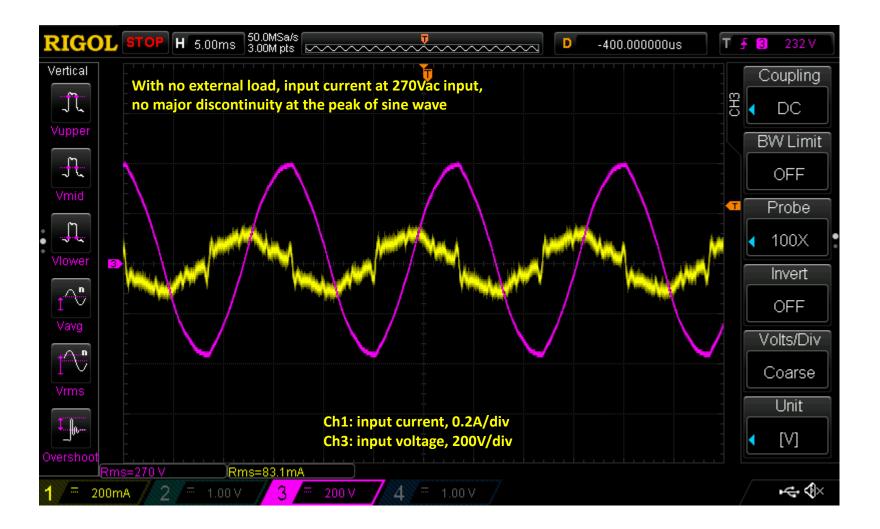


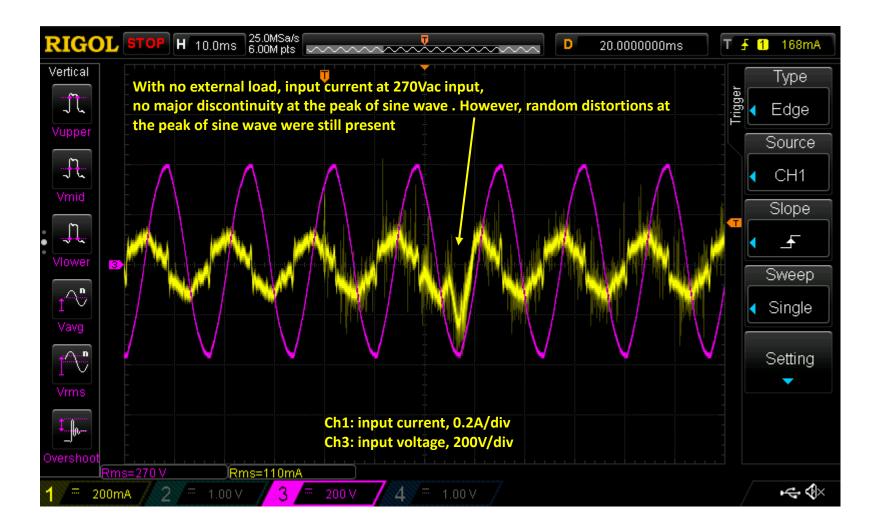


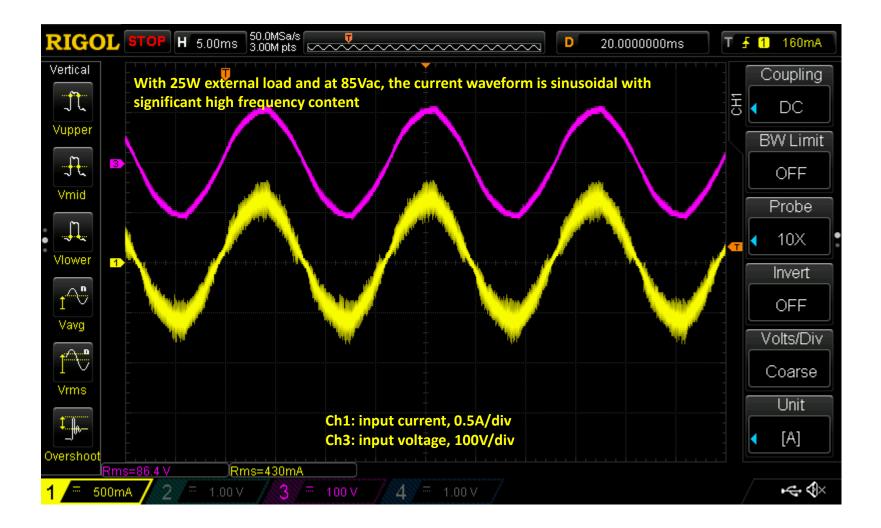


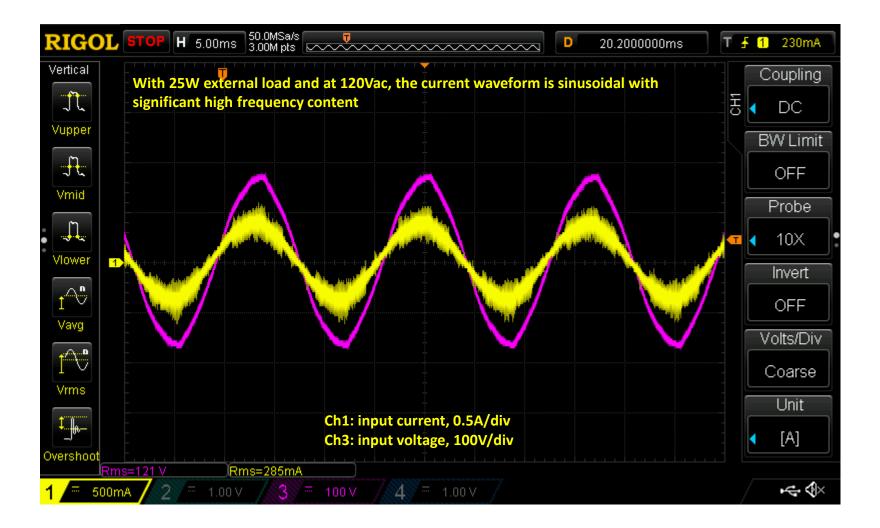


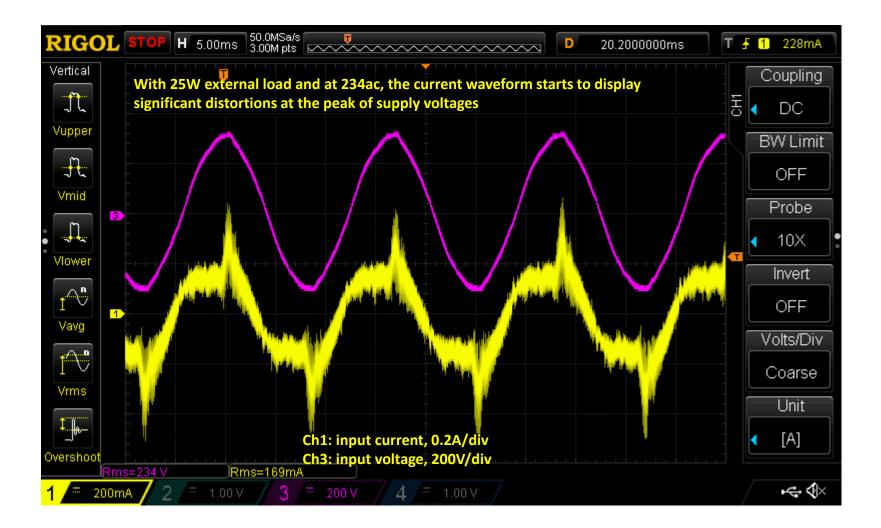
RefDes on data sheet	RefDes in design	values	Values on 12/11/2022	Changes made
R1	R47+R50	766K		on 12/11 are
R2	R43	0.22	0.44	highlighted
R8/R12	R4/R9	3.16K	2.74K	
R3	R44+R49	1124K		
R4	R60	22.1k		
C1	C32	150uF		
L1	L2	660uH		
R13	R10	15.8K	55K (56K//3.3Meg)	Also tried 15.8k
C6	C6	680pF	233pF (200p//33p)	
C7	C8	150pF	33pF	
R15	R11	30.1K		
C8	С9	4.7uF		
C10	C1	1.5uF		
C11	C2	150nF		
R21	R1	48.7K		
R14	R13	10K		
R7	R5	1.18K	1.50K (3.3K//2.74K)	
С9	C4	1uF		25









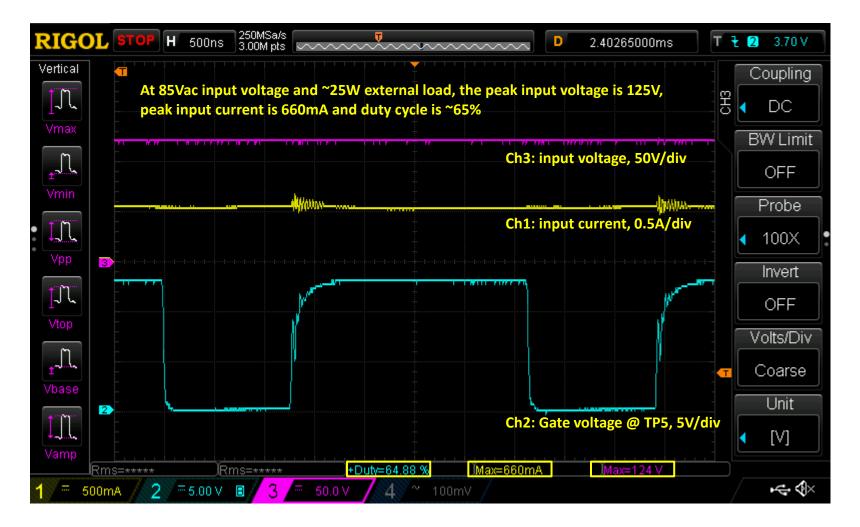


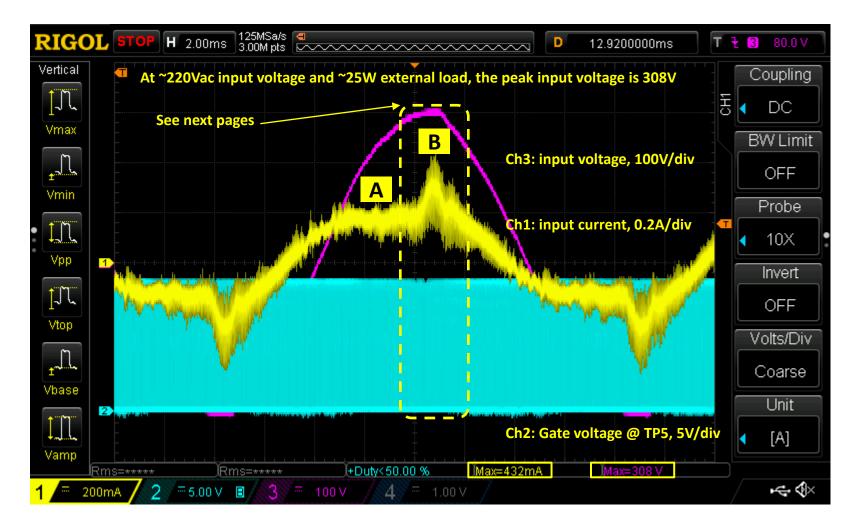
There are only two current probes at the moment:

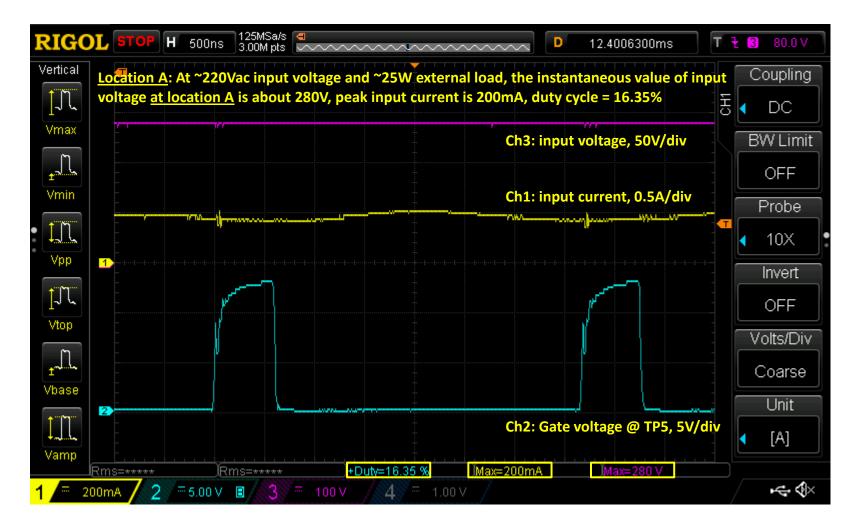
Ch1: Fluke 80i-110S has limited bandwidth and is used to measure 60Hz input current only.

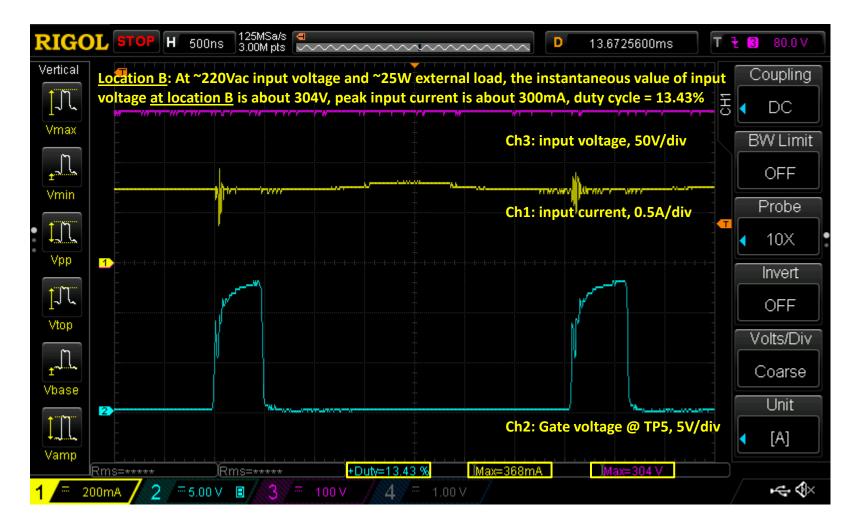
Ch4: Rogowski probe, CWTUM-015-B, is used to measure the high frequency switching ripple only.

In addition, a  $100m\Omega$  and  $20m\Omega$  sense resistor was connected in series with inductor and the voltage across the resistor was measured with a differential probe. However, doing so resulted in further instability and distortion and therefore abandoned.





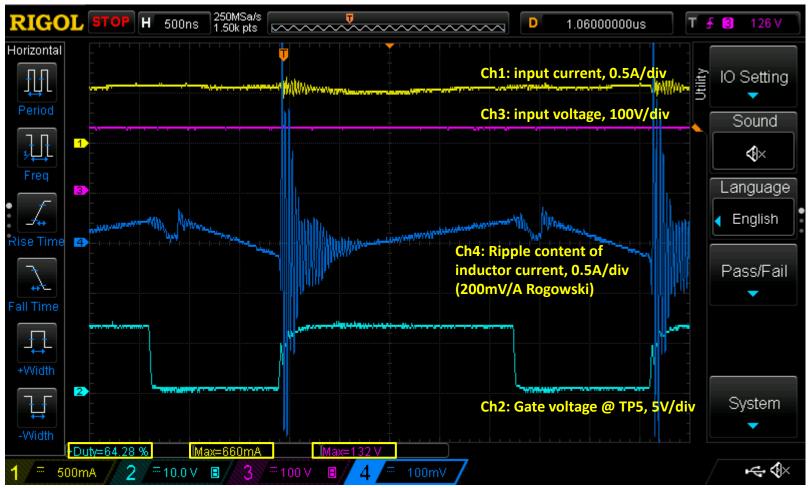




Ch1: Current probe is Fluke 80i-110S, which has limited bandwidth and is used to measure 60Hz input current

Ch4: Current probe is Rogowski CWTUM-015-B, which can measure high frequency only.

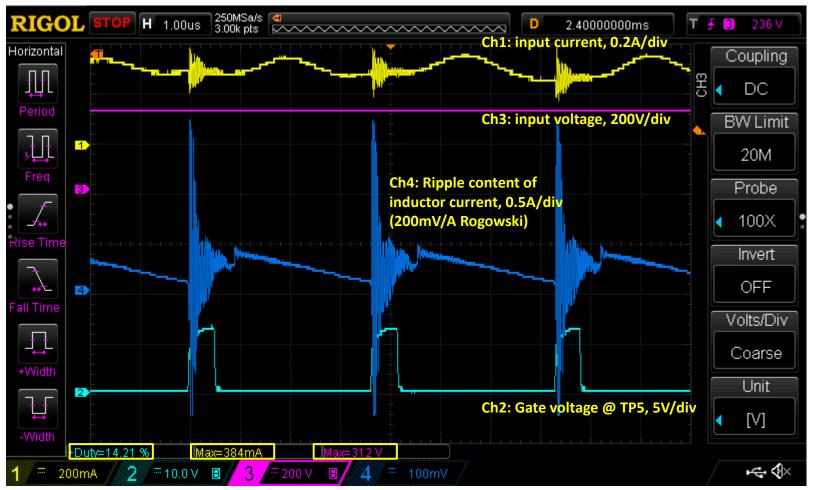
At the peak of 85Vac input voltage and ~25W external load, the instantaneous value of input voltage is 132V, peak input current is 660mA, duty cycle = 64.28%



Ch1: Current probe is Fluke 80i-110S, which has limited bandwidth and is used to measure 60Hz input current

Ch4: Current probe is Rogowski CWTUM-015-B, which can measure high frequency only.

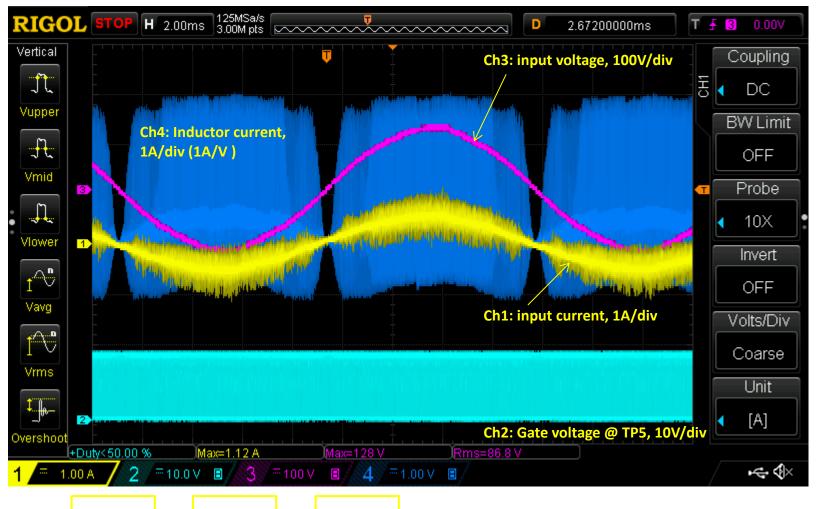
At the peak of 220Vac input voltage and ~25W external load, the instantaneous value of input voltage is 312V, peak input current is ~300mA (location B), duty cycle is about 14.2%



37

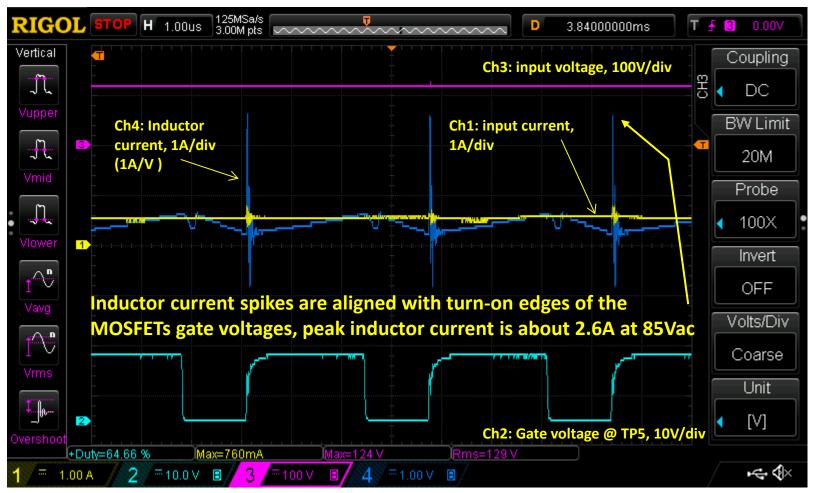
# Measuring inductor current vs gate voltages, 12/25 Ch1: Fluke 80i-110S, which has limited bandwidth Ch4: Tek TCPA300 w/ TCP312 Current probe

At 85Vac input voltage and ~25W external load, no major distortions observed



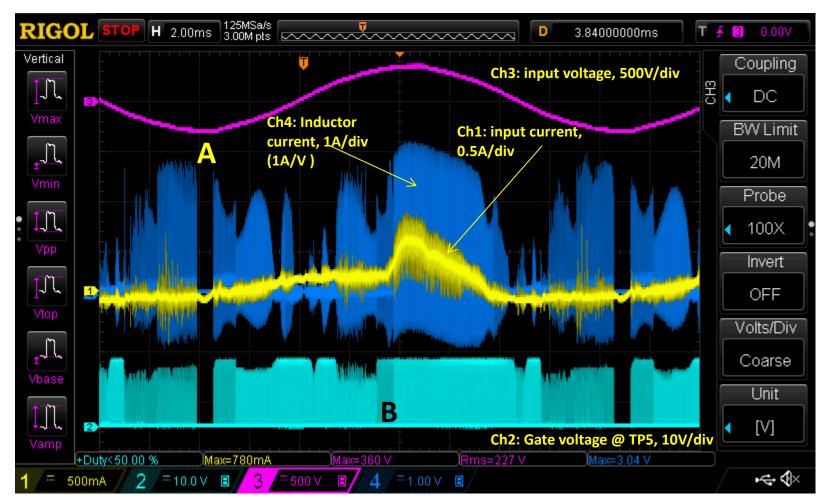
# Measuring inductor current vs gate voltages, 12/25 Ch1: Fluke 80i-110S, which has limited bandwidth Ch4: Tek TCPA300 w/ TCP312 Current probe

At 85Vac input voltage and ~25W external load, no major distortions observed



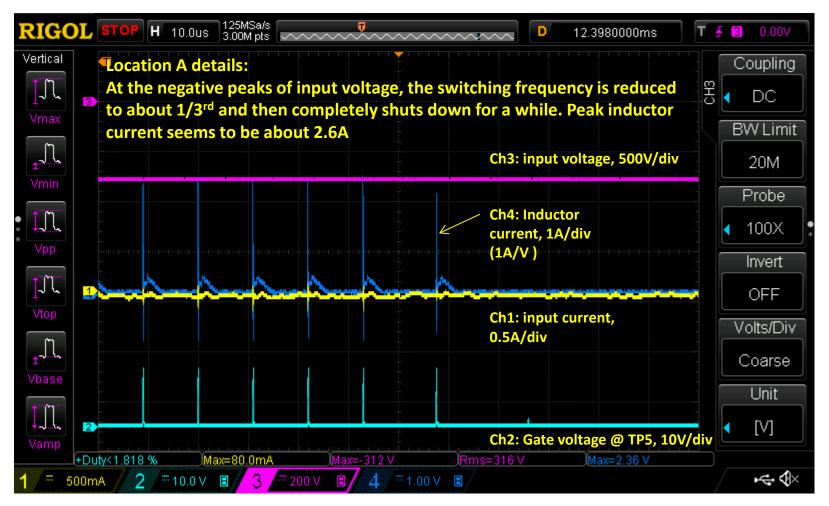
Ch1: Fluke 80i-110S, which has limited bandwidth Ch4: Tek TCPA300 w/ TCP312 Current probe

At ~230Vac input voltage and ~25W external load, distortions observed. See next slides for location A, B details



Ch1: Fluke 80i-110S, which has limited bandwidth Ch4: Tek TCPA300 w/ TCP312 Current probe

At ~230Vac input voltage and ~25W external load, distortions observed.



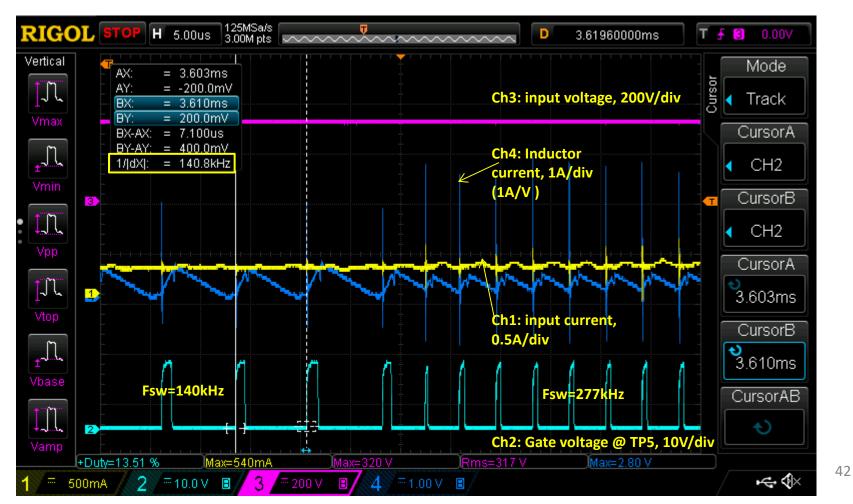
Ch1: Fluke 80i-110S, which has limited bandwidth

Ch4: Tek TCPA300 w/ TCP312 Current probe

At ~230Vac input voltage and ~25W external load, distortions observed.

#### Location B details:

At the positive peaks of input voltage, the switching frequency is reduced to about ½ and this results in "flat top" on the current waveform. After that the switching frequency is raised and around that time the current surge is observed



Ch1: Fluke 80i-110S, which has limited bandwidth

Ch4: Tek TCPA300 w/ TCP312 Current probe

At ~230Vac input voltage and ~25W external load, distortions observed.

#### Location B details:

At the positive peaks of input voltage, the switching frequency is reduced to about ½ and this results in "flat top" on the current waveform. After that the switching frequency is raised and around that time the current surge is observed

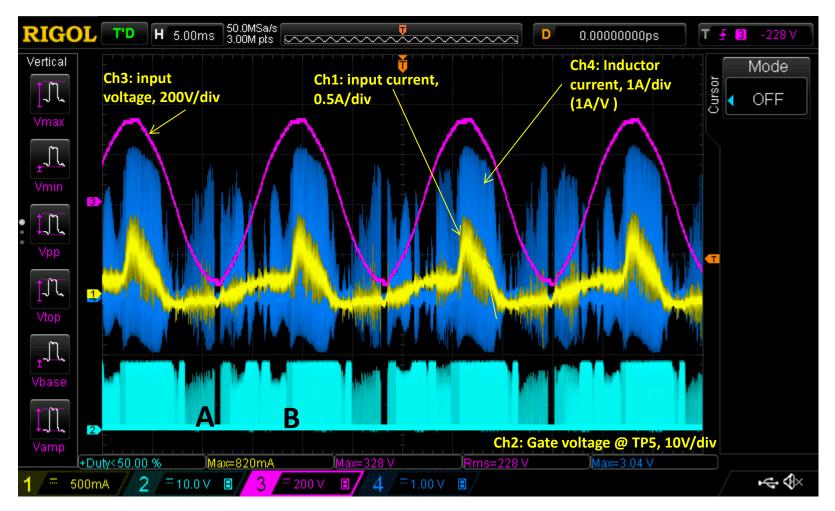


Ch1: Fluke 80i-110S, which has limited bandwidth

Ch4: Tek TCPA300 w/ TCP312 Current probe

At ~230Vac input voltage and ~25W external load, distortions observed.

## At 230Vac input, 25W external load, the view of locations A (negative peak) and location B (positive peak)

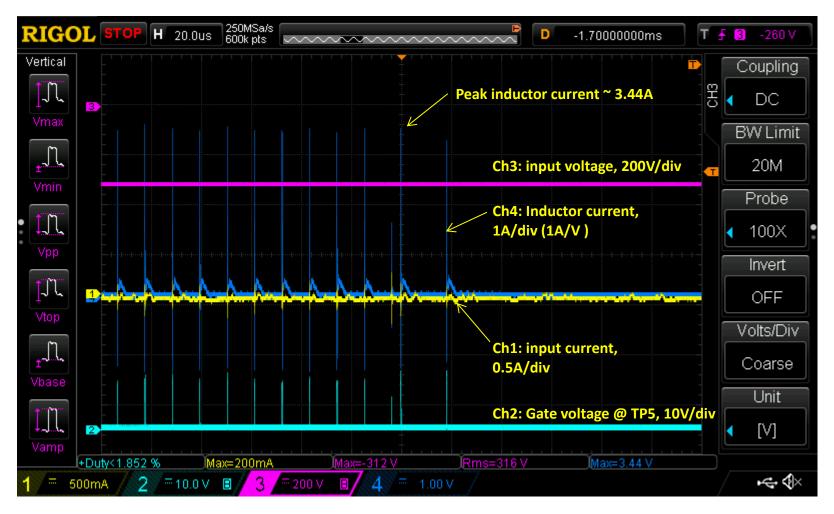


Ch1: Fluke 80i-110S, which has limited bandwidth

Ch4: Tek TCPA300 w/ TCP312 Current probe

At ~230Vac input voltage and ~25W external load, distortions observed.

#### Location A: Current probe on Ch1 has low BW and is used to measure input current only.

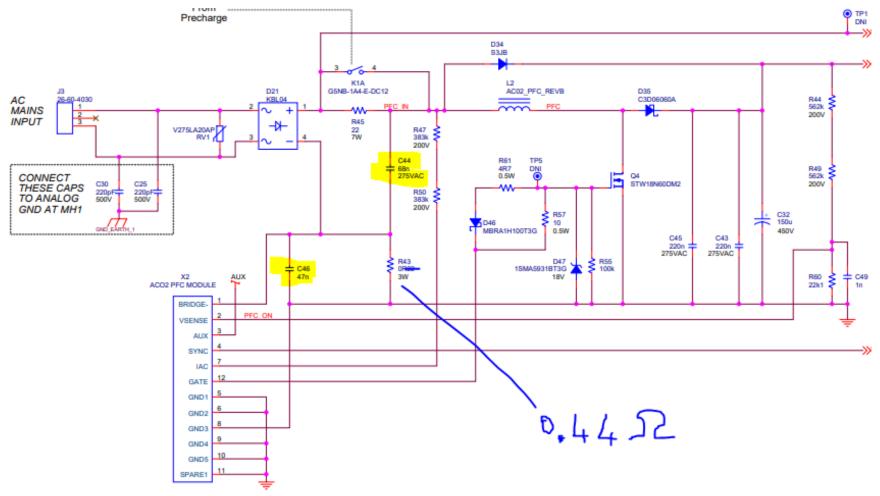


Ch1: Fluke 80i-110S, which has limited bandwidth

Ch4: Tek TCPA300 w/ TCP312 Current probe

At ~230Vac input voltage and ~25W external load, distortions observed.

#### There is a 68nF cap after the rectifier. It is increased to 2x68=136nF, did not observe any improvements

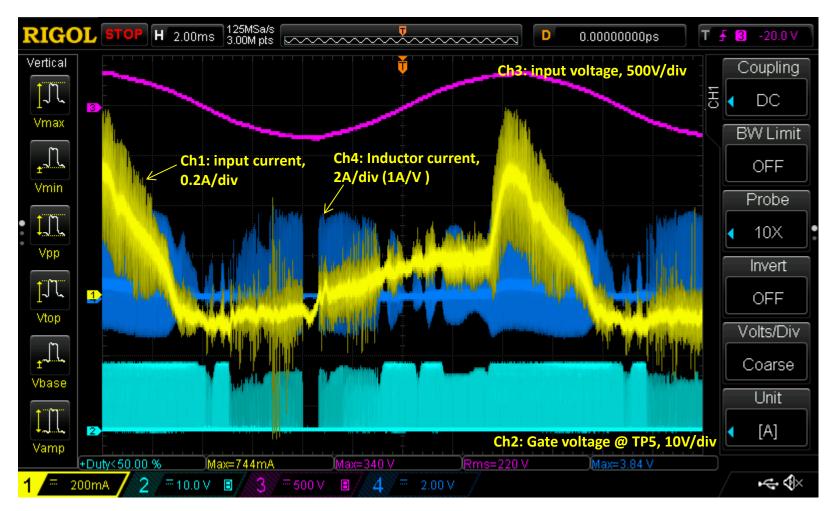


Ch1: Fluke 80i-110S, which has limited bandwidth

Ch4: Tek TCPA300 w/ TCP312 Current probe

At ~230Vac input voltage and ~25W external load, distortions observed.

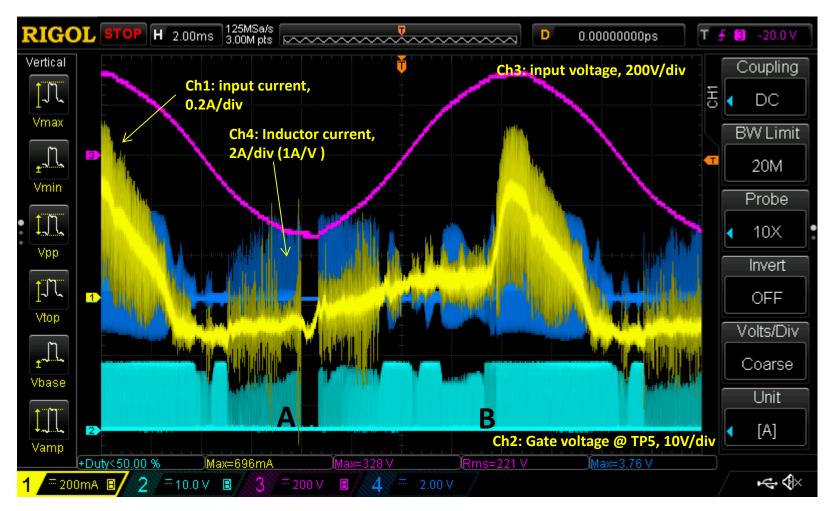
#### There is a 68nF cap after the rectifier. It is increased to 2x68=136nF, did not observe any improvements



Ch1: Fluke 80i-110S, which has limited bandwidth

Ch4: Tek TCPA300 w/ TCP312 Current probe

At ~230Vac input voltage and ~25W external load, distortions observed.



Ch1: Fluke 80i-110S, which has limited bandwidth

Ch4: Tek TCPA300 w/ TCP312 Current probe

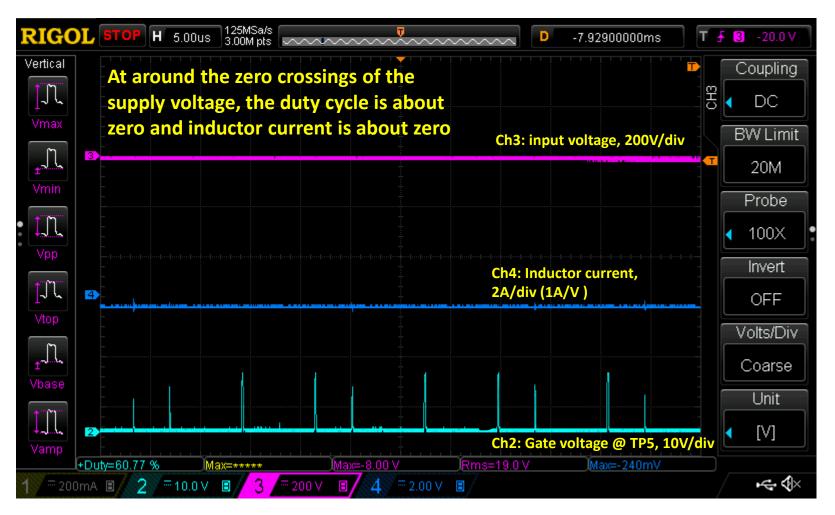
At ~230Vac input voltage and ~25W external load, distortions observed.



Ch1: Fluke 80i-110S, which has limited bandwidth

Ch4: Tek TCPA300 w/ TCP312 Current probe

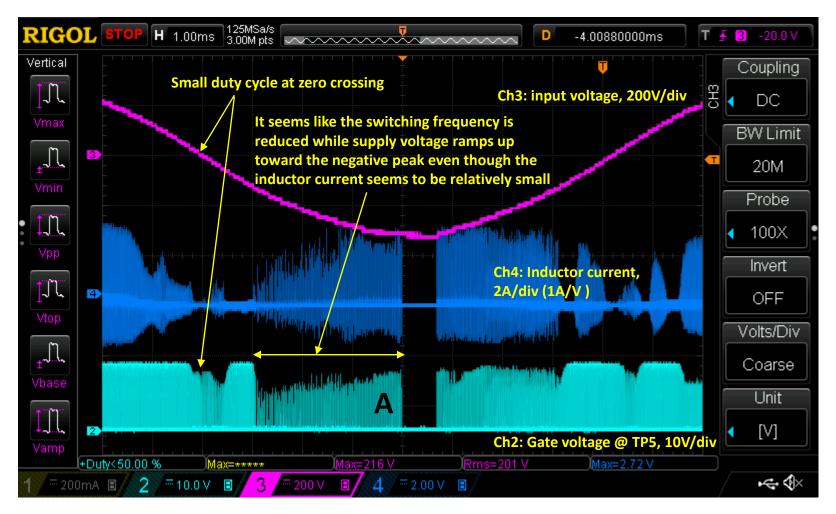
At ~230Vac input voltage and ~25W external load, distortions observed.



Ch1: Fluke 80i-110S, which has limited bandwidth

Ch4: Tek TCPA300 w/ TCP312 Current probe

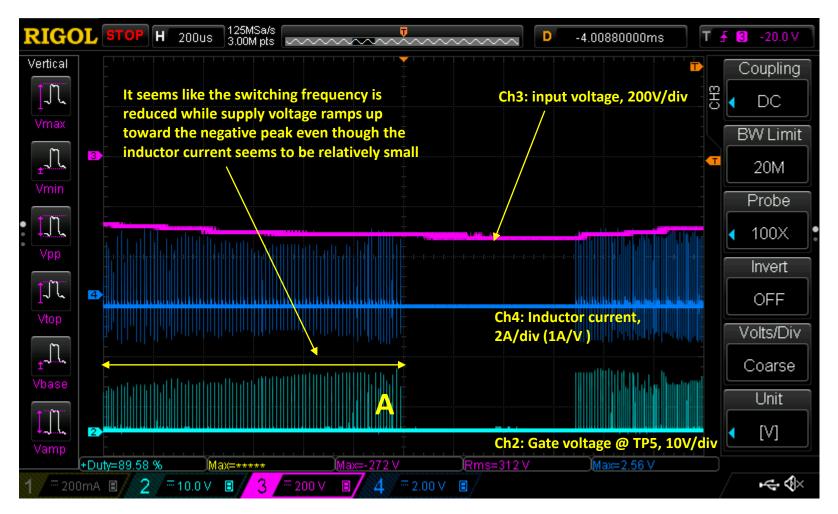
At ~230Vac input voltage and ~25W external load, distortions observed.



Ch1: Fluke 80i-110S, which has limited bandwidth

Ch4: Tek TCPA300 w/ TCP312 Current probe

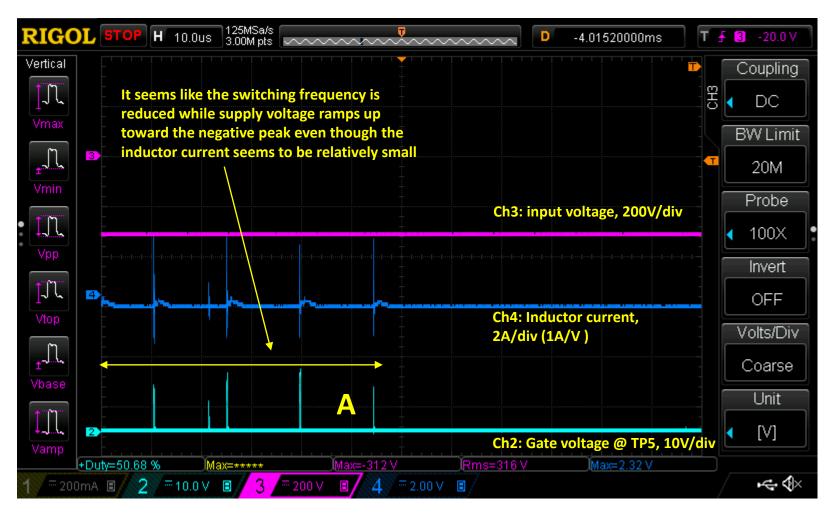
At ~230Vac input voltage and ~25W external load, distortions observed.



Ch1: Fluke 80i-110S, which has limited bandwidth

Ch4: Tek TCPA300 w/ TCP312 Current probe

At ~230Vac input voltage and ~25W external load, distortions observed.



Ch1: Fluke 80i-110S, which has limited bandwidth Ch4: Tek TCPA300 w/ TCP312 Current probe At ~230Vac input voltage and ~25W external load, distortions observed.

# **Observations:**

- 1) Location A: While the supply voltage ramps up toward the negative peak, the switching frequency is reduced significantly and then MOSFET shuts down for a while at the negative peak. It seems like the inductor current is relatively small and this may not be current limit initiated turn off.
- 2) Location B: While the supply voltage ramps up toward the positive peak, the switching frequency is reduced by about 50%. It is observed this corresponds to "flat top" on supply current. At around the peak of supply voltage, the switching frequency suddenly snaps back to normal frequency and this corresponds to surge in peak of the supply voltage. It is not clear if this phenomenon is caused by activation of current limit.
- 3) Adding an other 68nF cap after rectifier did not improve the issue
- 4) Adding 100nF cap across R5 (R7 on data sheet) did not improve the issue

РСВ	RefDes on datasheet	RefDes in design	12/11/2022 Fci=44kHz, Gci=5.6	12/25/2022 Fci=11kHz, Gci=1.6
PSB- 04	R1	R47, R50	383K	383K
	R2	R43	0.44	0.44
	L1	L2	660uH	660uH
PFC- 03	R8, R12	R4, R9	2.74K	2.74К
	R13	R10	15.8K	4.7K
	C6	C6	233pF (200p//33p)	3.3n
	С7	C8	33pF	150pF
	R15	R11	30.1K	30.1K
	C8	С9	4.7uF	4.7uF
	C10	C1	1.5uF	1.5uF
	C11	C2	150nF	150nF
	R21	R1	48.7K	48.7K
	R14	R13	10K	10К
	R7	R5	1.50K (3.3K//2.74K) +100pF	1.50K (3.3K//2.74K <b>) + 100pF</b>
	С9	C4	1uF	1uF

55

Ch1: Fluke 80i-110S, which has limited bandwidth

Ch4: Tek TCPA300 w/ TCP312 Current probe

Per changes listed on page 55

At ~85Vac input voltage and ~25W external load, no major distortions observed

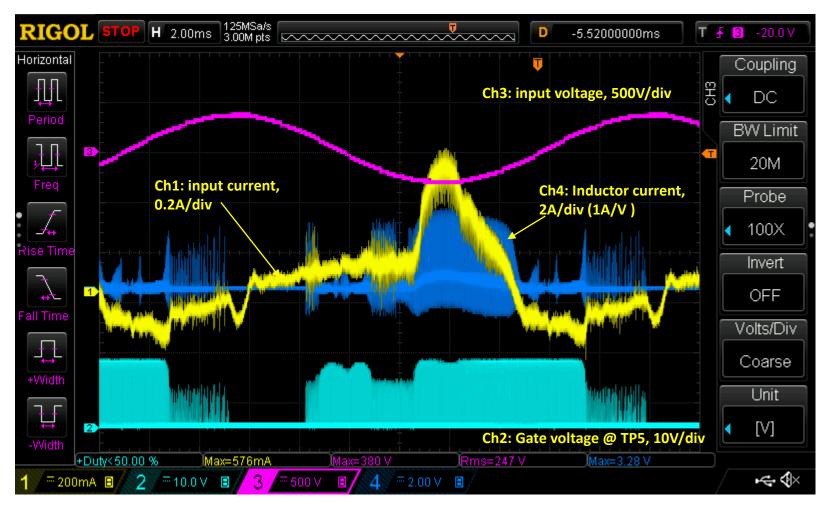


Ch1: Fluke 80i-110S, which has limited bandwidth

Ch4: Tek TCPA300 w/ TCP312 Current probe

Per changes listed on page 55

At ~230Vac input voltage and ~25W external load, major distortions observed

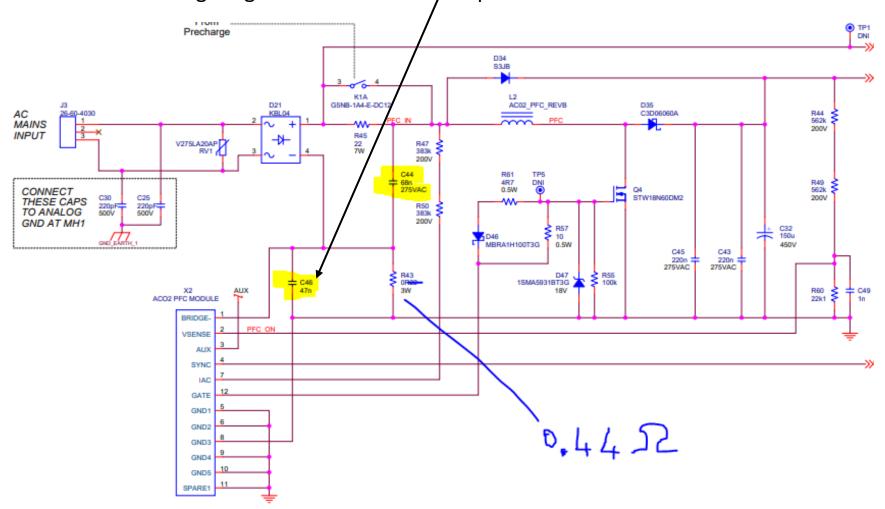


Ch1: Fluke 80i-110S, which has limited bandwidth

Ch4: Tek TCPA300 w/ TCP312 Current probe

Per changes listed on page 55

At ~230Vac input voltage and ~25W external load, major distortions observed Investigating the effect of C46 on input current distortions

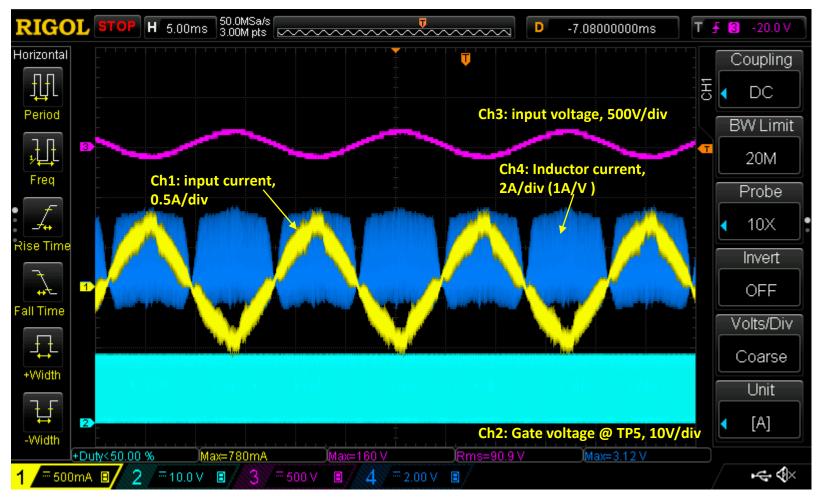


Ch1: Fluke 80i-110S, which has limited bandwidth

Ch4: Tek TCPA300 w/ TCP312 Current probe

Per changes listed on page 55

At 90Vac input voltage, <u>no C46</u>, no major distortions observed Ch4: Tek TCPA300, Ch1: Fluke 80i-110S

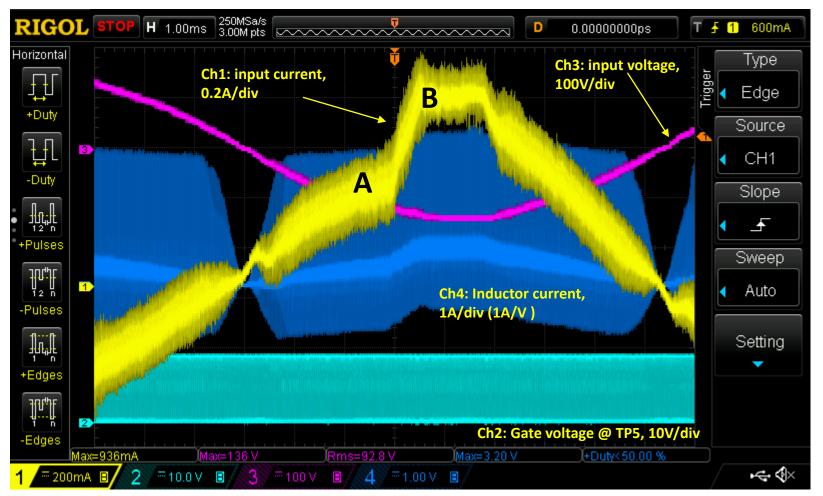


Ch1: Fluke 80i-110S, which has limited bandwidth

Ch4: Tek TCPA300 w/ TCP312 Current probe

Per changes listed on page 55

At ~100Vac input voltage, <u>no C46</u>, distortions started, notice the current surge from location A to B Ch4: Tek TCPA300, Ch1: Fluke 80i-110S

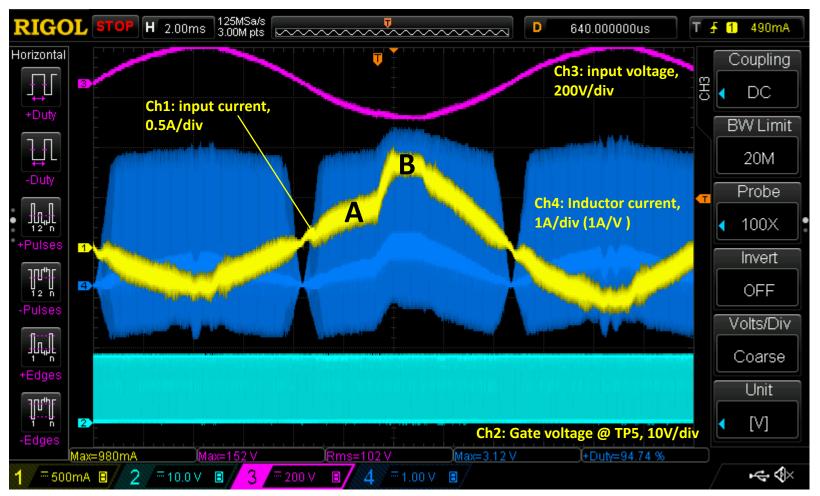


Ch1: Fluke 80i-110S, which has limited bandwidth

Ch4: Tek TCPA300 w/ TCP312 Current probe

Per changes listed on page 55

At ~100Vac input voltage, <u>no C46</u>, distortions started Ch4: Tek TCPA300, Ch1: Fluke 80i-110S

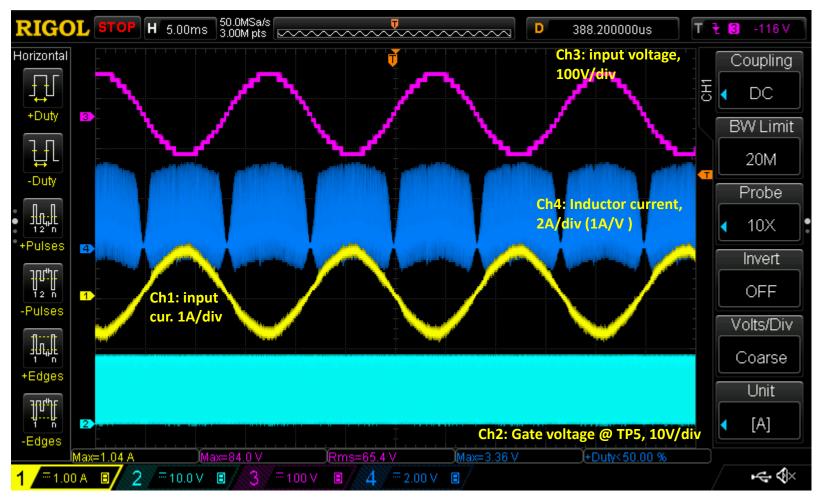


Ch1: Fluke 80i-110S, which has limited bandwidth

Ch4: Tek TCPA300 w/ TCP312 Current probe

Per changes listed on page 55

At ~85Vac input voltage, <u>C46=100nF</u>, no major distortions Ch4: Tek TCPA300, Ch1: Fluke 80i-110S

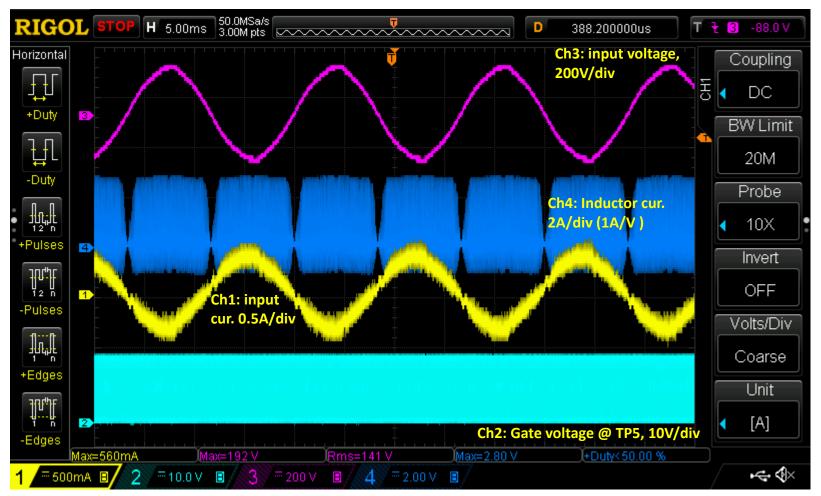


Ch1: Fluke 80i-110S, which has limited bandwidth

Ch4: Tek TCPA300 w/ TCP312 Current probe

Per changes listed on page 55

At ~140Vac input voltage, <u>C46=100nF</u>, no major distortions Ch4: Tek TCPA300, Ch1: Fluke 80i-110S

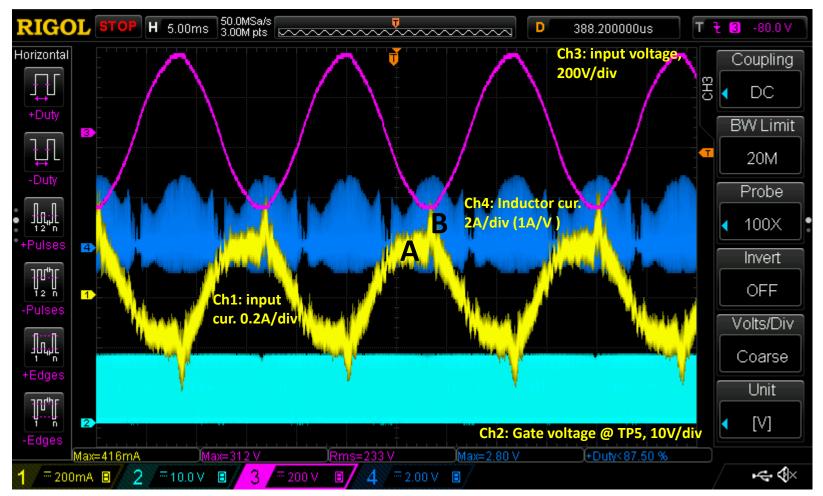


Ch1: Fluke 80i-110S, which has limited bandwidth

Ch4: Tek TCPA300 w/ TCP312 Current probe

Per changes listed on page 55

At ~230Vac input voltage, <u>C46=100nF</u>, symmetric distortions show up on peaks of voltage waveform Ch4: Tek TCPA300, Ch1: Fluke 80i-110S

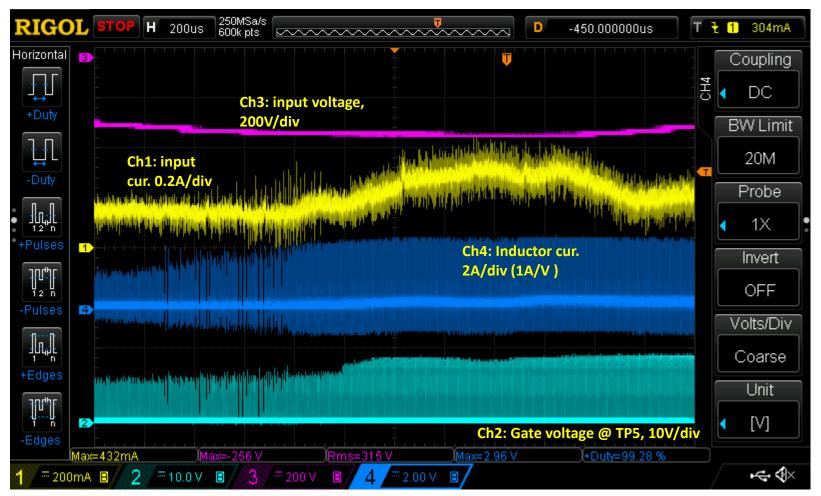


Ch1: Fluke 80i-110S, which has limited bandwidth

Ch4: Tek TCPA300 w/ TCP312 Current probe

Per changes listed on page 55

At ~230Vac input voltage, <u>C46=100nF</u>, location A; ON times gets very small & pulses start to drop Ch4: Tek TCPA300, Ch1: Fluke 80i-110S



Ch1: Fluke 80i-110S, which has limited bandwidth

Ch4: Tek TCPA300 w/ TCP312 Current probe

Per changes listed on page 55

At ~230Vac input voltage, <u>C46=100nF</u>, location A; ON times gets very small & pulses start to drop Ch4: Tek TCPA300, Ch1: Fluke 80i-110S



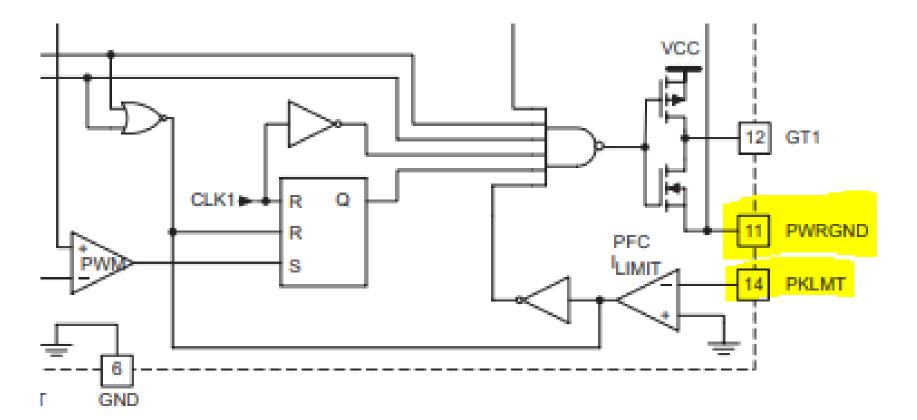
Measuring inductor current vs gate voltages, 12/28 Ch1: Fluke 80i-110S, which has limited bandwidth Ch4: Tek TCPA300 w/ TCP312 Current probe Per changes listed on page 55

#### Conclusions on 12/28:

- 1) Removing the 47nF cap across the sense resistor made the issue worse that the current became more unstable and distortions started even at low voltages of ~100Vac
- 2) Replacing the capacitor across the sense resistor (C46) with 100nF, did not improve the problem that the current waveform was stable up to ~ 230Vac and distortions started above this voltage, as it was the case with C46=47nF
- 3) Referring to location A; it appears that the duty cycle gets very small and even some pulses were dropped even though the current through the inductor does not appear to be the max. This suggests that the event is not initiated by peak current limit
- 4) Referring to location B; at this point no pulse dropping is observed. On the contrary, the duty-cycle increases which results in surge in inductor current.

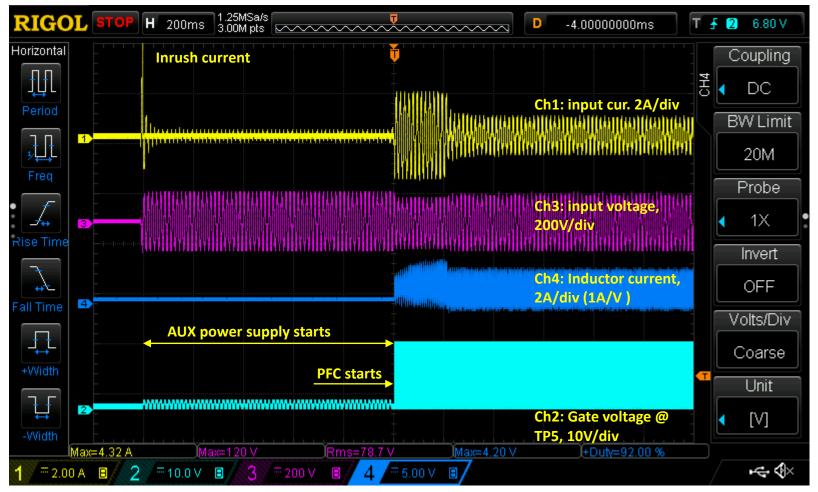
Measuring inductor current vs gate voltages, 1/8/2023 Ch1: Fluke 80i-110S, which has limited bandwidth Ch4: Tek TCPA300 w/ TCP312 Current probe Per changes listed on page 55, 100pF cap removed from R5

100pF leaded ceramic capacitor was connected from pin14 (PKLMT) to pin11 (PWRGND). No improve observed After that, a 1nF capacitor was added from pin14 to pin11, and again no improvements were observed



Measuring inductor current vs gate voltages, 1/8/2023 Ch1: Fluke 80i-110S, which has limited bandwidth Ch4: Tek TCPA300 w/ TCP312 Current probe Per changes listed on page 55, 100pF cap removed from R5

#### Start-up timing of PFC stage



Ch1: Fluke 80i-110S, which has limited bandwidth

Ch4: Tek TCPA300 w/ TCP312 Current probe

Per changes listed on page 55, 100pF cap removed from R5

At the time when PFC stage starts operating, it seems like the ON time pulse-width starts from zero and increases slowly



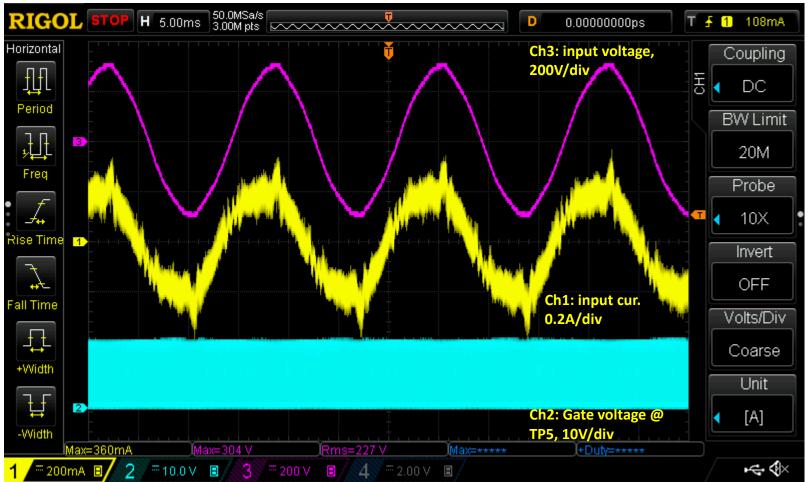
Measuring inductor current vs gate voltages, 1/8/2023 Ch1: Fluke 80i-110S, which has limited bandwidth Ch4: Tek TCPA300 w/ TCP312 Current probe Per changes listed on page 55, 100pF cap removed from R5

#### STOP H 5.00ms 3.00M pts RIGOL D T 🛃 2 7.80 V 6.20000000us Horizontal Ch3: input voltage, Coupling 100V/div ſĮſ CH1 DC Period **BW Limit** <u>, l</u>l 20M Freq Probe Ch1: input cur. 1A/div ⅎ 10X Rise Time Invert OFF ++ Fall Time Ch4: Inductor current, Volts/Div 2A/div (1A/V) £ Coarse +Width Unit Ch2: Gate voltage @ [A] TP5, 10V/div -Width Max=124 V +Duty<77.78 % Max=760mA Rms=83.3 V Max=3.12 V •€• ∜× 2 ≖1.00 A 🔳 = 10.0 V 🗉 🖉 🗧 100 V 🗉 🎊 4 = 2.00 V 🔳

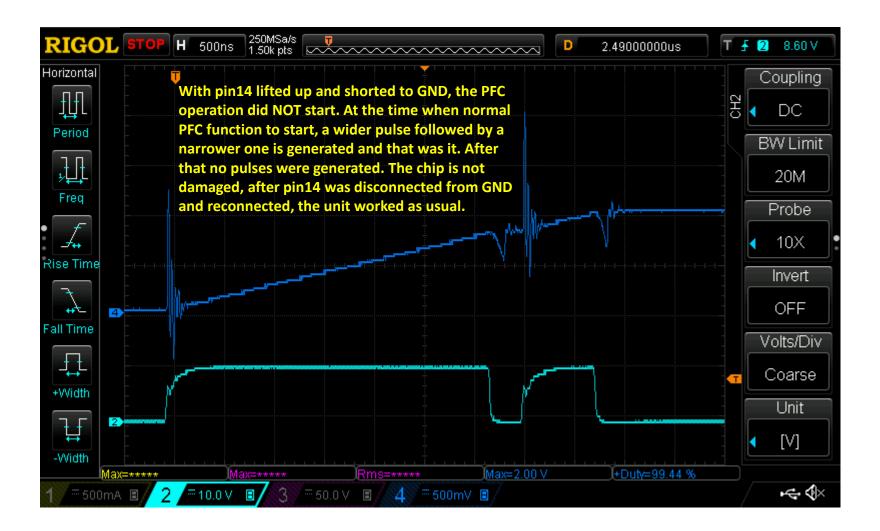
#### With 1nF from PKLMT (pin14) to GND (pin11), no major distortions at 85Vac

Measuring inductor current vs gate voltages, 1/8/2023 Ch1: Fluke 80i-110S, which has limited bandwidth Ch4: Tek TCPA300 w/ TCP312 Current probe Per changes listed on page 55, 100pF cap removed from R5

With 1nF from PKLMT (pin14) to GND (pin11), distortions start at around 220Vac (also tried 100pF from pin14 to pin11, no improvements were observed)



Measuring inductor current vs gate voltages, 1/8/2023 Ch1: Fluke 80i-110S, which has limited bandwidth Ch4: Tek TCPA300 w/ TCP312 Current probe Per changes listed on page 55, 100pF cap removed from R5



Measuring inductor current vs gate voltages, 1/8/2023 Ch1: Fluke 80i-110S, which has limited bandwidth Ch4: Tek TCPA300 w/ TCP312 Current probe Per changes listed on page 55, 100pF cap removed from R5 **Conclusions on 1/8**:

- Connecting 100pF and then 1nF capacitor from pin14 (PKLMT) and pin11 (GND), right on the control chip, did not result in any improvements and that input current started to get distorted at around 230Vac
- 2) When PFC chip starts to operate, after AUX power supply is established, it seems like the ON time of the MOSFET starts from zero and is increased slowly. This makes sense, as doing so would reduce the chance of triggering PKLMT while DC-link cap is charged.
- 3) When pin14 is lifted up and shorted to pin11, at the time when it normally starts, the PFC chip generated a wider single pulse followed by a narrower one. The PFC chip did not go through the normal ramp up sequence. It is not clear why shorting the PKLMT to GND disables the ramp up function. And, since PKLMT is shorted to GND, it is presumed that the interruption of PFC function is not due to activation of PKLMT function.

**SS2 (pin 13):** A capacitor between SS2 and GND programs the softstart duration of the PWM stage gate drive. When the UVLO2 comparator enables the PWM stage, an internal 10.5-μA current source charges the external capacitor at SS2 to 3 V to ramp the voltage at VERR during startup. This allows the GT2 duty cycle to increase from 0% to the maximum clamped by the duty cycle comparator over a controlled time delay t<sub>SS</sub> given by:

 $C_{SS2} = \frac{t_{SS} \times 10.5 \times 10^{-6} \times Amp}{3 \text{ V}}$ 

#### C<sub>SS2</sub> is in Farads

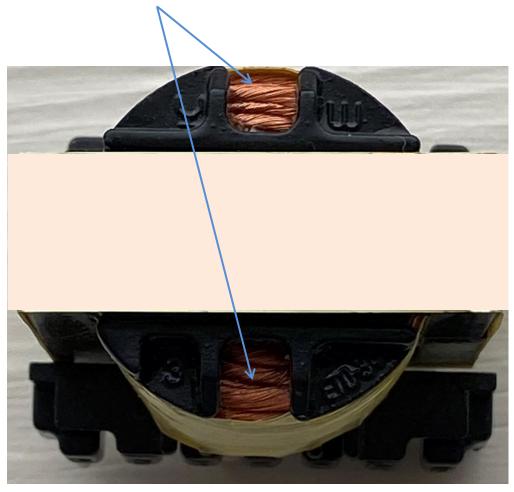
In the event of a disable command or a UVLO2 dropout, SS2 quickly discharges to ground to disable the PWM stage gate drive.

**CAOUT (Pin 15):** This is the output of a wide-bandwidth operational amplifier that senses line current and commands the PFC stage PWM comparator to force the correct duty cycle. This output can swing close to GND to command maximum duty cycle, and above the PFC ramp peak voltage to force zero duty cycle when necessary. Connect current loop compensation components between CAOUT and MOUT.

Measuring inductor current vs gate voltages, 1/15/2023 Ch1: Fluke 80i-110S, which has limited bandwidth Ch4: Tek TCPA300 w/ TCP312 Current probe Per changes listed on page 55, 100pF cap removed from R5

Trying out with PFC boost inductors that are built by using toroid cores with no overlapping windings

**Original PFC inductor has overlapping layers of winding** 

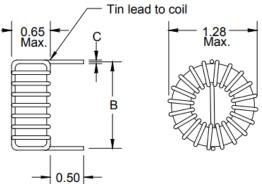


Measuring inductor current vs gate voltages, 1/15/2023 Ch1: Fluke 80i-110S, which has limited bandwidth Ch4: Tek TCPA300 w/ TCP312 Current probe Per changes listed on page 55, 100pF cap removed from R5

Trying out with PFC boost inductors that are built by using toroid cores with no overlapping windings



**Inductor #1**: Bourns PN: 2300LL-681-H-RC, 680uH Built by using toroid core, single layer winding. However, some amount of winding overlapping is visible.





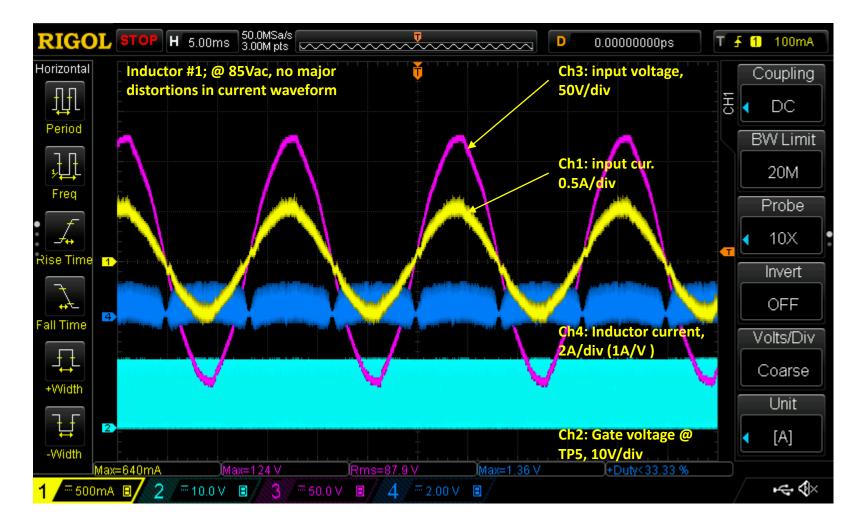
**Inductor #2**: Homemade by using toroid core Wurth PN: 7427015 and 43 turns of single layer winding.

Inductance measured at 1.39mH @ 300kHz.

Ch1: Fluke 80i-110S, which has limited bandwidth

Ch4: Tek TCPA300 w/ TCP312 Current probe

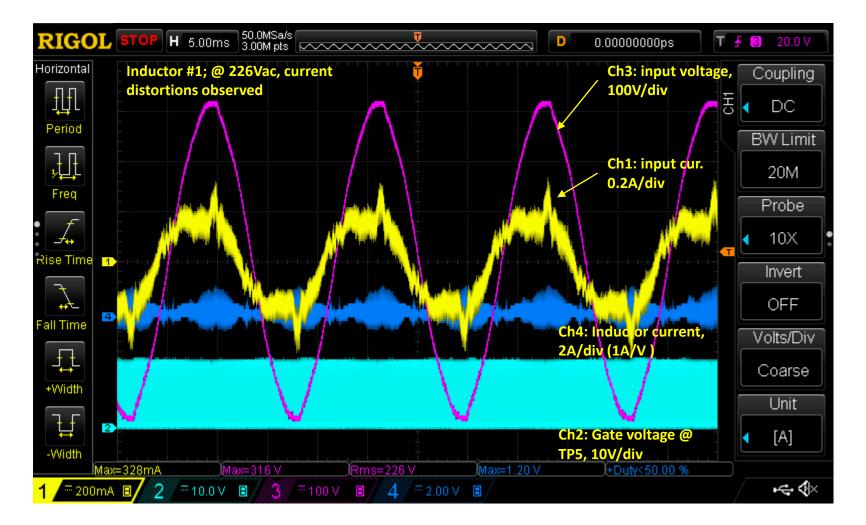
Per changes listed on page 55, 100pF cap removed from R5



Ch1: Fluke 80i-110S, which has limited bandwidth

Ch4: Tek TCPA300 w/ TCP312 Current probe

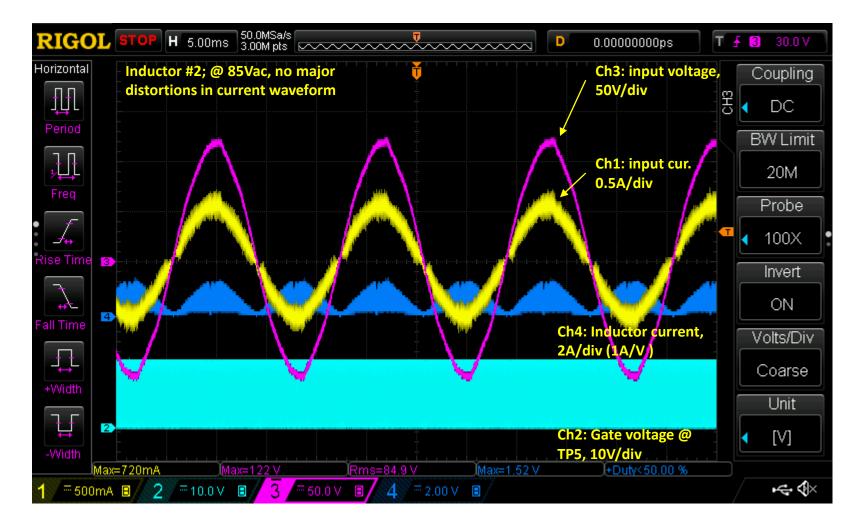
Per changes listed on page 55, 100pF cap removed from R5



Ch1: Fluke 80i-110S, which has limited bandwidth

Ch4: Tek TCPA300 w/ TCP312 Current probe

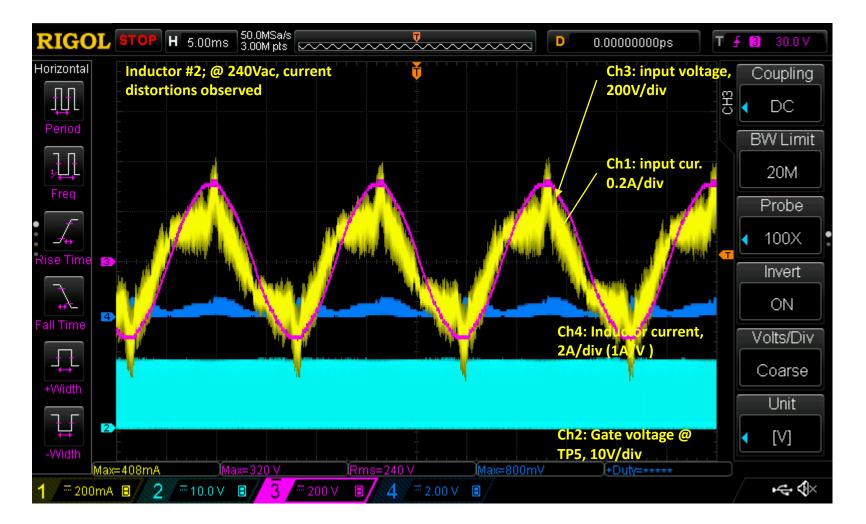
Per changes listed on page 55, 100pF cap removed from R5



Ch1: Fluke 80i-110S, which has limited bandwidth

Ch4: Tek TCPA300 w/ TCP312 Current probe

Per changes listed on page 55, 100pF cap removed from R5



Measuring inductor current vs gate voltages, 1/15/2023 Ch1: Fluke 80i-110S, which has limited bandwidth Ch4: Tek TCPA300 w/ TCP312 Current probe Per changes listed on page 55, 100pF cap removed from R5

Trying out with PFC boost inductors that are built by using toroid cores with no overlapping windings

### Conclusions on 1/15:

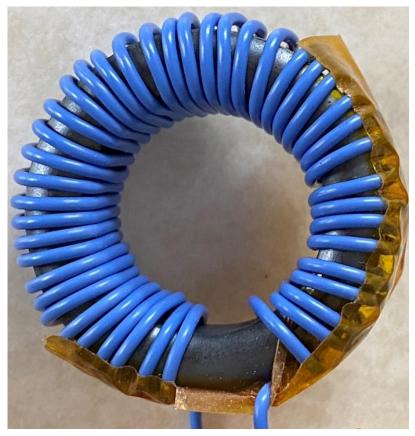
- 1) Two different inductors with no or minimal winding overlapping are tried out. Current distortions at high voltages were observe in both case.
- 2) Original inductor has overlapping windings and new ones do not. Even though the winding to winding capacitance is not measured, it is assumed that a single layer toroid inductor would result in lowest inter-winding capacitance.
- 3) Is there any practical way to measure the inter-winding capacitance?
- 4) Is there any rule of thumb as to how much inter-winding capacitance would be too much?

Measuring inductor current vs gate voltages, 1/22/2023 Ch1: Fluke 80i-110S, which has limited bandwidth

Ch4: Tek TCPA300 w/ TCP312 Current probe

Per changes listed on page 55, 100pF cap removed from R5, **<u>10nF from UCC28513 pin14-pin11</u>** 

Trying out with PFC boost inductors that are built by using toroid cores with no overlapping windings

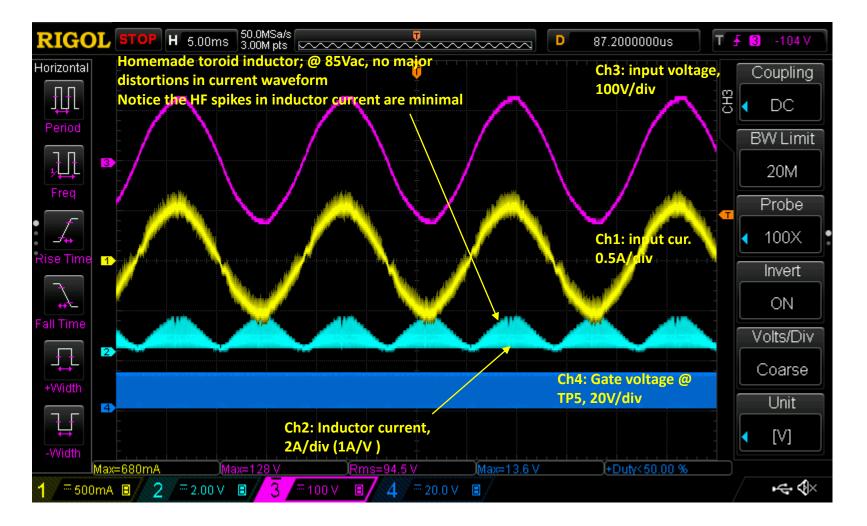


**Inductor #2**: Homemade inductor by using toroid core Wurth PN: 7427015 and 43 turns of single layer winding. Inductance measured at 1.39mH @ 300kHz.

Ch1: Fluke 80i-110S, which has limited bandwidth

Ch4: Tek TCPA300 w/ TCP312 Current probe

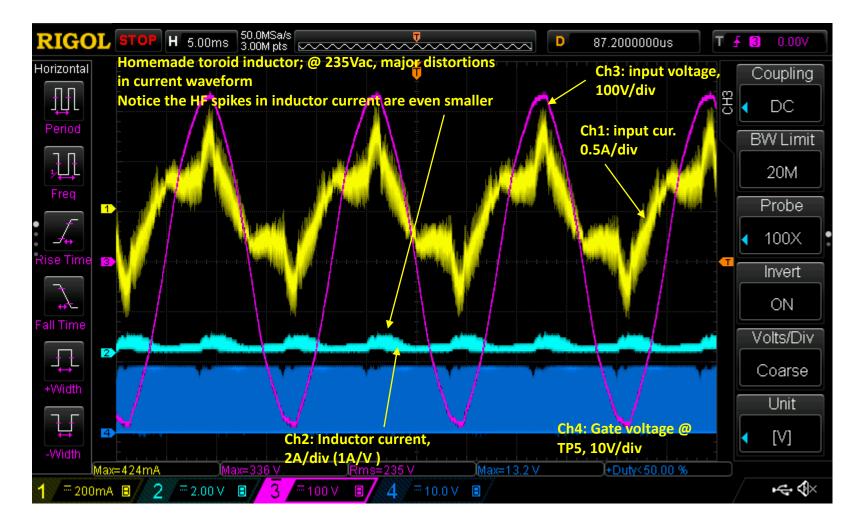
Per changes listed on page 55, 100pF cap removed from R5, 10nF from UCC28513 pin14-pin11



Ch1: Fluke 80i-110S, which has limited bandwidth

Ch4: Tek TCPA300 w/ TCP312 Current probe

Per changes listed on page 55, 100pF cap removed from R5, 10nF from UCC28513 pin14-pin11

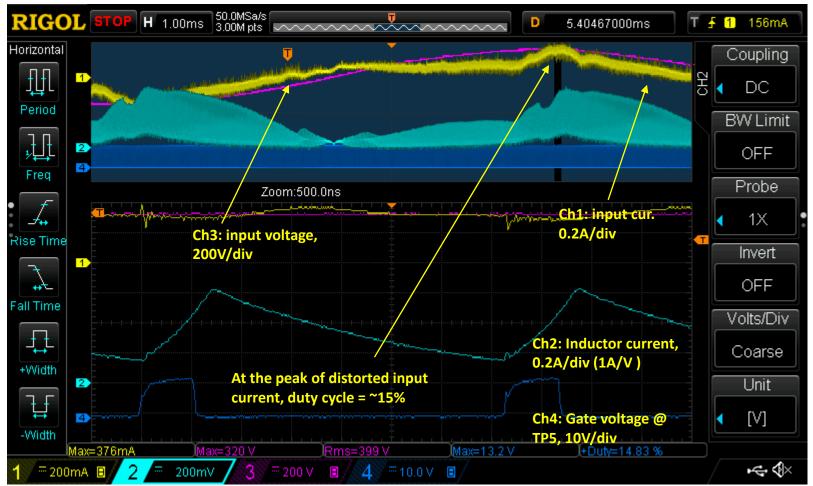


Ch1: Fluke 80i-110S, which has limited bandwidth

Ch4: Tek TCPA300 w/ TCP312 Current probe

Per changes listed on page 55, 100pF cap removed from R5, 100pF from UCC28513 pin14-pin11

Trying out with PFC boost inductors that are built by using toroid cores with no overlapping windings



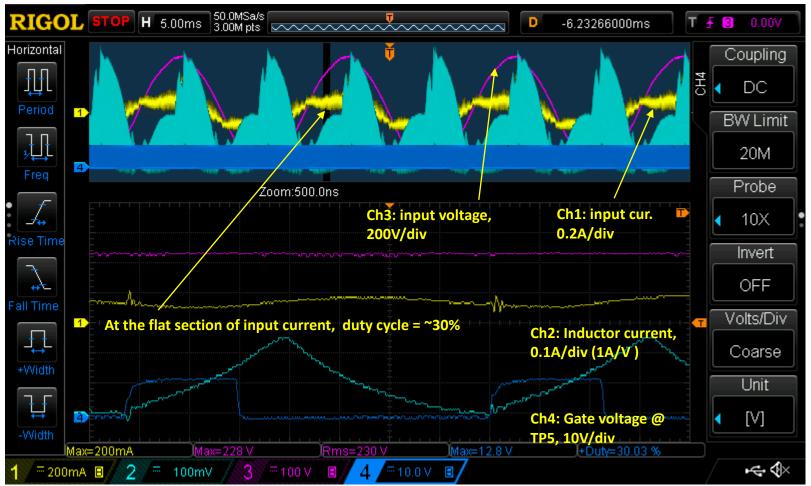
Homemade toroid inductor; @ 235Vac, major distortions in current waveform. Notice that there are no turn-on spikes in inductor current waveform

Ch1: Fluke 80i-110S, which has limited bandwidth

Ch4: Tek TCPA300 w/ TCP312 Current probe

Per changes listed on page 55, 100pF cap removed from R5, 100pF from UCC28513 pin14-pin11

Trying out with PFC boost inductors that are built by using toroid cores with no overlapping windings



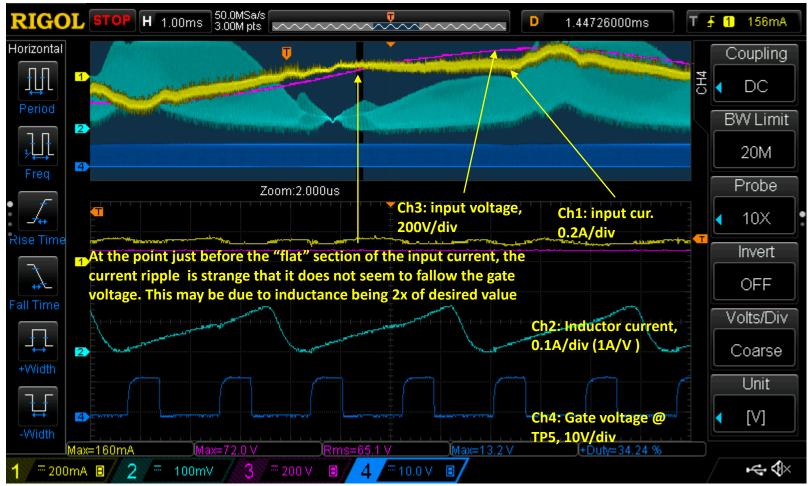
Homemade toroid inductor; @ 235Vac, major distortions in current waveform. Notice that there are no turn-on spikes in inductor current waveform

Ch1: Fluke 80i-110S, which has limited bandwidth

Ch4: Tek TCPA300 w/ TCP312 Current probe

Per changes listed on page 55, 100pF cap removed from R5, 10nF from UCC28513 pin14-pin11

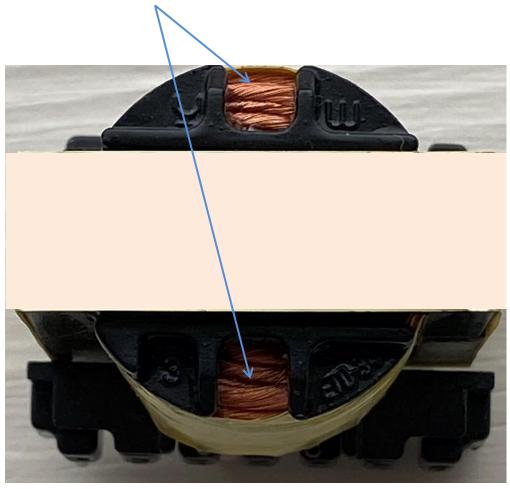
Trying out with PFC boost inductors that are built by using toroid cores with no overlapping windings



Homemade toroid inductor; @ 235Vac, major distortions in current waveform. Notice that there are no turn-on spikes in inductor current waveform

Measuring inductor current vs gate voltages, 1/22/2023 Ch1: Fluke 80i-110S, which has limited bandwidth Ch4: Tek TCPA300 w/ TCP312 Current probe Per changes listed on page 55, 100pF cap removed from R5, <u>10nF from UCC28513 pin14-pin11</u>

## **Original PFC inductor (680uH) has overlapping layers of winding**

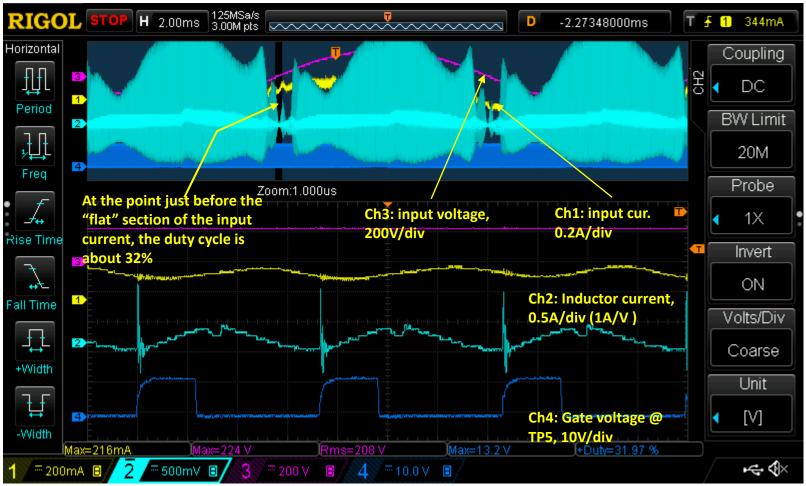


Ch1: Fluke 80i-110S, which has limited bandwidth

Ch4: Tek TCPA300 w/ TCP312 Current probe

Per changes listed on page 55, 100pF cap removed from R5, 100pF from UCC28513 pin14-pin11

Original inductor @ 235Vac, major distortions in current waveform. <u>Notice that there are significant</u> <u>current spikes at the time when MOSFET turns on.</u>

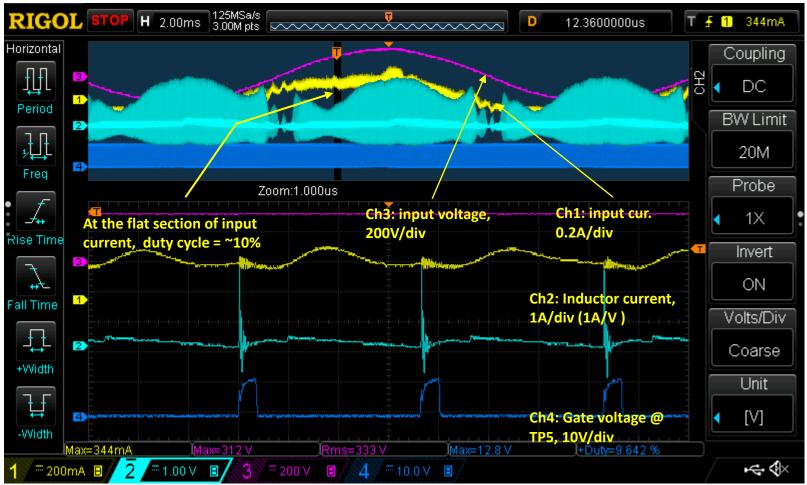


Ch1: Fluke 80i-110S, which has limited bandwidth

Ch4: Tek TCPA300 w/ TCP312 Current probe

Per changes listed on page 55, 100pF cap removed from R5, 10nF from UCC28513 pin14-pin11

Original inductor @ 235Vac, major distortions in current waveform. <u>Notice that there are significant</u> <u>current spikes at the time when MOSFET turns on.</u>

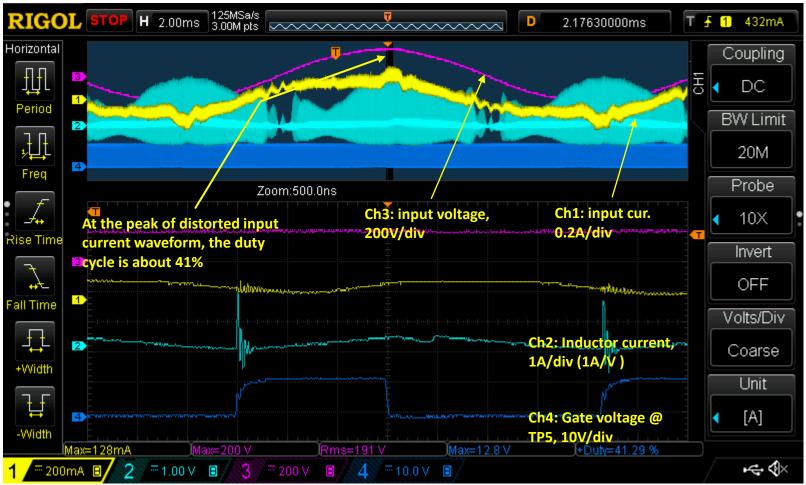


Ch1: Fluke 80i-110S, which has limited bandwidth

Ch4: Tek TCPA300 w/ TCP312 Current probe

Per changes listed on page 55, 100pF cap removed from R5, 10nF from UCC28513 pin14-pin11

Original inductor @ 235Vac, major distortions in current waveform. <u>Notice that there are significant</u> <u>current spikes at the time when MOSFET turns on.</u>



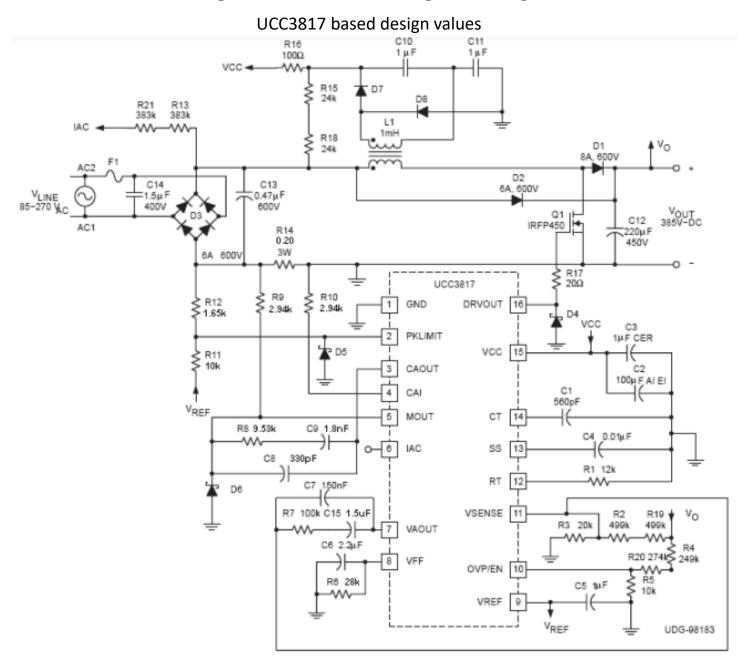
Measuring inductor current vs gate voltages, 1/22/2023 Ch1: Fluke 80i-110S, which has limited bandwidth Ch4: Tek TCPA300 w/ TCP312 Current probe Per changes listed on page 55, 100pF cap removed from R5, <u>10nF from UCC28513 pin14-pin11</u>

### Conclusions on 1/22:

- It seems like there is significant inter-winding capacitance in original inductor (TSD-3222, 680uH) which creates significant current spikes at the time when MOSFET turns on. Additional measurements conducted with 10nF cap on PKLMT pin14 to GND do not show any pulse droppings. However, the low frequency distortions in input current waveform are still visible.
- 2. The home-made toroid inductor (1.39mH @ 300kHz) was also tried out with 10nF on PKLMT pin. No pulse droppings observed. However, the low frequency distortions in input current waveforms were still visible. There was some unexpected results at the zero crossing of the voltage. This may be due to inductance being larger than the expected value. Repeat the same test with smaller toroid inductor with 680uH inductance.

Even though the original inductor has some inter-winding capacitance and even though it should be addressed, it seems that the current distortion may not be caused by the inter-winding capacitance since:

- 1. The current distortions are visible even when a toroid inductor with minimum inter-winding capacitance is used. There were no turn-on spikes and no pulse dropping observed with 10nF capacitance on PKLMT.
- 2. When the original inductor was used, there were significant current spikes at the turn on. Even though no pulse droppings observed with 10nF on PKLMT pin, the input current waveform was still distorted.



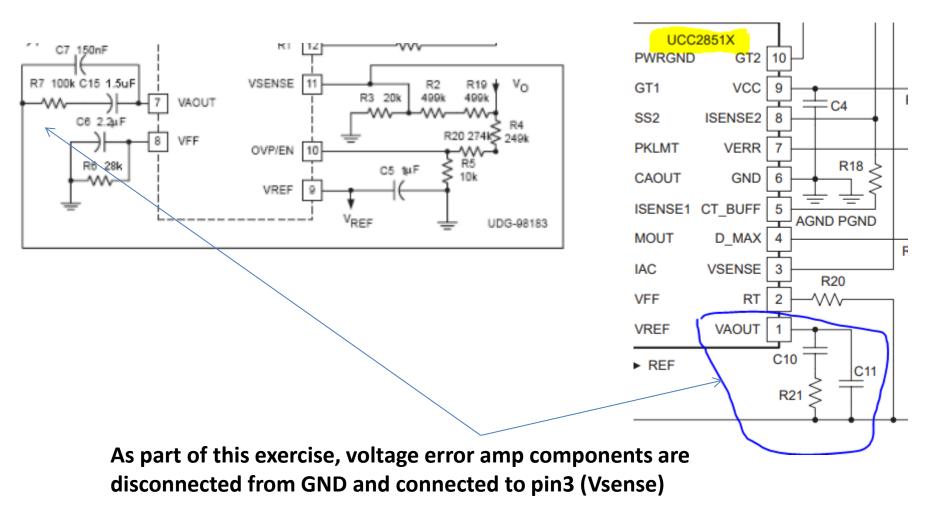
### UCC3817 based design values

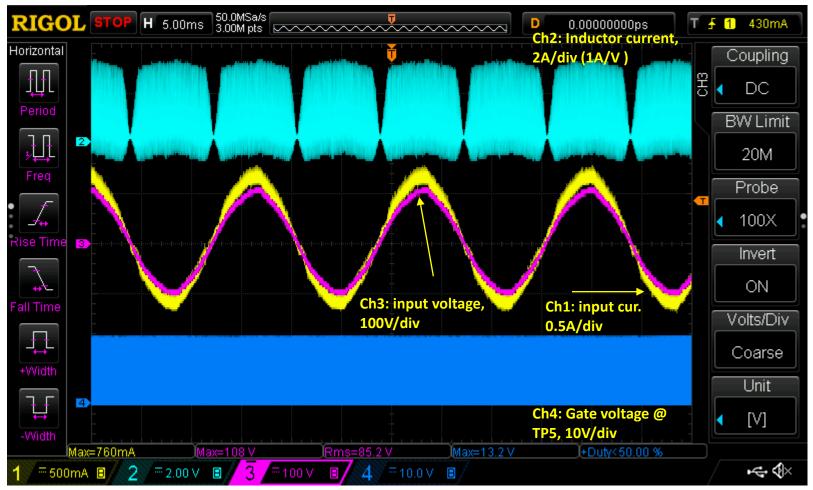
RefDes on UCC3817	RefDes on UCC28513	RefDes in Listen	РСВ	Existing values	New values
R14=0.2	R2	R43		0.44	0.22
R3=20K	-	R60	PSB-04	22.1K	20К
R2/R19=499K	-	R44/R49		562K	499K
R21/R13	-	R47/R50		383K	No change
R11=10K	R14	R13		10K	No change
R12=1.65k	R7	R5		1.5K	1.62K
R9=2.94K	R12	R4		2.74K	2.94K (3.16k//39k)
C8=330p	C7	C8		150pF	330p
C9=1.8nF	C6	C6		3.3n	1.6nF
R8=9.53K	R13	R10	-	4.7K	9.53K (20k//18.2k)
R10=2.94K	R8	R9	PFC-03	2.74К	2.94K (3.16k//39k)
R6=28K	R15	R11		30.1K	28K (56k//56k)
C6=2.2uF	C8	С9	-	4.7uF	2uF (1uF//1uF)
C7=150n	C11	C2		150n	No change
C15=1.5uF	C10	C1		1.5uF	No change
R7=100k	R21	R1		48.7k	100k

UCC3817 based design values

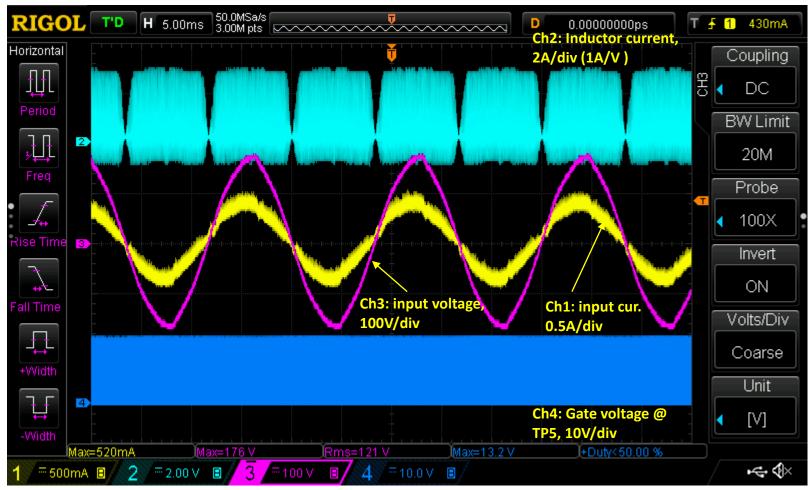
## UCC3817 voltage error amp.

### UCC28513 voltage error amp.

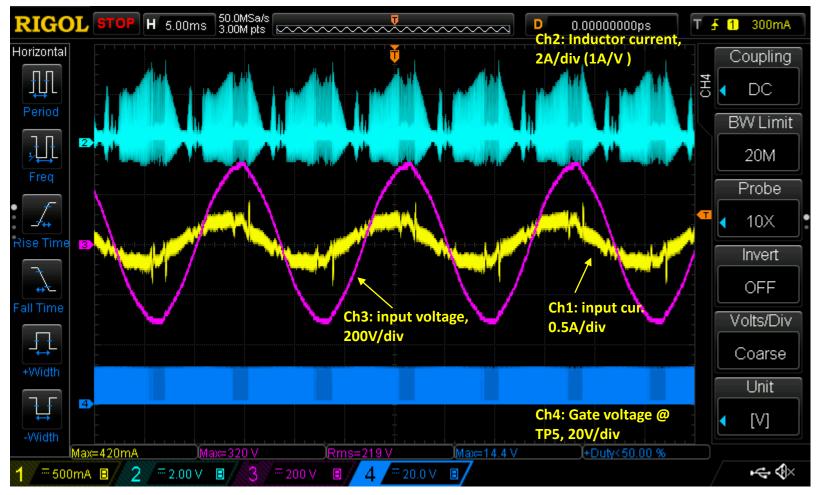




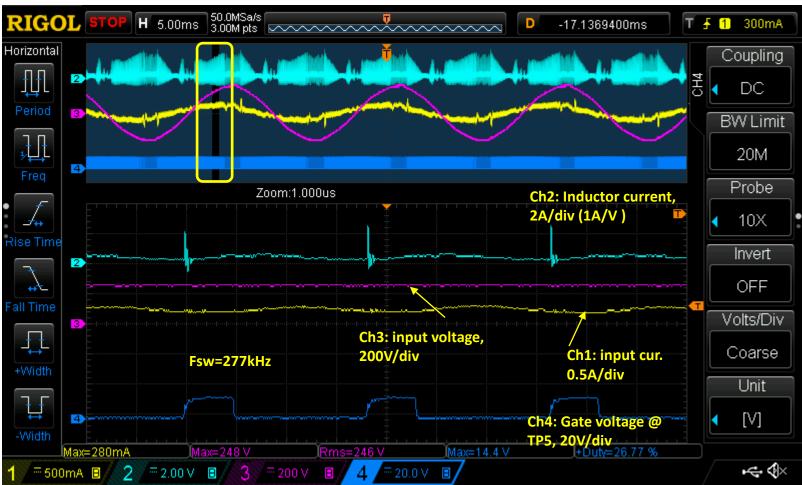
No major distortions at 85Vac input voltage



No major distortions at 120Vac input voltage



Distortions start at around 220Vac

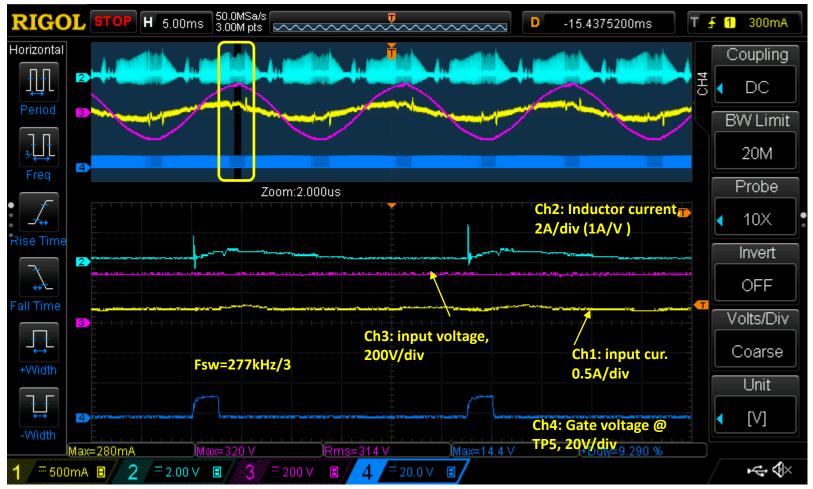


Distortions start at around 220Vac; zooming into time just before input voltage reaches its peak region

#### Measuring inductor current vs gate voltages, 2/5/2023 PSB-04, PFC-03, CONT A w/ PFC board ,SN: AG155544221261437

L1, Q5, Q6 on PSB removed, 25W external load across the DC-link, no capacitor across R5 Original boost inductor (680uH), 10nF cap on PKLMT pin14 to GND, see slide 94 for modifications

Distortions start at around 220Vac; zooming into the region where input voltage is at its peak Notice that the switching frequency is reduced to 1/3rd



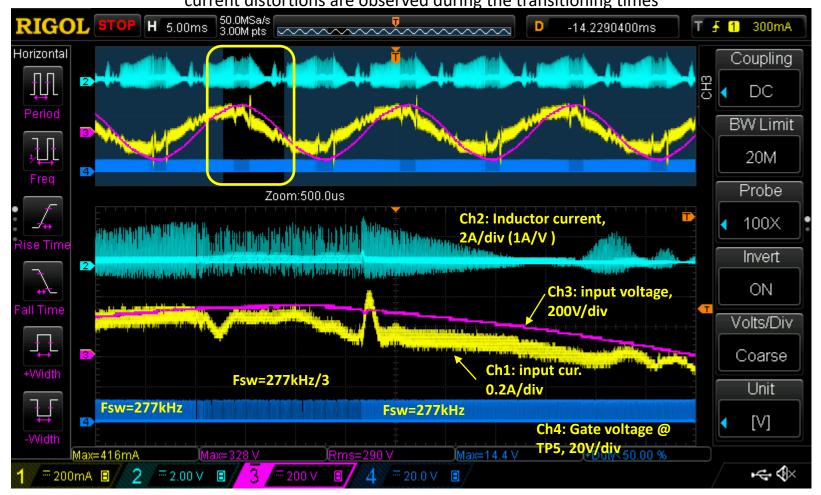
#### Measuring inductor current vs gate voltages, 2/5/2023 PSB-04, PFC-03, CONT A w/ PFC board ,SN: AG155544221261437

L1, Q5, Q6 on PSB removed, 25W external load across the DC-link, no capacitor across R5

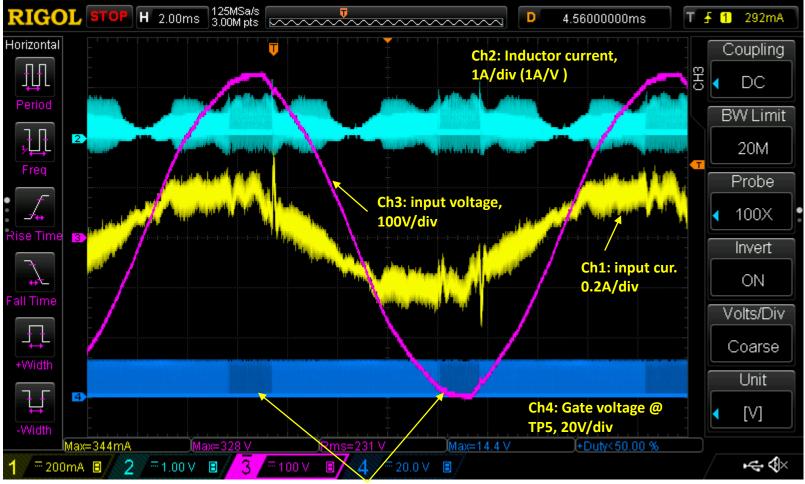
Original boost inductor (680uH), 10nF cap on PKLMT pin14 to GND, see slide 94 for modifications

Distortions start at around 220Vac; zooming into the region where input voltage is at its peak

Notice that the switching frequency is reduced to 1/3<sup>rd</sup> at the peak of input voltage and then changes back to Fsw and current distortions are observed during the transitioning times

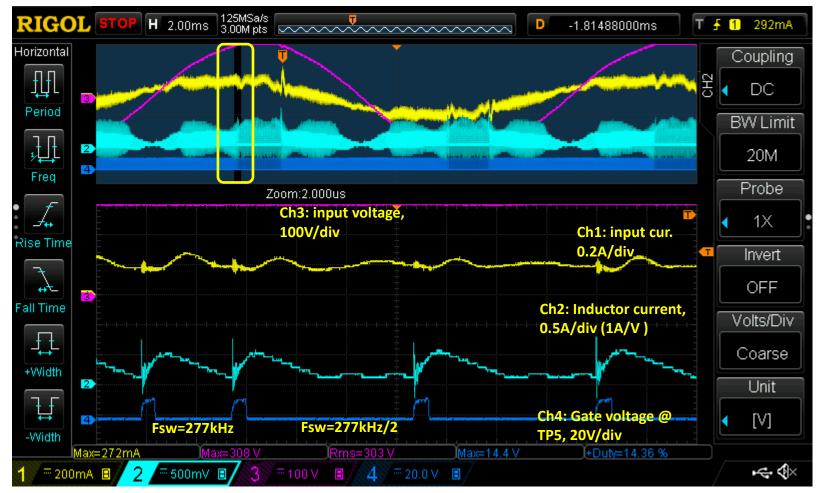


Distortions start at around 220Vac; notice less HF cur. through inductor probably due to less inter-winding capacitance

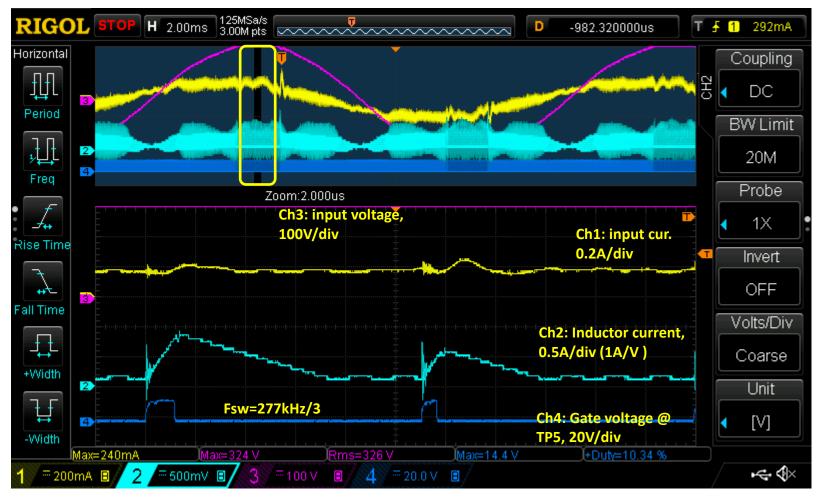


Areas of interest

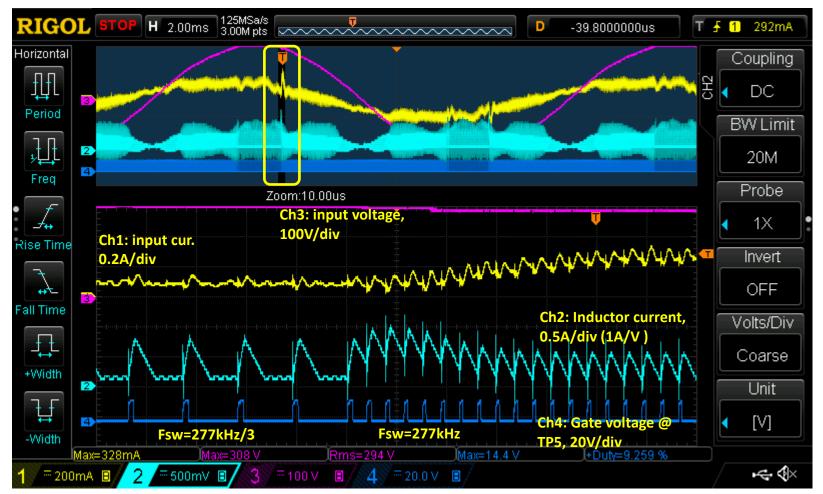
Distortions start at around 220Vac; as input voltage reaches its peak, switching frequency is reduced by half



Distortions start at around 220Vac; at the peak of input voltage , switching frequency is reduced to 1/3 rd



Distortions start at around 220Vac; current distortions observed as the switching frequency changes back to 277kHz



#### **Conclusions:**

- Referencing UCC3817 design, component values are updated
- Voltage feedback circuit is disconnected from GND and connected to pin3
- Two inductors were tried: original boost inductor (probably with some inter-winding capacitance) and an other toroid inductor, presumably with less inter-winding inductance. Both resulted in similar current distortions at high supply voltages.
- In both cases, the switching frequency was reduced at the time when supply voltage approached to its peak and switching frequency increased back as supply voltage starts to decrease. Current distortions were observed during the times when switching frequency changes were observed.
- There is no specific indication that PKLMT was initiated. All tests were conducted with 10nF cap from pin14 (PKLMT) to pin11 (GND) on UCC28513

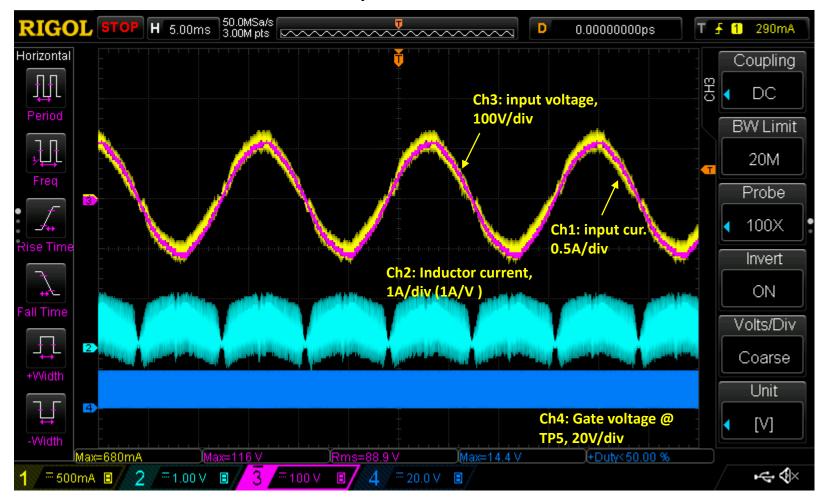
#### Measuring inductor current vs gate voltages, 2/12/2023 PSB-04, PFC-03, CONT A w/ PFC board ,SN: AG155544221261437 25W external load across the DC-link 560uH toroid (2300LL-561-H-RC), 10nF cap on PKLMT pin14 to GND

RefDes on UCC28513	RefDes in Listen	РСВ	Existing values	New values 2/5/23	New values 2/12/23
R2	R43		0.44	0.22	0.44
-	R60	PSB-04	22.1K	20K	No change
-	R44/R49		562K	499K	No change
-	R47/R50		383K	No change	No change
R14	R13		10K	No change	No change
R7	R5		1.5K	1.62K	No change
R12	R4		2.74K	2.94K (3.16k//39k)	3k (3.16k//56k)
C7	C8		150pF	330p	No change
C6	C6		3.3n	1.6nF	4.9nF (1.6n+3.3n)
R13	R10		4.7К	9.53K (20k//18.2k)	3.23k (3.3k//150k)
R8	R9	PFC-03	2.74K	2.94K (3.16k//39k)	3k (3.16k//56k)
R15	R11		30.1K	28K (56k//56k)	No change
C8	C9		4.7uF	2uF (1uF//1uF)	No change
C11	C2		150n	No change	No change
C10	C1		1.5uF	No change	No change
R21	R1		48.7k	100k	No change

### Measuring inductor current vs gate voltages, 2/12/2023 PSB-04, PFC-03, CONT A w/ PFC board ,SN: AG155544221261437

25W external load across the DC-link

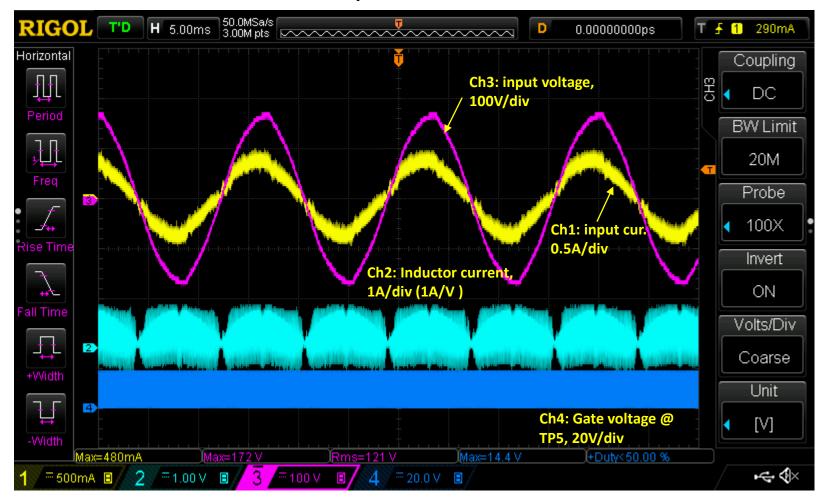
560uH toroid (2300LL-561-H-RC), 10nF cap on PKLMT pin14 to GND, see slide 107 for modifications



No major distortions at 85Vac

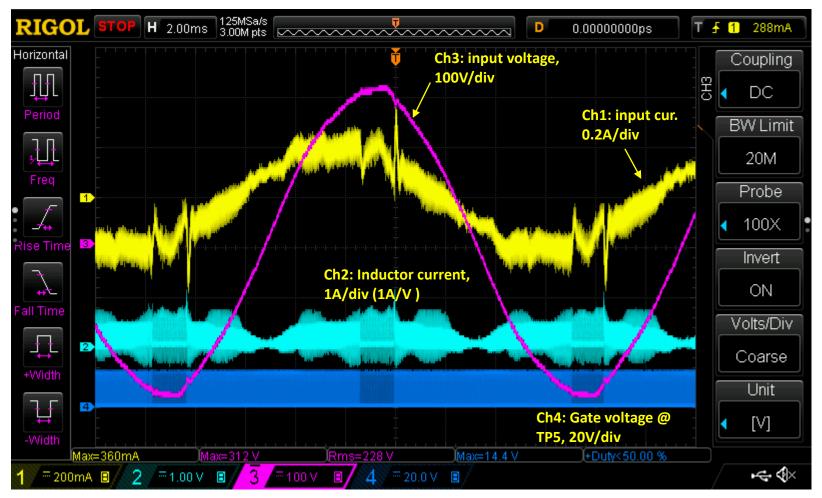
25W external load across the DC-link

560uH toroid (2300LL-561-H-RC), 10nF cap on PKLMT pin14 to GND, see slide 107 for modifications



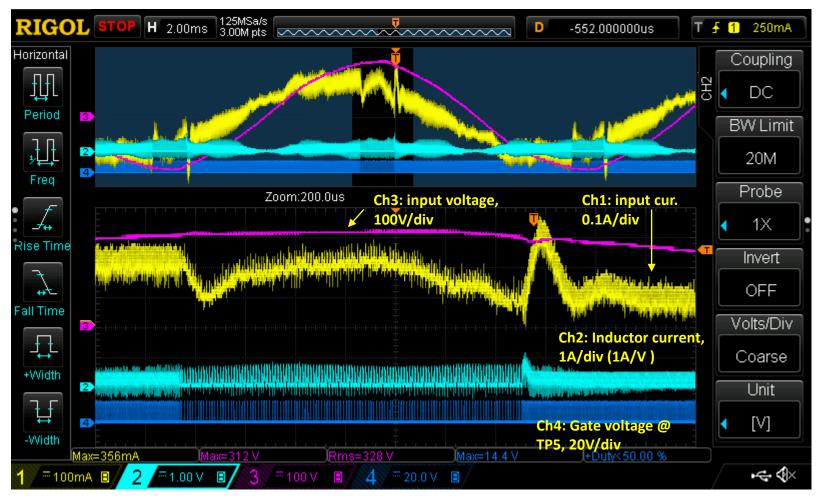
No major distortions at 120Vac

560uH toroid (2300LL-561-H-RC), 10nF cap on PKLMT pin14 to GND, see slide 107 for modifications



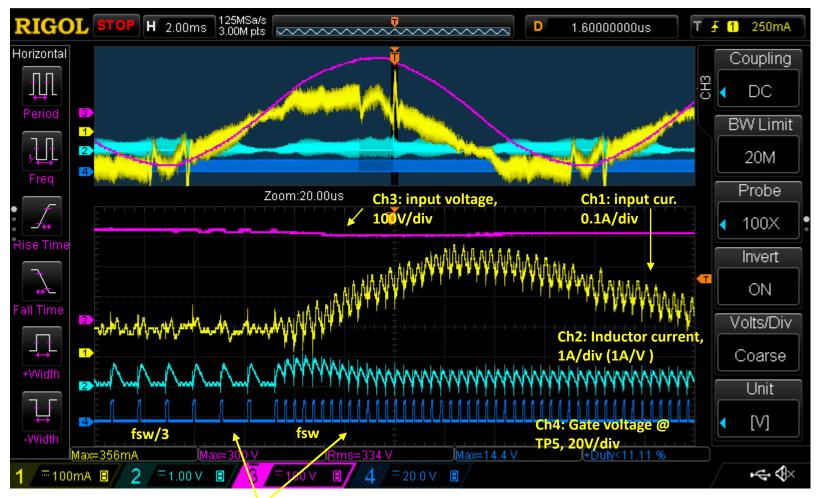
At around 230Vac, current distortions appear

560uH toroid (2300LL-561-H-RC), 10nF cap on PKLMT pin14 to GND, see slide 107 for modifications



At around 230Vac, current distortions appear

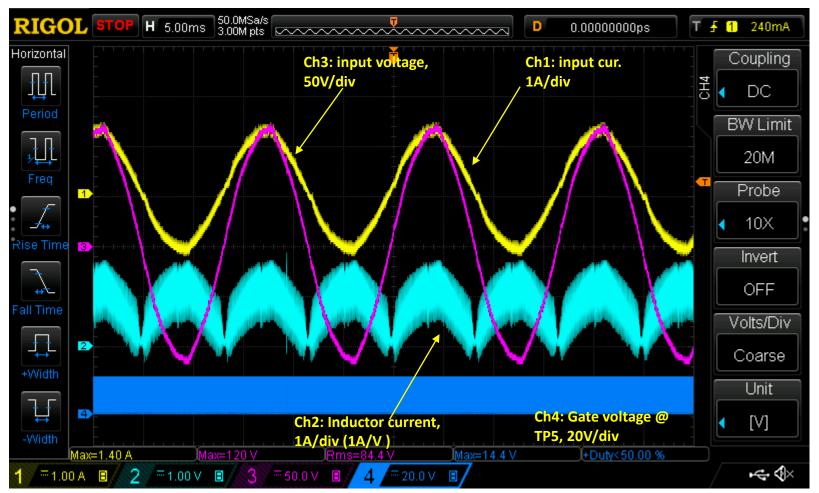
560uH toroid (2300LL-561-H-RC), 10nF cap on PKLMT pin14 to GND, see slide 107 for modifications



At around 230Vac, current distortions appear

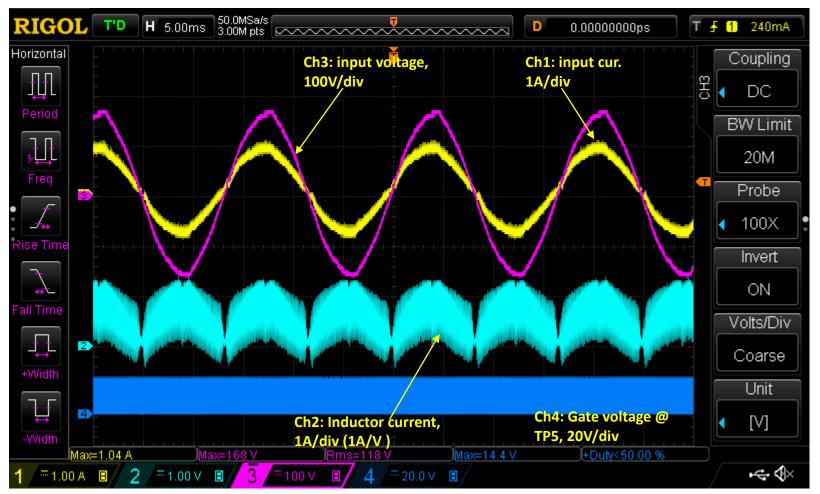
Switching frequency was reduced to 1/3<sup>rd</sup> and then increased back; at which point current spike was observed

560uH toroid (2300LL-561-H-RC), 10nF cap on PKLMT pin14 to GND, see slide 107 for modifications



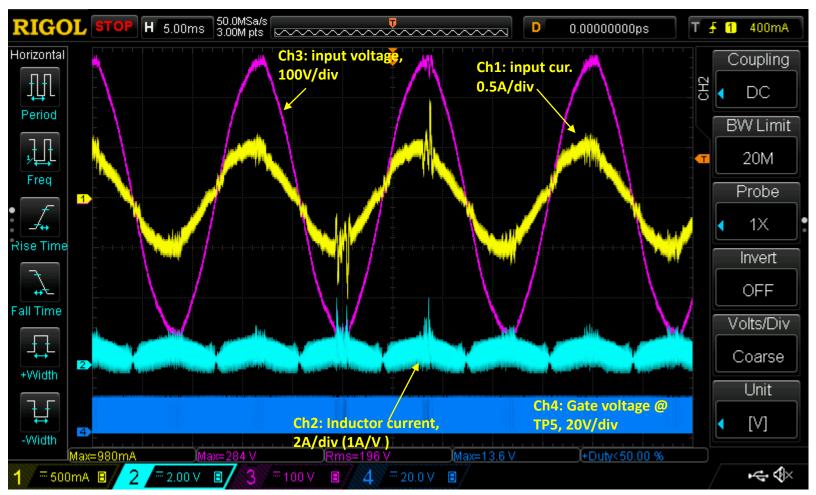
With 60W output power, no major distortions at 85Vac input

560uH toroid (2300LL-561-H-RC), 10nF cap on PKLMT pin14 to GND, see slide 107 for modifications



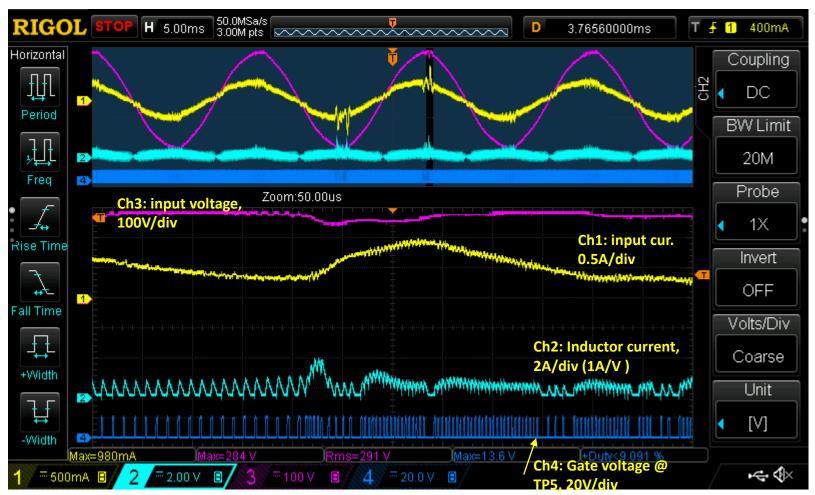
With 60W output power, no major distortions at 120Vac input

560uH toroid (2300LL-561-H-RC), 10nF cap on PKLMT pin14 to GND, see slide 107 for modifications



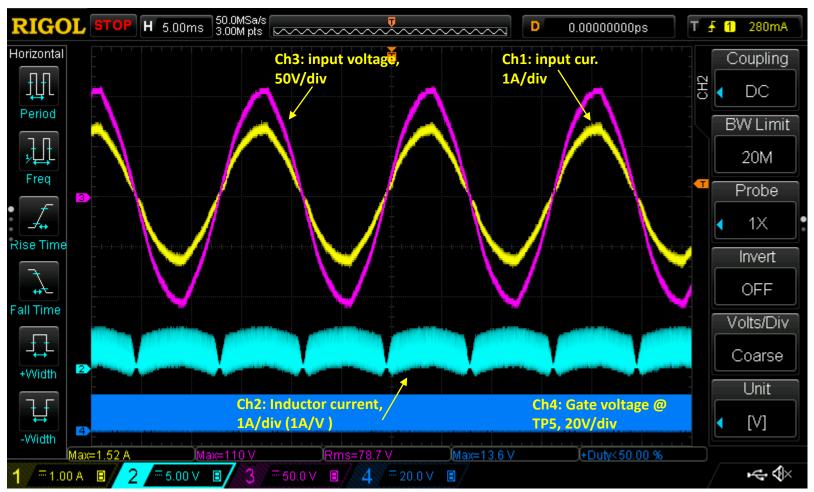
With 60W output power, major distortions at around 200Vac input (got worse)

560uH toroid (2300LL-561-H-RC), 10nF cap on PKLMT pin14 to GND, see slide 107 for modifications



With 60W output power, major distortions at around 200Vac input (got worse)

Original boost inductor (680uH), 10nF cap on PKLMT pin14 to GND, see slide 107 for modifications

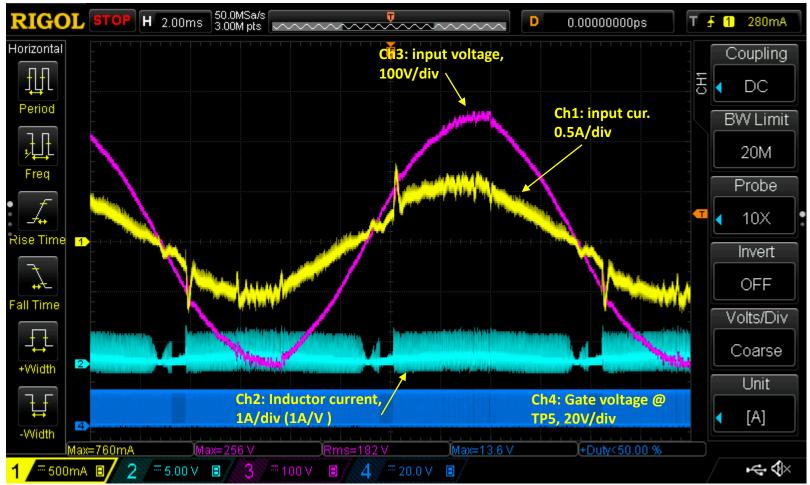


With original inductor and 60W output power, no major distortions at 85Vac

60W external load across the DC-link

Original boost inductor (680uH), 10nF cap on PKLMT pin14 to GND, see slide 107 for modifications

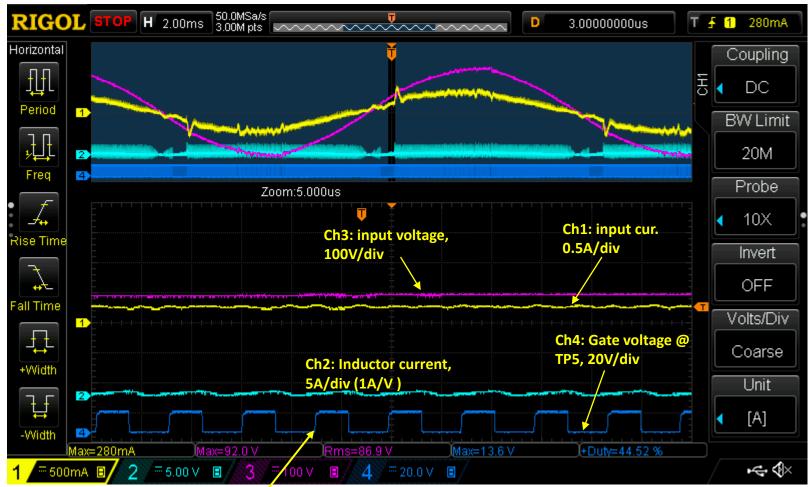
With original inductor and 60W output power, distortions at slightly different locations started at even lower voltage, 180Vac



60W external load across the DC-link

Original boost inductor (680uH), 10nF cap on PKLMT pin14 to GND, see slide 107 for modifications

With original inductor and 60W output power, distortions at slightly different locations started at even lower voltage, 180Vac



Switching frequency was reduced to fsw/s , duty cycle was ~50% prior to current spike

60W external load across the DC-link

Original boost inductor (680uH), 10nF cap on PKLMT pin14 to GND, see slide 107 for modifications

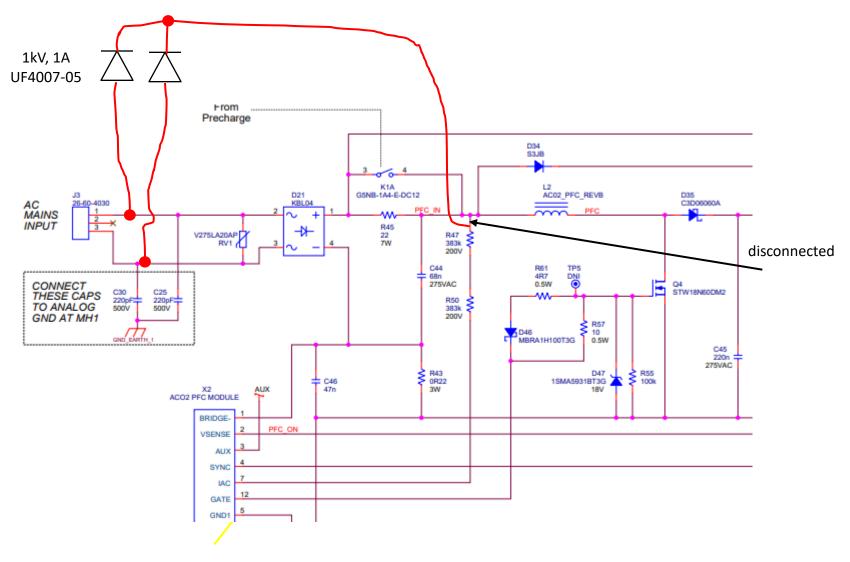
With original inductor and 60W output power, distortions at slightly different locations started at even lower voltage, 180Vac



Switching frequency was increased back to fsw; at which point current spike was observed, duty cycle was about 70%

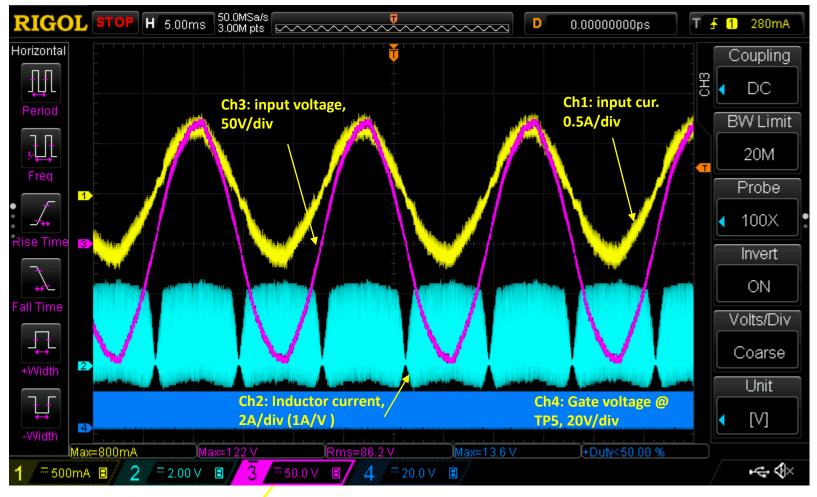
30W external load across the DC-link

Original boost inductor (680uH), 10nF cap on PKLMT pin14 to GND, see slide 107 for modifications



Original boost inductor (680uH), 10nF cap on PKLMT pin14 to GND, see slide 107 for modifications

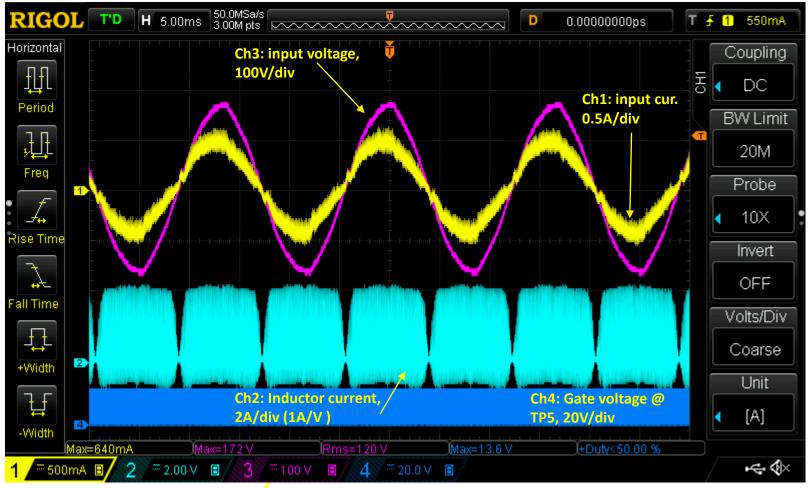
With original inductor, 30W output power and Iac connection moved to input of rectifier, no major distortions at 85Vac



### 30W external load across the DC-link

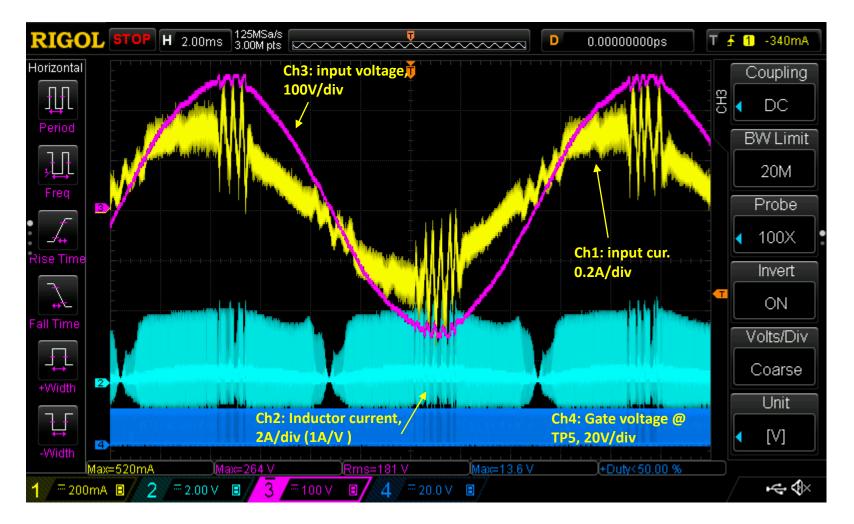
Original boost inductor (680uH), 10nF cap on PKLMT pin14 to GND, see slide 107 for modifications

With original inductor, 30W output power and Iac connection moved to input of rectifier, no major distortions at 120Vac



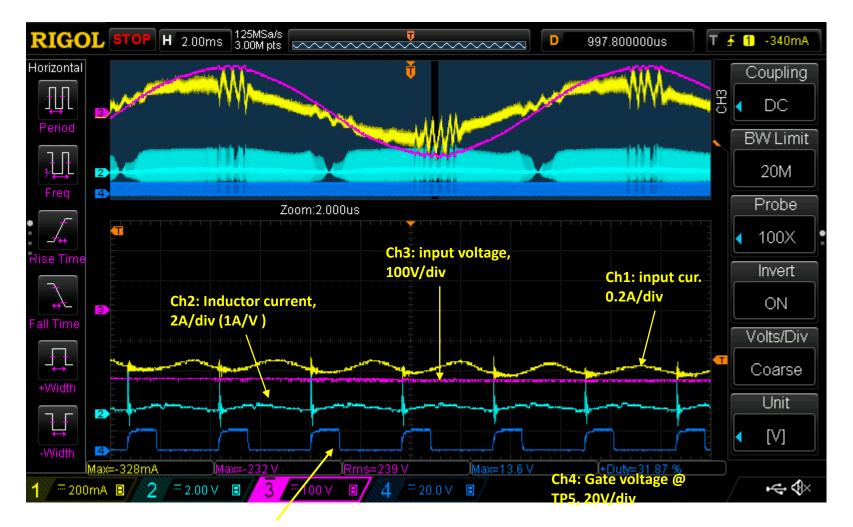
Original boost inductor (680uH), 10nF cap on PKLMT pin14 to GND, see slide 107 for modifications

With original inductor, 30W output power and Iac connection moved to input of rectifier, major distortions at 180Vac



**Original boost inductor (680uH),** 10nF cap on PKLMT pin14 to GND, see slide 107 for modifications

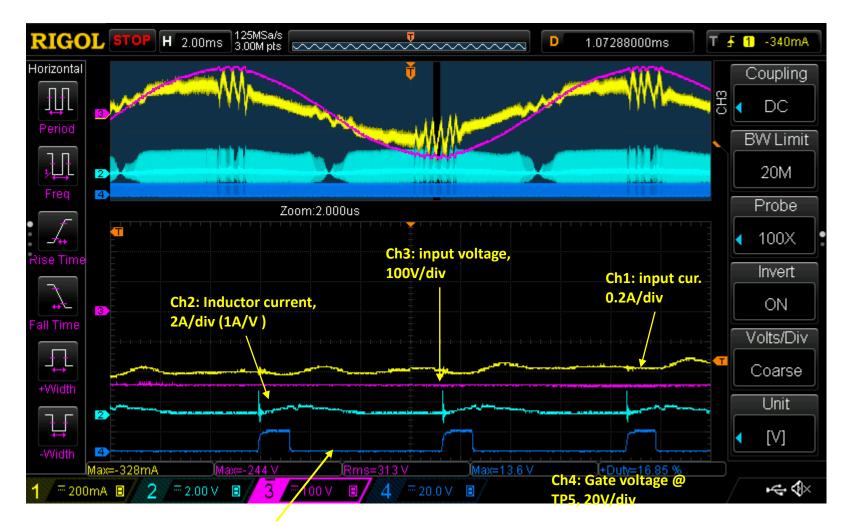
With original inductor, 30W output power and Iac connection moved to input of rectifier, major distortions at 180Vac



Switching frequency was normal and duty cycle was about 32% (notice that the on-time was constant)

Original boost inductor (680uH), 10nF cap on PKLMT pin14 to GND, see slide 107 for modifications

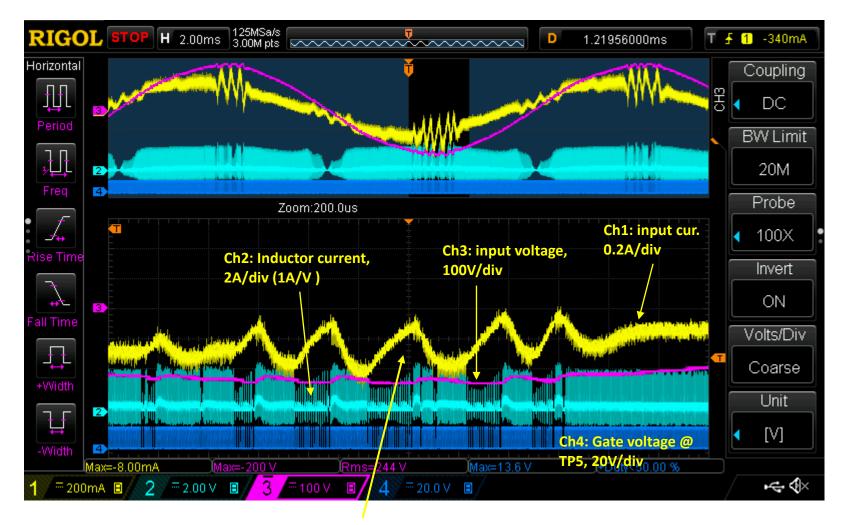
With original inductor, 30W output power and Iac connection moved to input of rectifier, major distortions at 180Vac



Switching frequency was reduced to fsw/2 and duty cycle was about 16% (notice that the on-time was constant)

Original boost inductor (680uH), 10nF cap on PKLMT pin14 to GND, see slide 107 for modifications

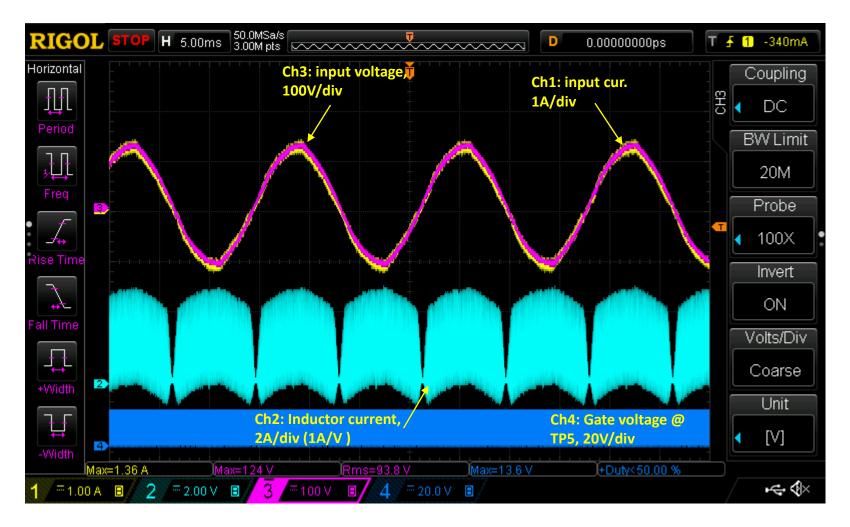
With original inductor, 30W output power and Iac connection moved to input of rectifier, major distortions at 180Vac



About 3.3kHz current oscillations

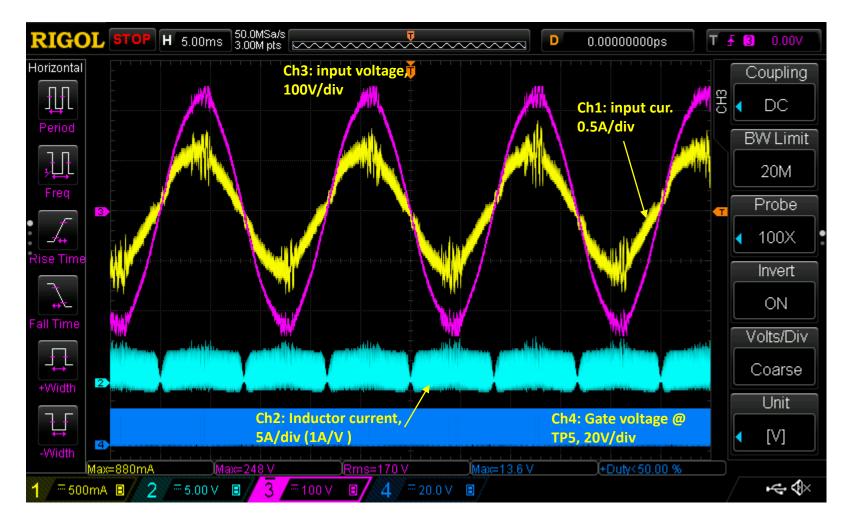
**Original boost inductor (680uH),** 10nF cap on PKLMT pin14 to GND, see slide 107 for modifications

With original inductor, 60W output power and Iac connection moved to input of rectifier, no major distortions at 85Vac



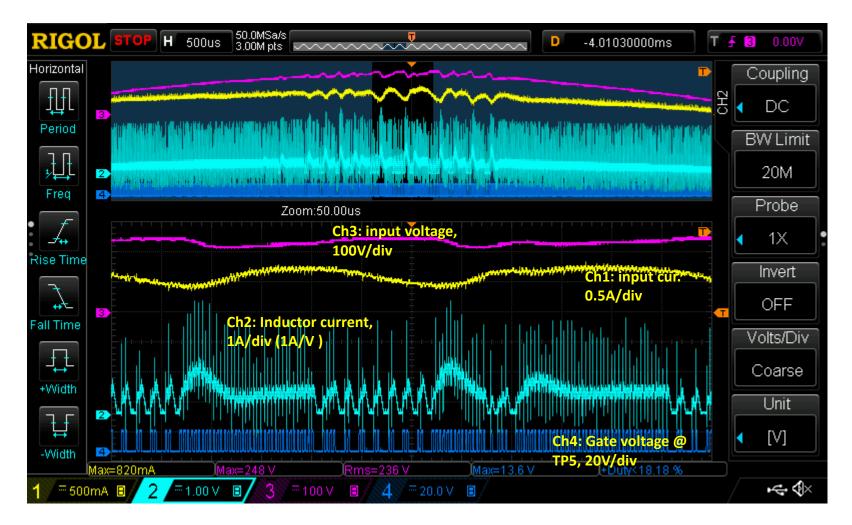
**Original boost inductor (680uH),** 10nF cap on PKLMT pin14 to GND, see slide 107 for modifications

With original inductor, 60W output power and Iac connection moved to input of rectifier, major distortions at ~180Vac



**Original boost inductor (680uH),** 10nF cap on PKLMT pin14 to GND, see slide 107 for modifications

With original inductor, 60W output power and Iac connection moved to input of rectifier, major distortions at ~180Vac

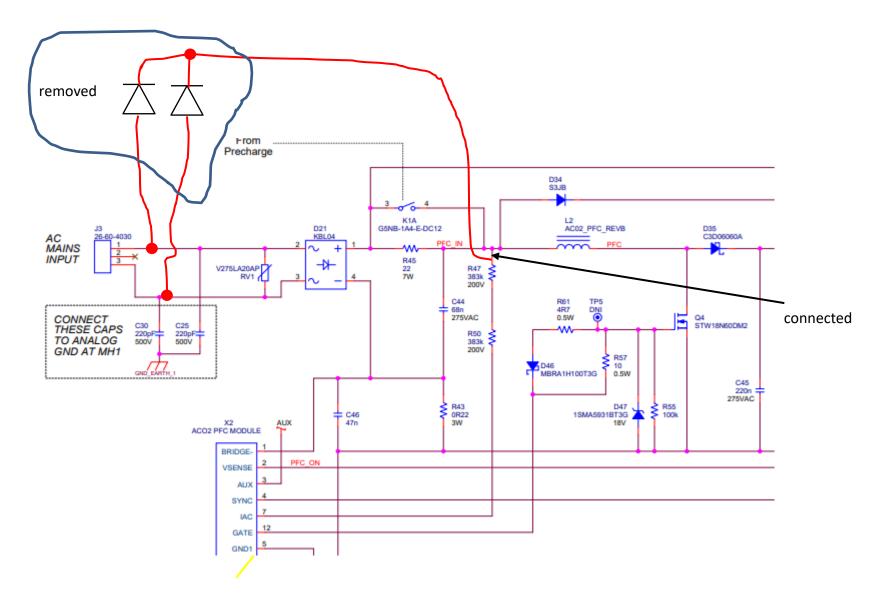


Same phenomenon observed; switching frequency was reduced and then increased, at which time current spike was observed

**Original boost inductor (680uH),** 10nF cap on PKLMT pin14 to GND, see slide 107 for modifications

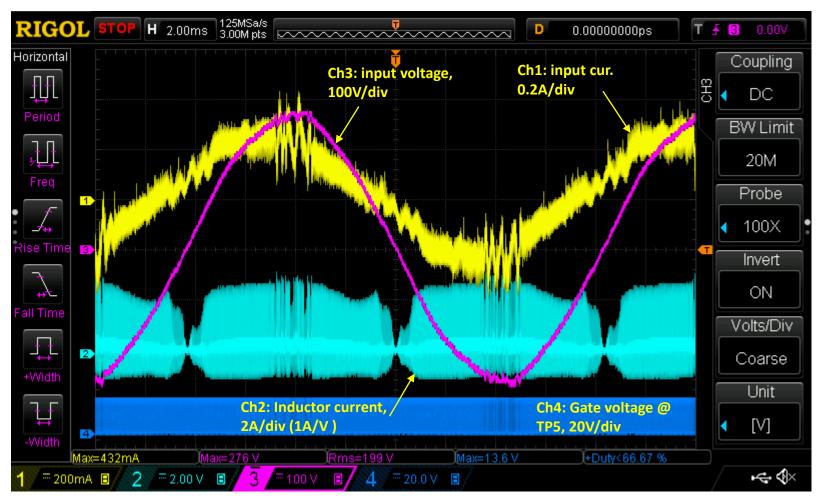
Conclusions as of 2/12:

- 1) Changes on slide 107 were implemented; load was changed from 25W to 60W and inductance with lower interwinding capacitance was tried out. No change
- 2) lac sense point was moved to input of rectifier. Tried with different loads and inductors; the nature of distortion appears to change and the voltage at which distortions begins was lowered; so it got worse.



Original boost inductor (680uH), 10nF cap on PKLMT pin14 to GND, see slide 107 for modifications

With original inductor, 30W output power major distortions start above 200Vac



L1, Q5, Q6 on PSB removed, 30W external load across the DC-link

2pc of original boost inductors in series (1.36mH total), 10nF cap on PKLMT pin14 to GND, see slide 107 for modifications

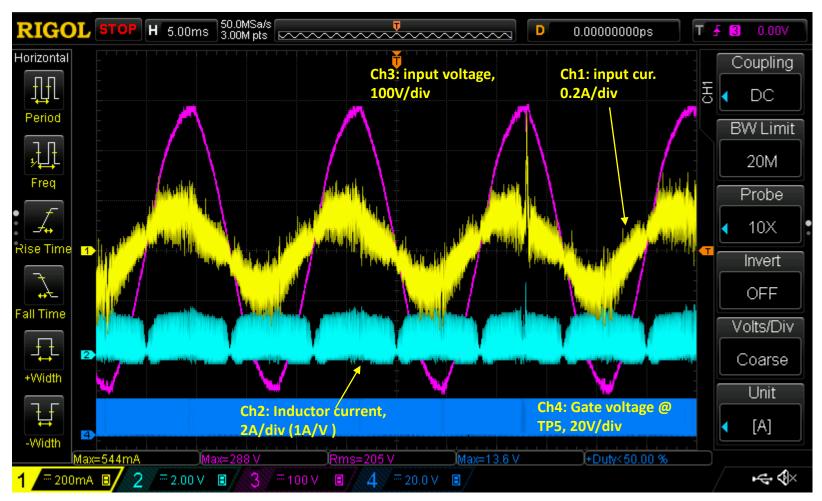
H 5.00ms 50.0MSa/s RIGOL D 0.00000000ps T 🗲 🕄 0.00V STOP Horizontal Coupling Ch3: input voltage, ſĮſ CH3 100V/div DC Period **BW Limit** ļļ 3 20M Probe 100X ≠⇔ **Rise Time** Ch1: input cur. Invert 0.5A/div ΟN ++ Volts/Div £ Coarse Unit Ch2: Inductor current, Ch4: Gate voltage @ [V] 2A/div (1A/V) **TP5, 20V/div** Max=120 V Rms=84.6 V Max=560mA Max=13.6 V +Duty<50.00 % •**----**--{\$ 🏧 2.00 V 🛛 🖪 3 <sup>≕</sup>100 V 🚍 20.0 V 🛛 🔳 = 500mA 📳 2 

With 2x original inductor, 30W output power, no distortions at 85Vac

L1, Q5, Q6 on PSB removed, 30W external load across the DC-link

2pc of original boost inductors in series (1.36mH total), 10nF cap on PKLMT pin14 to GND, see slide 107 for modifications

With 2x original inductor, 30W output power, non-periodic distortions start to appear at 200Vac



L1, Q5, Q6 on PSB removed, 30W external load across the DC-link

2pc of original boost inductors in series (1.36mH total), 10nF cap on PKLMT pin14 to GND, see slide 107 for modifications

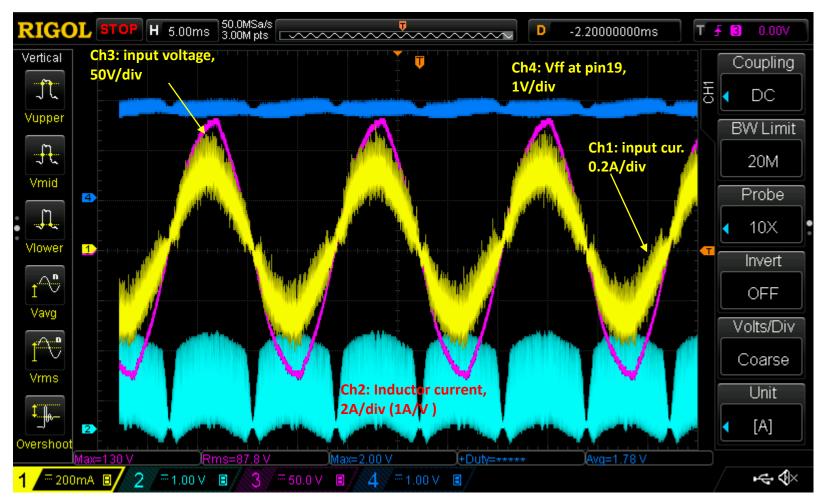
With 2x original inductor, 30W output power, periodic distortions start to appear at 210Vac, note: Vdc\_out=380V



L1, Q5, Q6 on PSB removed, 30W external load across the DC-link

2pc of original boost inductors in series (1.36mH total), 10nF cap on PKLMT pin14 to GND, see slide 107 for modifications

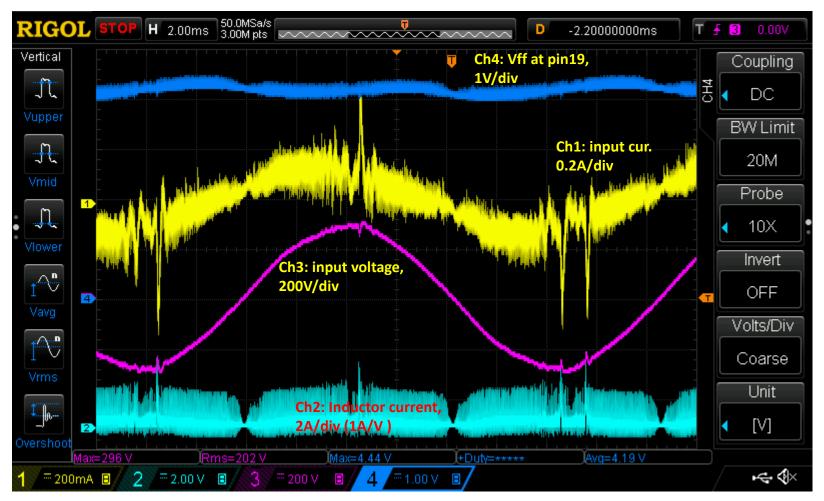
With 2x original inductor, 30W output power, no distortions at 85Vac, Vff=1.78V w/ differential probe



L1, Q5, Q6 on PSB removed, 30W external load across the DC-link

2pc of original boost inductors in series (1.36mH total), 10nF cap on PKLMT pin14 to GND, see slide 107 for modifications

With 2x original inductor, 30W output power, distortions at 200Vac, Vff=4.19V w/ differential probe



L1, Q5, Q6 on PSB removed, 30W external load across the DC-link

2pc of original boost inductors in series (1.36mH total), 10nF cap on PKLMT pin14 to GND, see slide 107 for modifications

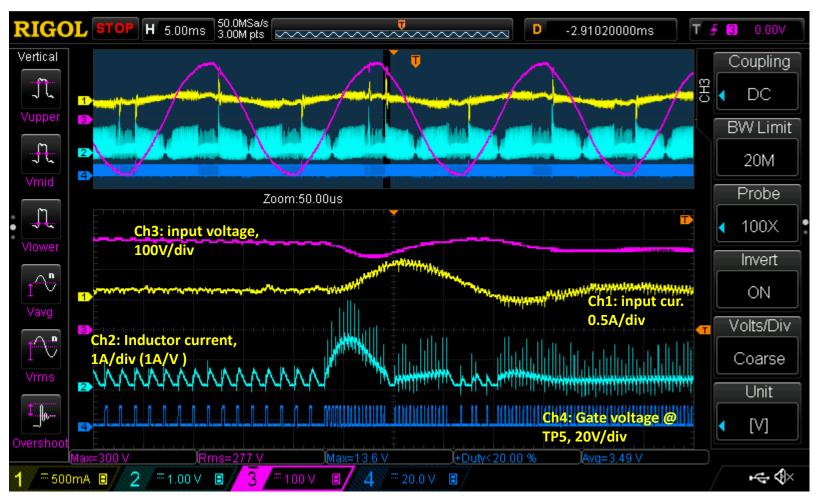
With 2x original inductor, 30W output power, distortions at 200Vac, Vff=4.19V w/ differential probe It looks like differential probe has some DC offset at low voltages. Vff is also measured with a DVM, Fluke 179, by removing differential probe

Input voltage (Vrms)	Vff @ pin19 (Vdc) w/ differential probe	Vff @ pin19 (Vdc) w/ DVM
85	1.78	1.46
120		2.11
200	4.19	3.50
220		3.85

L1, Q5, Q6 on PSB removed, 30W external load across the DC-link

2pc of original boost inductors in series (1.36mH total), 10nF cap on PKLMT pin14 to GND, see slide 107 for modifications

With 2x original inductor, 30W output power, distortions at 220Vac, Vff=3.85V w/ DVM



L1, Q5, Q6 on PSB removed, 60W external load across the DC-link

2pc of original boost inductors in series (1.36mH total), 10nF cap on PKLMT pin14 to GND, see slide 107 for modifications





L1, Q5, Q6 on PSB removed, 60W external load across the DC-link

2pc of original boost inductors in series (1.36mH total), 10nF cap on PKLMT pin14 to GND, see slide 107 for modifications

With 2x original inductor, 60W output power, distortions at 200Vac, Vff=3.45V w/ DVM



L1, Q5, Q6 on PSB removed, 60W external load across the DC-link

2pc of original boost inductors in series (1.36mH total), 10nF cap on PKLMT pin14 to GND, see slide 107 for modifications

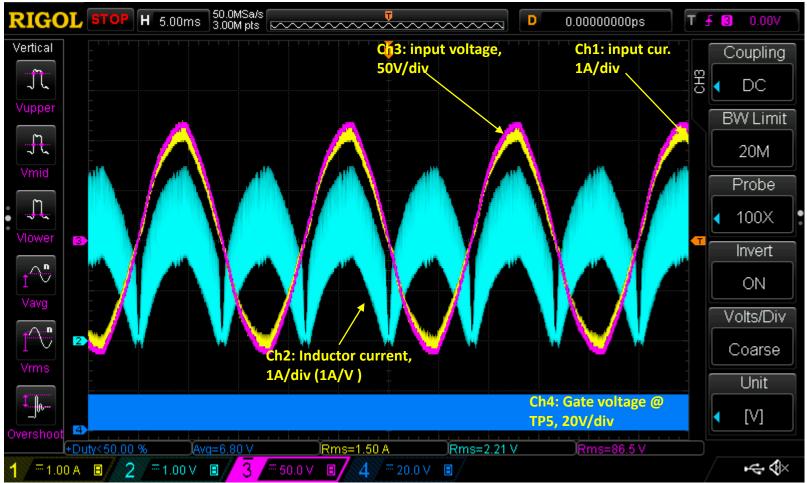
With 2x original inductor, 60W output power, distortions at 220Vac, Vff=3.79V w/ DVM



L1, Q5, Q6 on PSB removed, 120W external load across the DC-link

## 2pc of original boost inductors in series (1.36mH total), 10nF cap on PKLMT pin14 to GND, see slide 107 for modifications

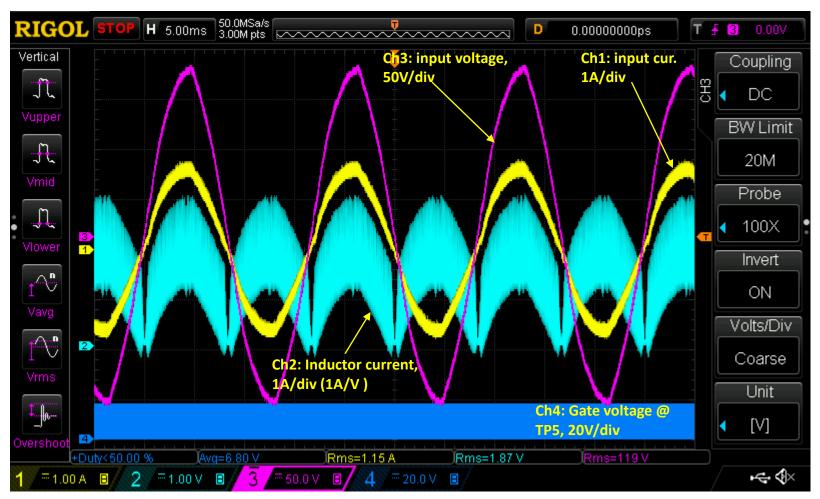
With 2x original inductor, 120W output power, no distortions at 85Vac; (Vdc\_out=355V maybe due to 2x input inductor and low input voltage)



L1, Q5, Q6 on PSB removed, 120W external load across the DC-link

2pc of original boost inductors in series (1.36mH total), 10nF cap on PKLMT pin14 to GND, see slide 107 for modifications

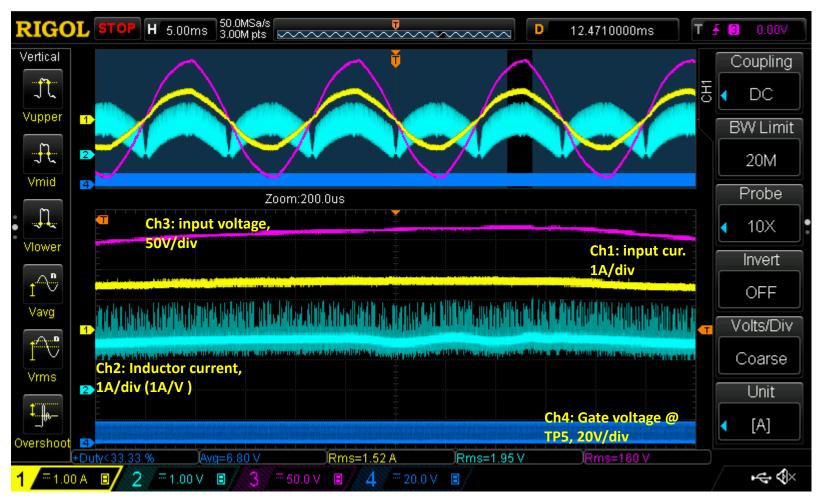
With 2x original inductor, 120W output power, no distortions at 120Vac, Vdc\_out=380V



L1, Q5, Q6 on PSB removed, 120W external load across the DC-link

2pc of original boost inductors in series (1.36mH total), 10nF cap on PKLMT pin14 to GND, see slide 107 for modifications

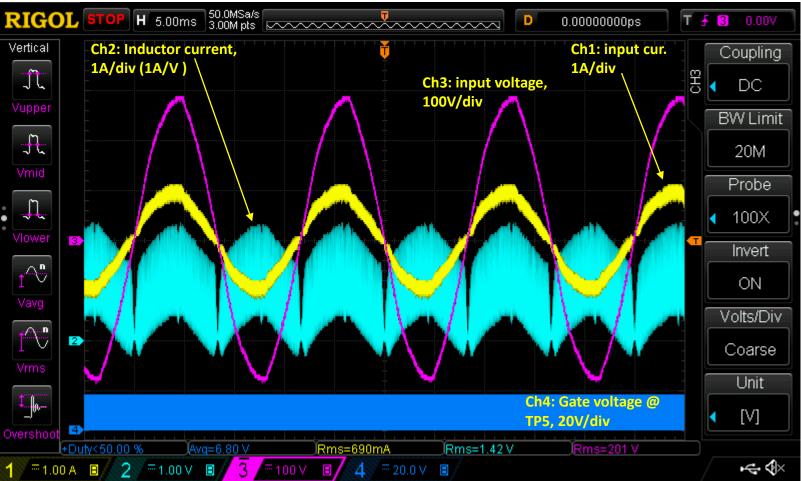
With 2x original inductor, 120W output power, no distortions at 120Vac, Vdc\_out=380V



L1, Q5, Q6 on PSB removed, 120W external load across the DC-link

2pc of original boost inductors in series (1.36mH total), 10nF cap on PKLMT pin14 to GND, see slide 107 for modifications

With 2x original inductor, 120W output power, no distortions at 200Vac, Vdc\_out=380V Pin=0.69Arms\*200Vrms=138W



L1, Q5, Q6 on PSB removed, 120W external load across the DC-link

2pc of original boost inductors in series (1.36mH total), 10nF cap on PKLMT pin14 to GND, see slide 107 for modifications

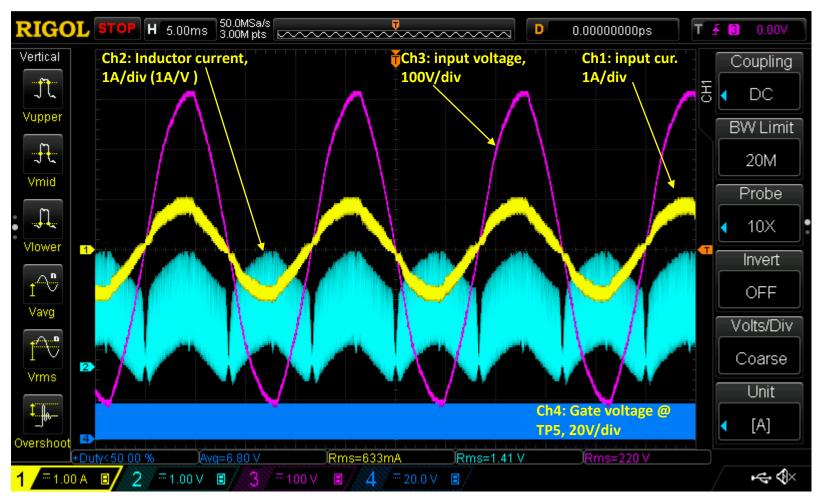
With 2x original inductor, 120W output power, no distortions at 200Vac, no pulse dropping, Vdc\_out=380V



L1, Q5, Q6 on PSB removed, 120W external load across the DC-link

2pc of original boost inductors in series (1.36mH total), 10nF cap on PKLMT pin14 to GND, see slide 107 for modifications

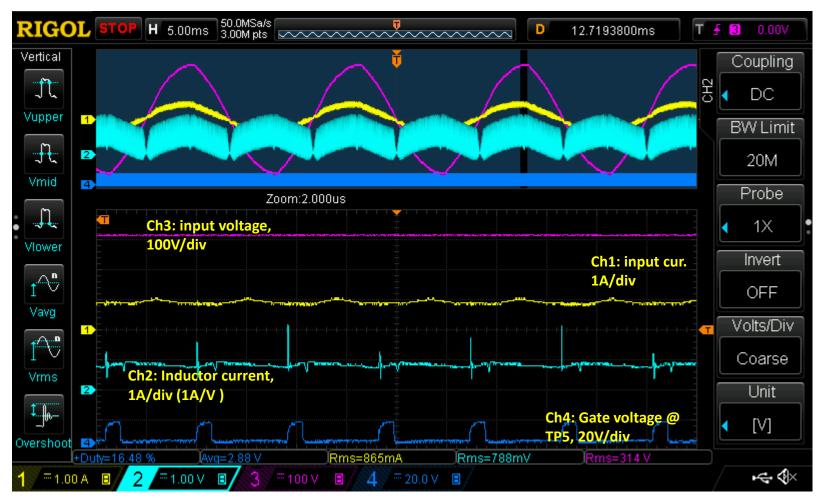
With 2x original inductor, 120W output power, no distortions at 220Vac, no pulse dropping, Vdc\_out=380V



L1, Q5, Q6 on PSB removed, 120W external load across the DC-link

2pc of original boost inductors in series (1.36mH total), 10nF cap on PKLMT pin14 to GND, see slide 107 for modifications

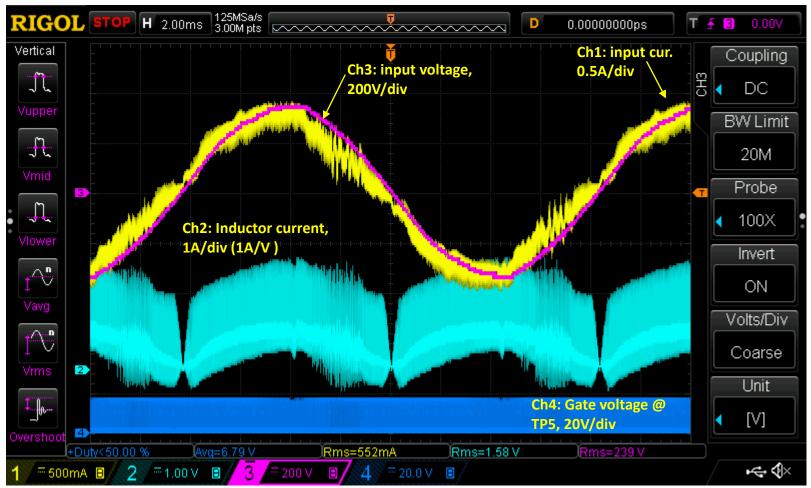
With 2x original inductor, 120W output power, no distortions at 220Vac, no pulse dropping, Vdc\_out=380V



L1, Q5, Q6 on PSB removed, 120W external load across the DC-link

# **2pc of original boost inductors in series (1.36mH total),** 10nF cap on PKLMT pin14 to GND, see slide 107 for modifications

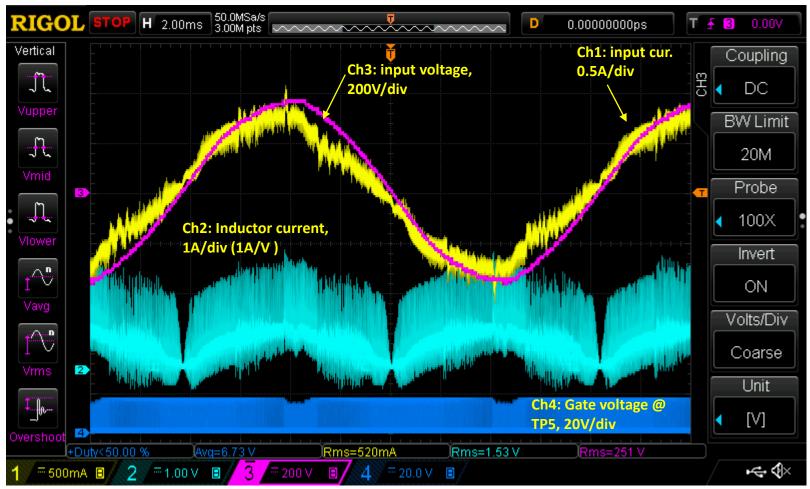
With 2x original inductor, 120W output power, no major distortions at 240Vac, however it appears like the distortions begin to start, Vdc\_out=380V



L1, Q5, Q6 on PSB removed, 120W external load across the DC-link

# **2pc of original boost inductors in series (1.36mH total),** 10nF cap on PKLMT pin14 to GND, see slide 107 for modifications

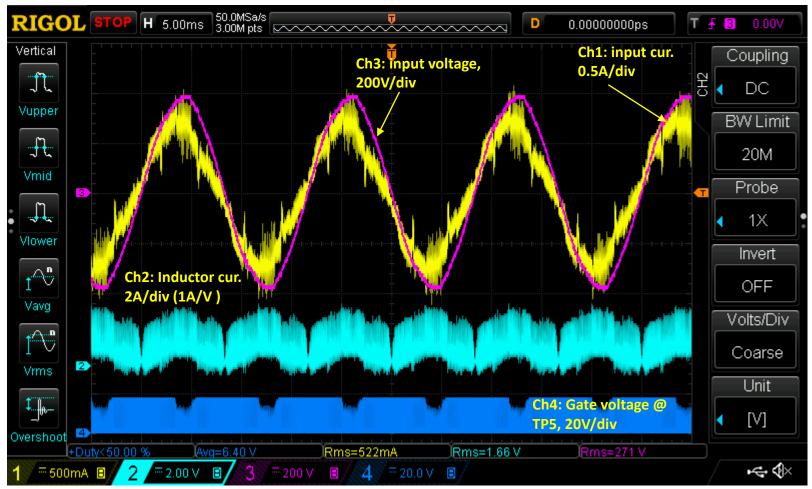
With 2x original inductor, 120W output power, no major distortions at 250Vac, however it appears like the distortions are a bit more than 240V case, Vdc\_out=380V



L1, Q5, Q6 on PSB removed, 120W external load across the DC-link

# 2pc of original boost inductors in series (1.36mH total), 10nF cap on PKLMT pin14 to GND, see slide 107 for modifications

With 2x original inductor, 120W output power, no major distortions at 265Vac, however it appears like the distortions are a bit more than 250V case, Vdc\_out=380V



Note: Input voltage is measured as 271Vac with differential probe and 265Vac with a DVM

L1, Q5, Q6 on PSB removed, 120W external load across the DC-link

# 2pc of original boost inductors in series (1.36mH total), 10nF cap on PKLMT pin14 to GND, see slide 107 for modifications

With 2x original inductor, 120W output power, no major distortions at 265Vac, pulse dropping observed, Vdc\_out=380V



Pulse dropping observed

L1, Q5, Q6 on PSB removed, **120W external load across the DC-link** 

2pc of original boost inductors in series (1.36mH total), 10nF cap on PKLMT pin14 to GND, see slide 107 for modifications

With 2x original inductor, 120W output power, when DMM is connected to pin 19 for Vff, more distortions observed at 265Vac, Vdc\_out=380V



L1, Q5, Q6 on PSB removed, **120W external load across the DC-link** 

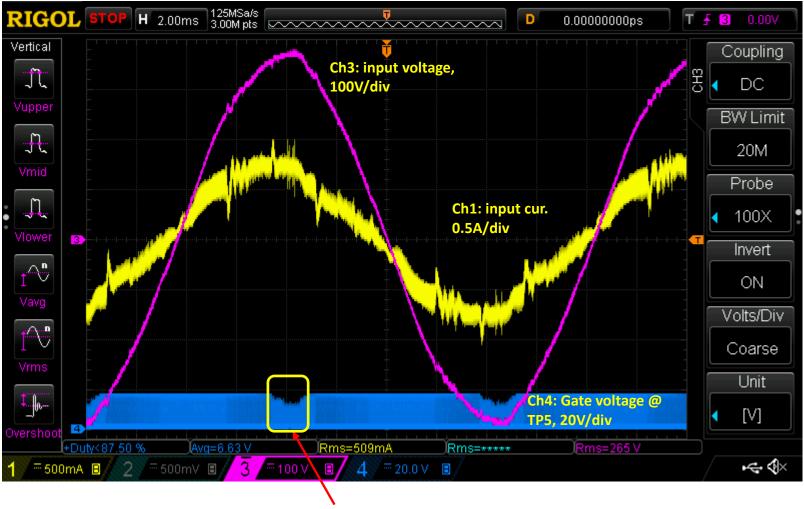
**2pc of original boost inductors in series (1.36mH total),** 10nF cap on PKLMT pin14 to GND, see slide 107 for modifications

Input voltage (Vrms)	Vff @ pin19 (Vdc) w/ DVM		
120	2.08		
200	3.50		
220	3.90		
264	4.51		

L1, Q5, Q6 on PSB removed, **120W external load across the DC-link** 

**2pc of original boost inductors in series (1.36mH total),** 10nF cap on PKLMT pin14 to GND, see slide 107 for modifications

With 2x original inductor, 120W output power, no DMM on pin 19 for Vff, minor distortions observed at 265Vac, Vdc out=380V



Pulse dropping observed

L1, Q5, Q6 on PSB removed, 120W external load across the DC-link

# 2pc of original boost inductors in series (1.36mH total), 10nF cap on PKLMT pin14 to GND, see slide 107 for modifications

With 2x original inductor, 120W output power, no DMM on pin 19 for Vff, minor distortions observed at 265Vac, Vdc\_out=380V



Very small duty cycle however no pulse dropping at the peak of sine wave

L1, Q5, Q6 on PSB removed, **120W external load across the DC-link** 

# 2pc of original boost inductors in series (1.36mH total), 10nF cap on PKLMT pin14 to GND, see slide 107 for modifications

With 2x original inductor, 120W output power, no DMM on pin 19 for Vff, minor distortions observed at 265Vac, Vdc\_out=380V

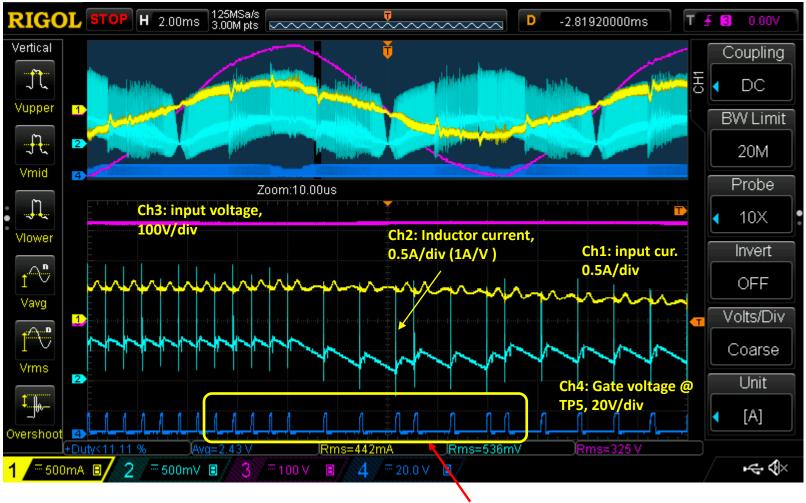


Pulse dropping observed

L1, Q5, Q6 on PSB removed, 120W external load across the DC-link

2pc of original boost inductors in series (1.36mH total), 10nF cap on PKLMT pin14 to GND, see slide 107 for modifications

With 2x original inductor, 120W output power, no DMM on pin 19 for Vff, minor distortions observed at 265Vac, Vdc\_out=380V



Pulse dropping observed

L1, Q5, Q6 on PSB removed, 30W external load across the DC-link

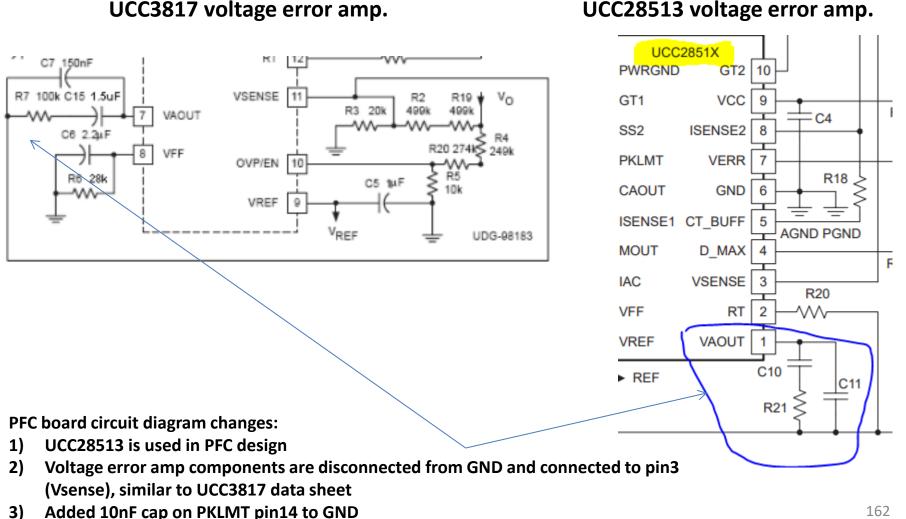
2pc of original boost inductors in series (1.36mH total), 10nF cap on PKLMT pin14 to GND, see slide 107 for modifications

# **Conclusions:**

- With 2x original inductors, current distortions were not observed up to 200Vac with 30W load on 380Vdc output. Periodic distortions started above ~210Vac
- With 2x original inductors, current distortions were not observed up to 200Vac with 60W load on 380Vdc output. Periodic distortions started above ~220Vac
- 3) With 2x original inductors, current distortions were not observed up to 250Vac with 120W load on 380Vdc output. Periodic but a lot smaller distortions started above ~ 250Vac. Similar small distortions observed at 265Vac
- 4) Connecting DMM on pin19 resulted in a bit more distortions at high voltages in general. No DMM was connected to pin19 unless needed.
- 5) With 2x original inductors and 85Vac, output voltage was at 355V (instead of 380). Output was constant at 380V above ~100Vrms input.
- 6) It appears like the current distortions at high voltages are related with the performance of current regulator as unit transitions between DCM and CCM modes

Unstable DC-link voltage investigation, 8/6/2023

Following pages describe the changes made to PFC stage in order to mitigate current distortions:



UCC3817 voltage error amp.

3)

# Measuring inductor current vs gate voltages, 8/6/2023

RefDes on UCC28513	RefDes in Listen	РСВ	Values on 6/25/2023
R2	R43		0.47
-	R60	PSB-04	22.1K
-	R44/R49	-	562K
-	R47/R50	-	383K
R14	R13		10К
R7	R5		1.62K
R12	R4		3k (3.16k//56k)
C7	C8	PFC-03	330p
C6	C6		4.9nF (1.6n+3.3n)
R13	R10		3.23k (3.3k//150k)
R8	R9		3k (3.16k//56k)
R15	R11	-	28K (56k//56k)
C8	С9		2uF (1uF//1uF)
C11	C2		150n
C10	C1		1.5uF
R21	R1		100K

In addition:

- 10nF cap added from PKLMT pin14 to GND on PFC card.
- PFC inductor (L2) is replaced with TSD-5033 (w/o base)
- Sense resistor on PSB (R43) part number: MOSX5CR47J



Old PFC inductor (L2) w/ overlapping windings 625uH @ 4.8A

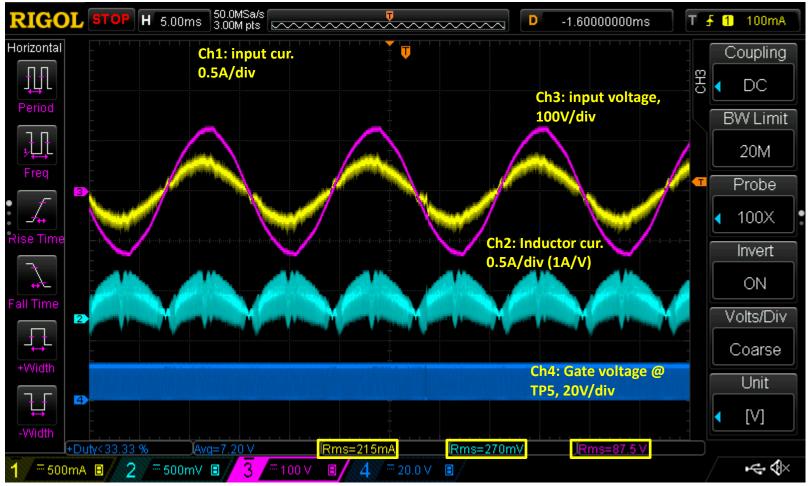


New toroidal PFC inductor (L2) w/o overlapping windings 750uH @ 8A

L1, Q5, Q6 on PSB are removed, R43 is 0.47Ω (PN: MOSX5CR47J), boost inductor is TSD-5033 and 6" away from PSB See slides 162 and 163 for circuit configuration

At 85Vac, 12.5K across DC-link:

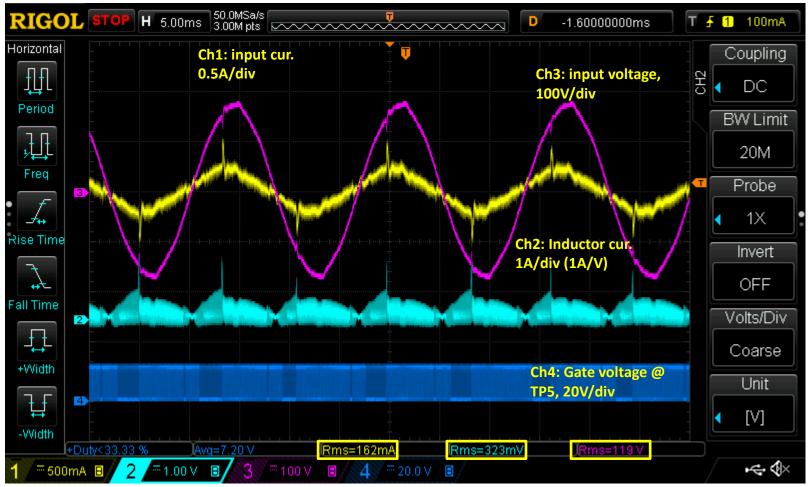
output=387Vdc, input cur. = 0.215Arms, inductor cur. = 0.282Arms, Sin=18.27VA (good PF)



L1, Q5, Q6 on PSB are removed, R43 is 0.47Ω (PN: MOSX5CR47J), boost inductor is TSD-5033 and 6" away from PSB See slides 162 and 163 for circuit configuration

At 120Vac, 12.5K across DC-link:

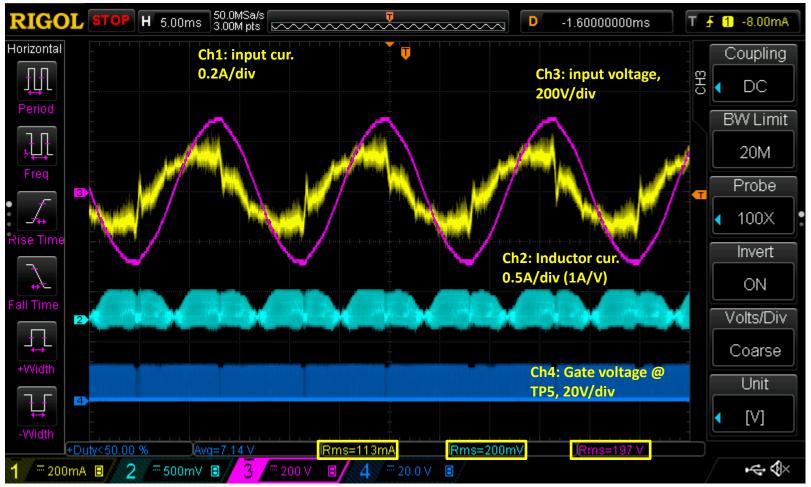
output=389Vdc, input cur. = 0.162Arms, inductor cur. = 0.323Arms, Sin=19.4VA (OK PF)



L1, Q5, Q6 on PSB are removed, R43 is 0.47Ω (PN: MOSX5CR47J), boost inductor is TSD-5033 and 6" away from PSB See slides 162 and 163 for circuit configuration

At 200Vac, 12.5K across DC-link:

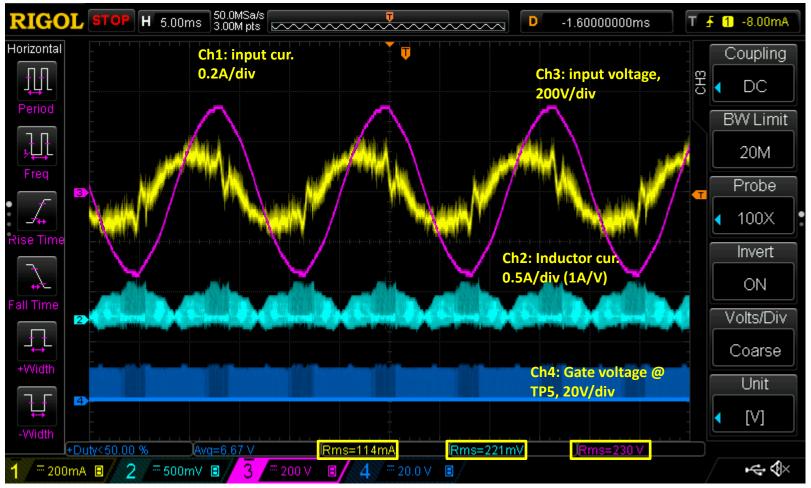
output=388Vdc, input cur. = 0.113Arms, inductor cur. = 0.200Arms, Sin=22.6VA (poor PF)



L1, Q5, Q6 on PSB are removed, R43 is 0.47Ω (PN: MOSX5CR47J), boost inductor is TSD-5033 and 6" away from PSB See slides 162 and 163 for circuit configuration

At 230Vac, 12.5K across DC-link:

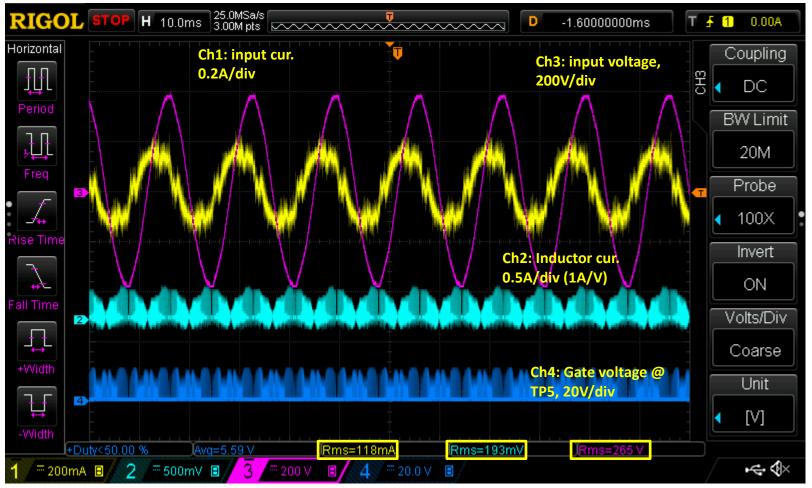
output=388Vdc, input cur. = 0.114Arms, inductor cur. = 0.221Arms, Sin=26.2VA (poor PF)



L1, Q5, Q6 on PSB are removed, R43 is 0.47Ω (PN: MOSX5CR47J), boost inductor is TSD-5033 and 6" away from PSB See slides 162 and 163 for circuit configuration

At 265Vac, 12.5K across DC-link:

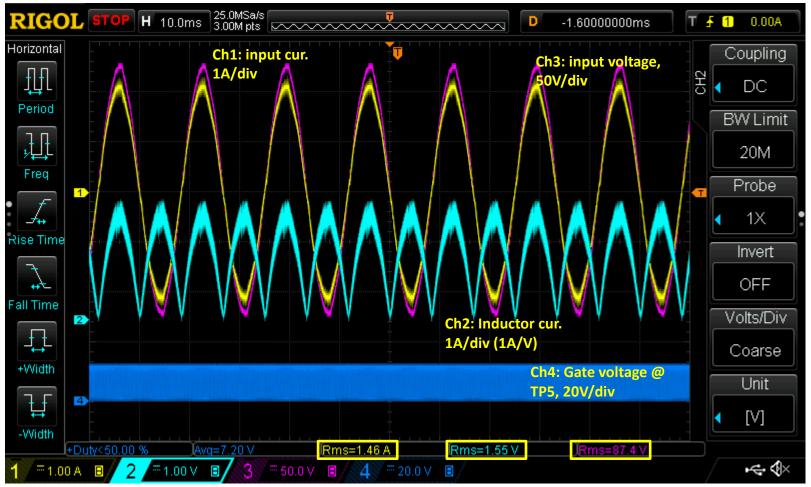
output=388Vdc, input cur. = 0.118Arms, inductor cur. = 0.193Arms, Sin=31.2VA (poor PF)



L1, Q5, Q6 on PSB are removed, R43 is 0.47Ω (PN: MOSX5CR47J), boost inductor is TSD-5033 and 6" away from PSB See slides 162 and 163 for circuit configuration

At 85Vac, 1.149K across DC-link:

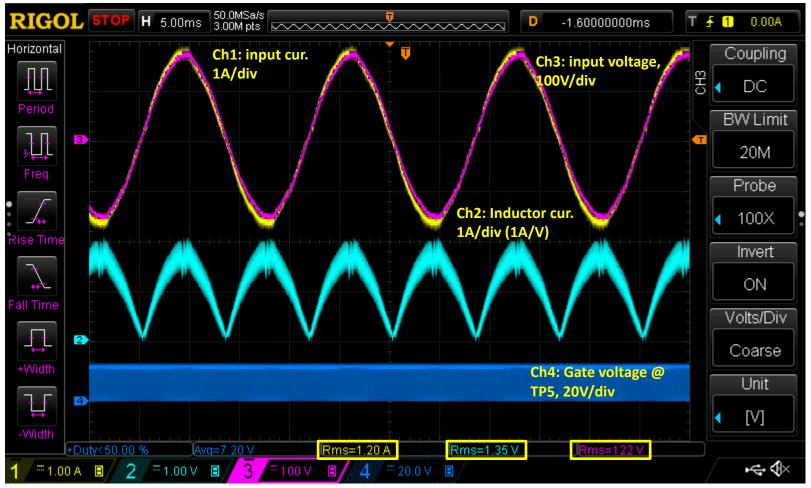
output=360Vdc, input cur. = 1.46Arms, inductor cur. = 1.55Arms, Sin=124VA (good PF)



L1, Q5, Q6 on PSB are removed, R43 is 0.47Ω (PN: MOSX5CR47J), boost inductor is TSD-5033 and 6" away from PSB See slides 162 and 163 for circuit configuration

At 120Vac, 1.149K across DC-link:

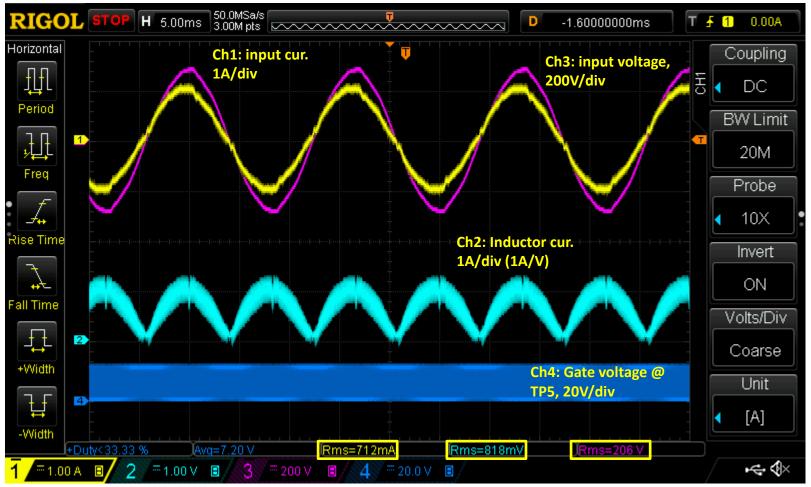
output=373Vdc, input cur. = 1.20Arms, inductor cur. = 1.35Arms, Sin=144VA (good PF)



L1, Q5, Q6 on PSB are removed, R43 is 0.47Ω (PN: MOSX5CR47J), boost inductor is TSD-5033 and 6" away from PSB See slides 162 and 163 for circuit configuration

At 200Vac, 1.149K across DC-link:

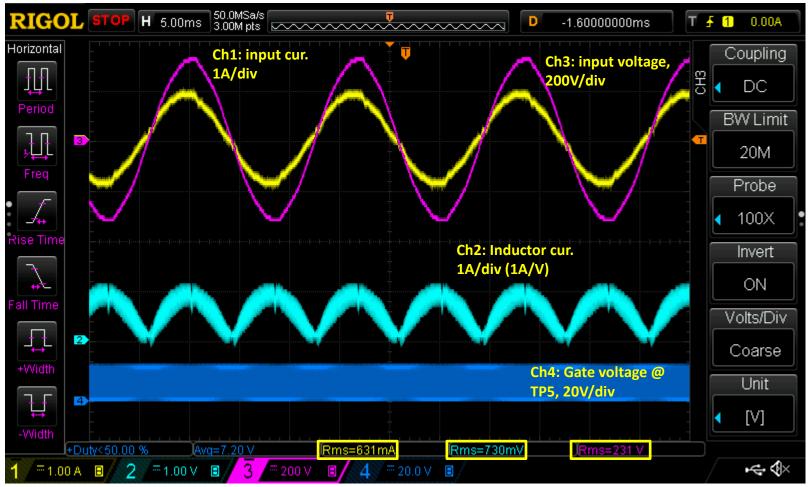
output=381Vdc, input cur. = 0.712Arms, inductor cur. = 0.818Arms, Sin=142.4VA (good PF)



L1, Q5, Q6 on PSB are removed, R43 is 0.47Ω (PN: MOSX5CR47J), boost inductor is TSD-5033 and 6" away from PSB See slides 162 and 163 for circuit configuration

At 230Vac, 1.149K across DC-link:

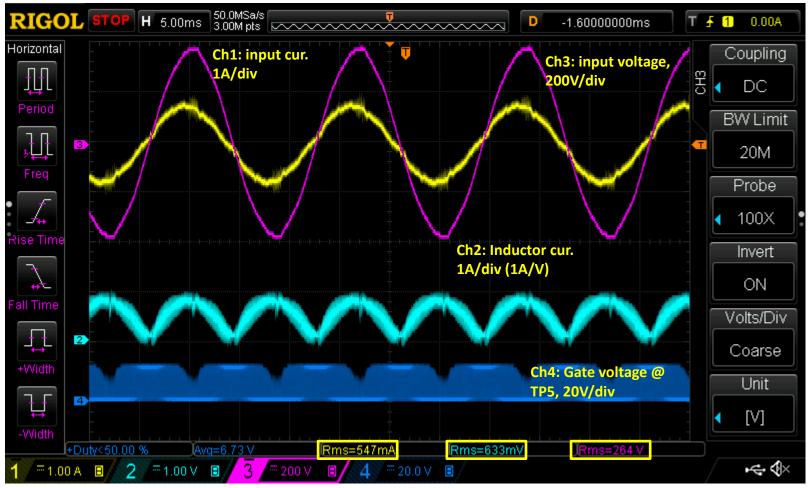
output=382Vdc, input cur. = 0.631Arms, inductor cur. = 0.73Arms, Sin=145.1VA (good PF)



L1, Q5, Q6 on PSB are removed, R43 is 0.47Ω (PN: MOSX5CR47J), boost inductor is TSD-5033 and 6" away from PSB See slides 162 and 163 for circuit configuration

At 265Vac, 1.149K across DC-link:

output=380Vdc, input cur. = 0.547Arms, inductor cur. = 0.633Arms, Sin=144.9VA (good PF)



# Measuring inductor current vs gate voltages, 8/6/2023 PSB-04, PFC-03, CONT A w/ PFC board ,SN: AG155544221261437 L1, Q5, Q6 on PSB are removed, R43 is 0.47Ω (PN: MOSX5CR47J), boost inductor is TSD-5033 and 6" away from PSB See slides 162 and 163 for circuit configuration

# Summary of testing PFC stage input current distortions with min/max resistive loads across the DC-link

- By removing L1, Q5, Q6 on PSB, only the PFC stage was tested w/o secondary stage power supply board
- By using larger toroidal inductor, the current distortions observed earlier were mostly eliminated
- Turn-on current spikes were reduced, this is visible in inductor current measurements
- At min load from 85Vac-265Vac, good DC-link regulation was achieved
- At max output load and low AC voltage, the DC-link voltage was less than the set point of 390V

Dc-Link load (kΩ)	Input voltage (Vrms) By using Diff Probe	DC-link w/ DVM (Vdc)	Input current (Arms)	Inductor current (Arms)	Input power (VA)	Comments
12.5 Min load	85	387	0.215	0.282	18.27	OK PF, no major distortions
	120	389	0.162	0.323	19.40	OK PF, minor distortions
	200	388	0.113	0.200	22.60	
	230	388	0.114	0.221	26.20	Poor PF, no major distortions
	265	388	0.118	0.193	31.20	
	→ 85	371	1.57	1.65	124.0	Good PF, no distortions, lower DC- link
1.149 Max load	120	382	1.12	1.25	144.0	
	200	382	0.677	0.769	142.2	Good PF, no distortions
	230	388	0.599	0.679	145.1	
	265	389	0.525	0.600	144.9	

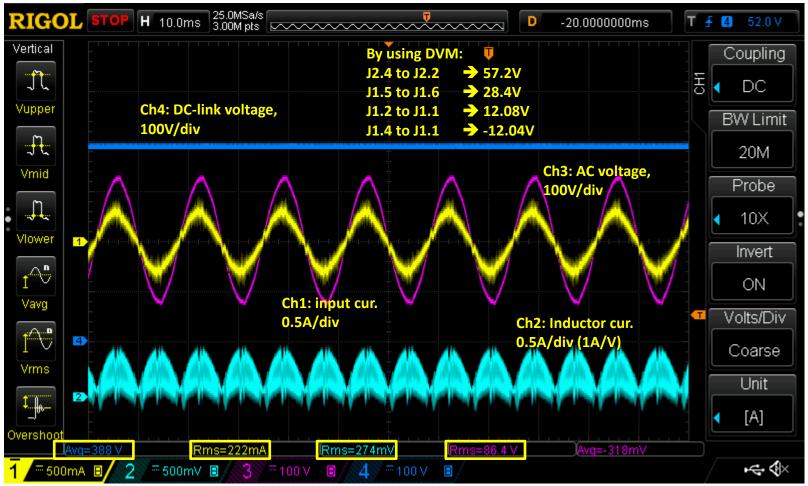
Measuring inductor current vs gate voltages, 8/6/2023 PSB-04, PFC-03, CONT A w/ PFC board ,SN: AG155544221261437 L1, Q5, Q6 (PN: IRFPC50A) on PSB **are installed**, R43=0.47Ω (PN:MOSX5CR47J), boost ind. is TSD-5033 and 6" away from PSB See slides 162 and 163 for circuit configuration

# Following slides show the test results by enabling the secondary stage DC/DC converter (L1, Q5, Q6 (PN: IRFPC50A) on PSB are installed)

L1, Q5, Q6 (PN: IRFPC50A) on PSB **are installed**, R43=0.47Ω (PN:MOSX5CR47J), boost ind. is TSD-5033 and 6" away from PSB See slides 162 and 163 for circuit configuration

At 85Vac, min loads on outputs at J1 and J2 connectors

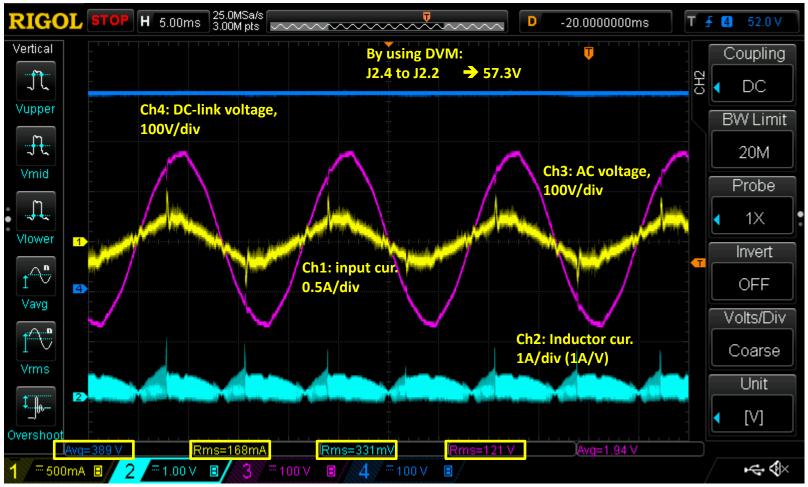
output=388Vdc, input cur. = 0.222Arms, inductor cur. = 0.274Arms, Sin=18.8VA (good PF)



L1, Q5, Q6 (PN: IRFPC50A) on PSB **are installed**, R43=0.47Ω (PN:MOSX5CR47J), boost ind. is TSD-5033 and 6" away from PSB See slides 162 and 163 for circuit configuration

At 120Vac, min loads on outputs at J1 and J2 connectors

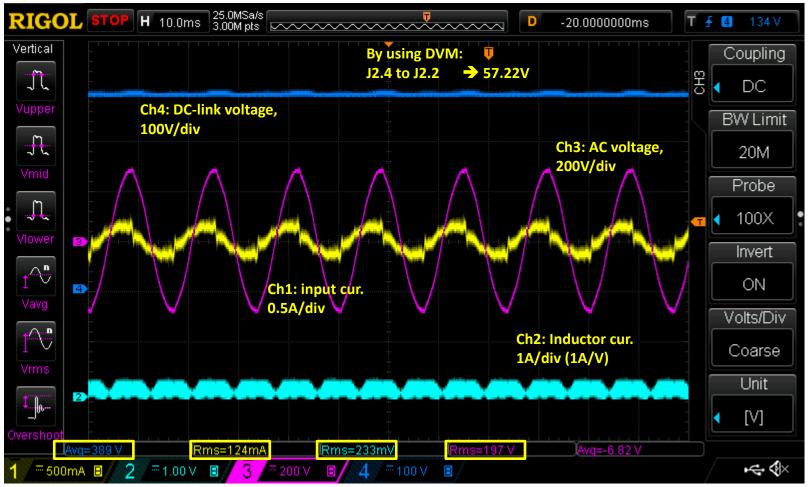
output=389Vdc, input cur. = 0.168Arms, inductor cur. = 0.331Arms, Sin=20.1VA (OK PF)



L1, Q5, Q6 (PN: IRFPC50A) on PSB **are installed**, R43=0.47Ω (PN:MOSX5CR47J), boost ind. is TSD-5033 and 6" away from PSB See slides 162 and 163 for circuit configuration

At 200Vac, min loads on outputs at J1 and J2 connectors

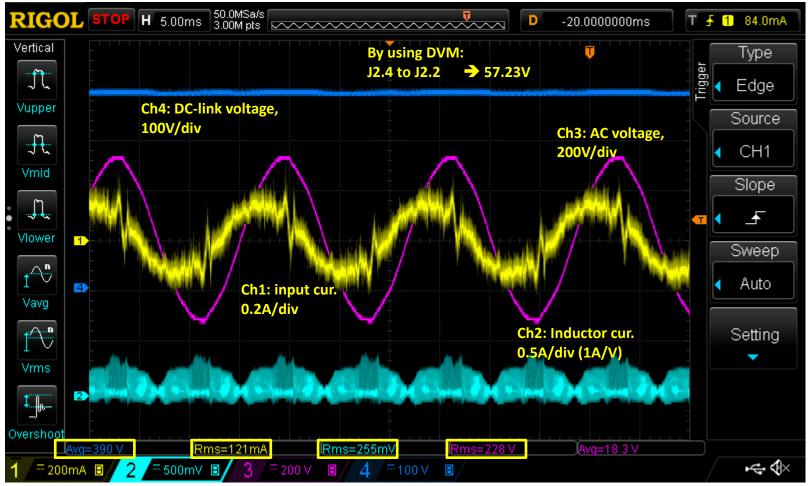
output=389Vdc, input cur. = 0.124Arms, inductor cur. = 0.233Arms, Sin=24.8VA (poor PF)



L1, Q5, Q6 (PN: IRFPC50A) on PSB **are installed**, R43=0.47Ω (PN:MOSX5CR47J), boost ind. is TSD-5033 and 6" away from PSB See slides 162 and 163 for circuit configuration

At 230Vac, min loads on outputs at J1 and J2 connectors

output=390Vdc, input cur. = 0.121Arms, inductor cur. = 0.255Arms, Sin=27.8VA (poor PF)



L1, Q5, Q6 (PN: IRFPC50A) on PSB **are installed**, R43=0.47Ω (PN:MOSX5CR47J), boost ind. is TSD-5033 and 6" away from PSB See slides 162 and 163 for circuit configuration

At 265Vac, min loads on outputs at J1 and J2 connectors

output=390Vdc, input cur. = 0.128Arms, inductor cur. = 0.238Arms, Sin=33.9VA (poor PF)



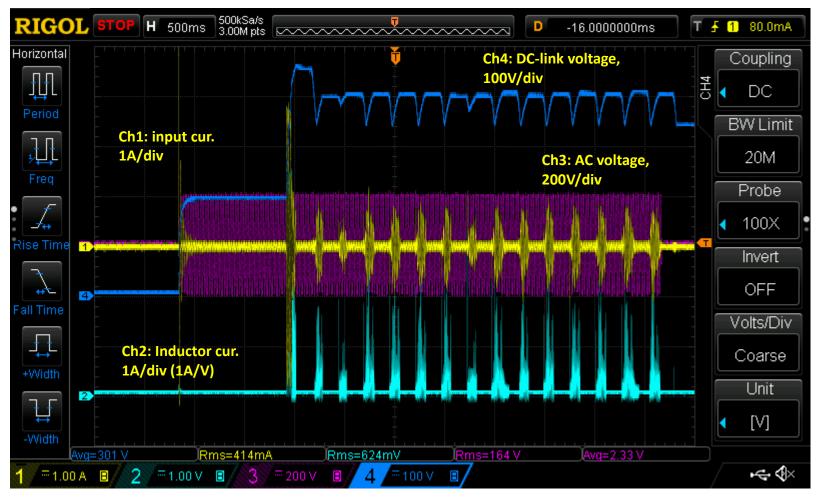
# Measuring inductor current vs gate voltages, 8/6/2023 PSB-04, PFC-03, CONT A w/ PFC board ,SN: AG155544221261437 L1, Q5, Q6 (PN: IRFPC50A) on PSB **are installed**, R43=0.47Ω (PN:MOSX5CR47J), boost ind. is TSD-5033 and 6" away from PSB See slides 162 and 163 for circuit configuration

# With minimum resistive load on secondary stage DC/DC converter, from 85Vac to 265Vac input voltage, stable DC-link voltage regulation and distortion free PFC stage input currents are obtained

Dc-Link load (kΩ)	Input voltage (Vrms) By using Diff Probe	DC-link w/ DVM (Vdc)	Input current (Arms)	Inductor current (Arms)	Input power (VA)	Comments
	85	388	0.220	0.274	18.70	OK PF, no major distortions
	120	389	0.171	0.316	20.52	OK PF, minor distortions
12.5	200	389	0.124	0.233	24.80	
	230	390	0.121	0.255	27.83	Poor PF, no major distortions
	265	390	0.128	0.238	33.92	

L1, Q5, Q6 (PN: IRFPC50A) on PSB **are installed**, R43=0.47Ω (PN:MOSX5CR47J), boost ind. is TSD-5033 and 6" away from PSB See slides 162 and 163 for circuit configuration

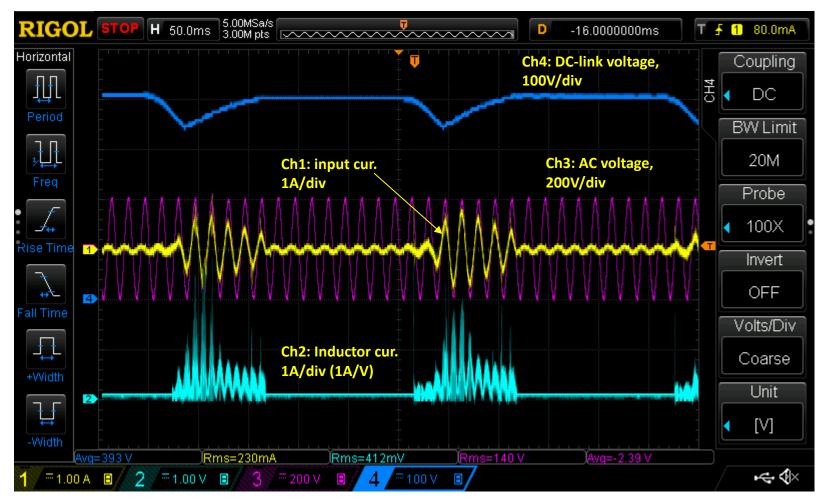
At ~120Vac, max loads on outputs at J1 and J2 connectors



DC-link voltage regulation does not work with max output power

L1, Q5, Q6 (PN: IRFPC50A) on PSB **are installed**, R43=0.47Ω (PN:MOSX5CR47J), boost ind. is TSD-5033 and 6" away from PSB See slides 162 and 163 for circuit configuration

At ~140Vac, max loads on outputs at J1 and J2 connectors

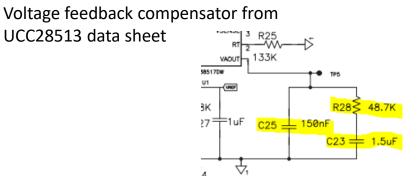


With output dc/dc converter and max load is connected on J1/J2 connectors, the DC-link voltage regulation is not stable.

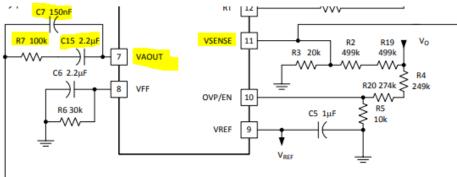
L1, Q5, Q6 (PN: IRFPC50A) on PSB **are installed**, R43=0.47Ω (PN:MOSX5CR47J), boost ind. is TSD-5033 and 6" away from PSB See slides 162 and 163 for circuit configuration

Conclusions:

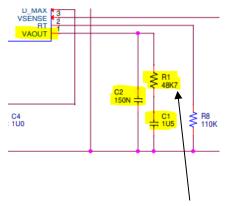
- With PFC stage only, without secondary stage DC/DC converter, at min AC voltage and max load on DClink, the DC-link voltage was lower than the set point (360V vs 390V)
- With PFC stage followed by secondary stage DC/DC converter, at low AC voltages and max load on dc/dc converter, the DC-link voltage was not stable and had oscillations.
- Below are the voltage feedback circuit used in the design:



UCC3817 voltage feedback circuit shown for reference



Voltage feedback compensator used in PFC board (prior to modifications shown on slides 162/163)



Changed to 100K per slides 162/163