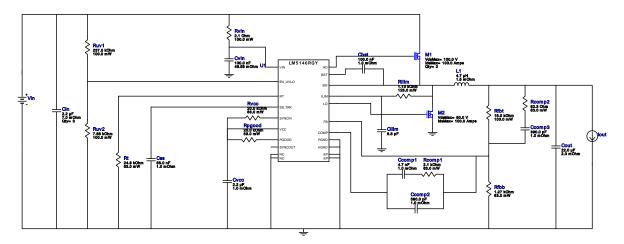
VinMin = 48.0V VinMax = 52.0V Vout = 12.0V lout = 13.0A Device = LM5146RGYR Topology = Buck Created = 2021-10-28 02:22:05.341 BOM Cost = \$7.78 BOM Count = 28 Total Pd = 4.28W

WEBENCH® Design Report

Design: 17 LM5146RGYR LM5146RGYR 48V-52V to 12.00V @ 13A



1. This regulator device is qualified for Automotive applications. All passives and other components selected in this design may not be qualified for Automotive applications. The user is required to verify that all components in the design meet the qualification and safety requirements for their specific application. View WEBENCH(R) Disclaimer.

Design Alerts

Component Selection Information

Please note that since parallel FETs have been chosen in this design, schematic and PCB export features will not work

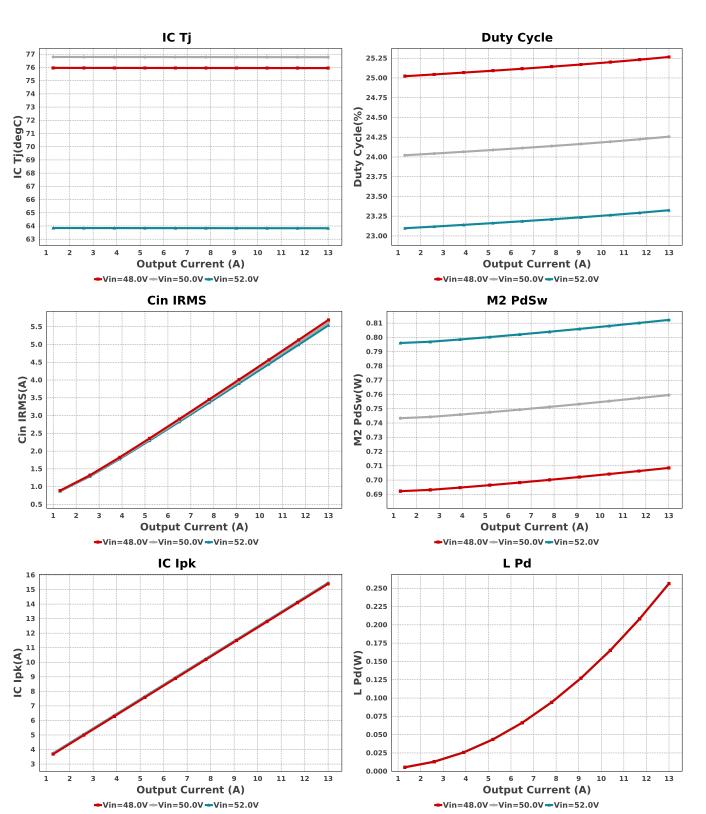
Electrical BOM

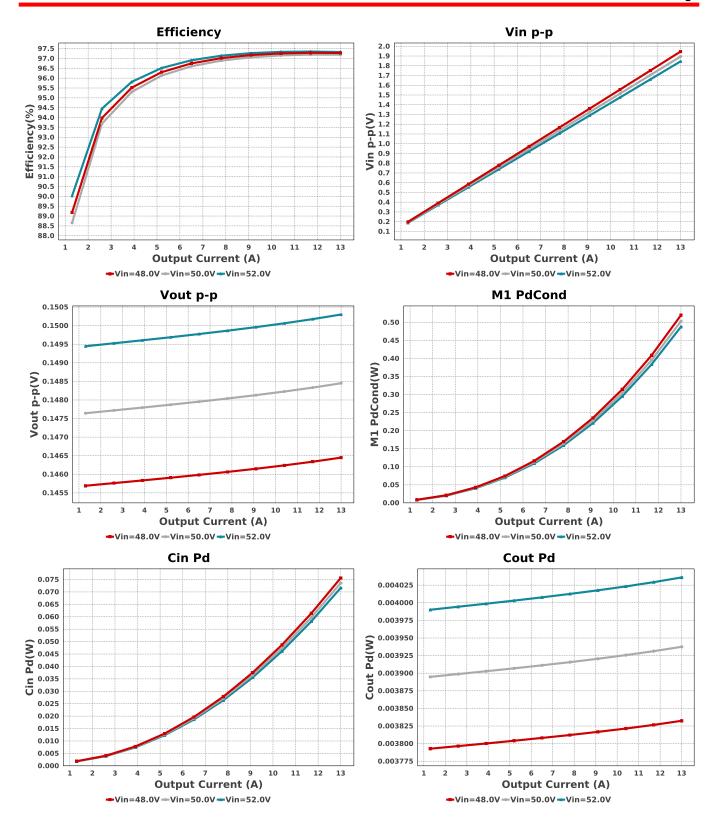
Name Manufacturer		Part Number	Properties	Qty	Price	Footprint
Cbst	Kemet	C0603C104Z3VACTU Series= Y5V	Cap= 100.0 nF ESR= 1.0 mOhm VDC= 25.0 V IRMS= 0.0 A	1	\$0.01	0603 5 mm ²
Ccomp1	MuRata	GRM155R71C472KA01D Series= X7R	Cap= 4.7 nF ESR= 1.0 mOhm VDC= 16.0 V IRMS= 0.0 A	1	\$0.01	0402 3 mm ²
Ccomp2	MuRata	GRM155R71H391KA01D Series= X7R	Cap= 390.0 pF ESR= 1.0 mOhm VDC= 50.0 V IRMS= 0.0 A	1	\$0.01	0402 3 mm ²
Ccomp3	MuRata	GRM155R71H391KA01D Series= X7R	Cap= 390.0 pF ESR= 1.0 mOhm VDC= 50.0 V IRMS= 0.0 A	1	\$0.01	0402 3 mm ²
Cilim	AVX	06031U6R8BAT2A Series= C0G/NP0	Cap= 6.8 pF VDC= 100.0 V IRMS= 0.0 A	1	\$0.07	0603 5 mm ²
Cin	MuRata	GRM32ER72A225KA35L Series= X7R	Cap= 2.2 uF ESR= 7.0 mOhm VDC= 100.0 V IRMS= 4.4 A	3	\$0.63	1210 15 mm ²
Cout	MuRata	GRM32ER61E226KE15L Series= X5R	Cap= 22.0 uF ESR= 2.0 mOhm VDC= 25.0 V IRMS= 3.67 A	1	\$0.65	1210 15 mm ²

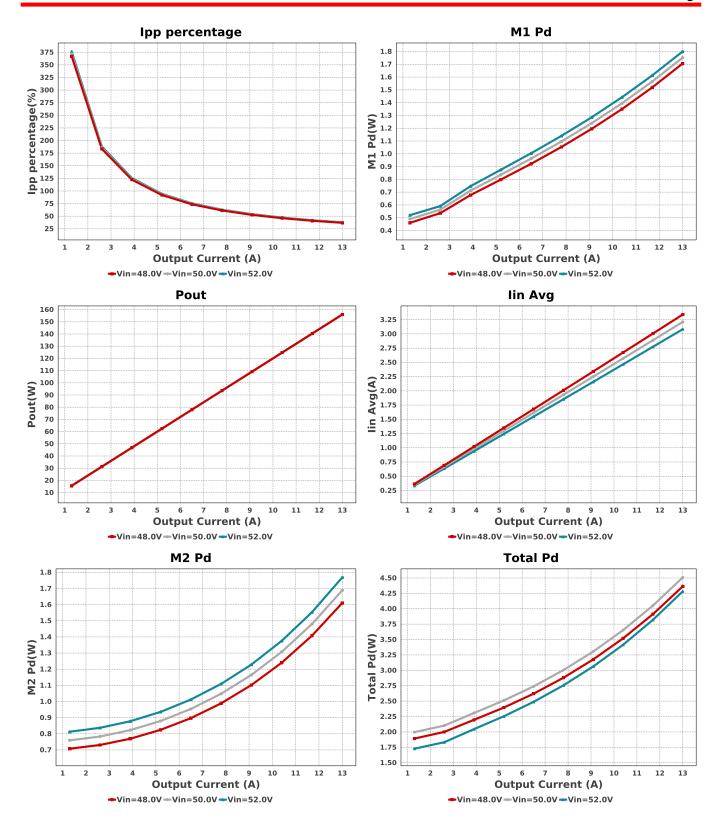
Name	Manufacturer	Part Number	Properties	Qty	Price	Footprint
Css	MuRata	GRM155R71C563KA88D Series= X7R	Cap= 56.0 nF ESR= 1.0 mOhm VDC= 16.0 V IRMS= 0.0 A	1	\$0.01	0402 3 mm ²
Cvcc	TDK	C1005X5R1V225K050BC Series= X5R	Cap= 2.2 uF ESR= 1.0 mOhm VDC= 35.0 V IRMS= 0.0 A	1	\$0.07	0402_065 3 mm ²
Cvin	TDK	C1608X7S2A104K080AB Series= X7S	Cap= 100.0 nF ESR= 49.59 mOhm VDC= 100.0 V IRMS= 751.62 mA	1	\$0.03	0603 5 mm ²
L1	Coilcraft	SER2915L-472KL	L= 4.7 μH 1.5 mOhm	1	\$1.88	
M1	Texas Instruments	CSD19534Q5A	VdsMax= 100.0 V IdsMax= 100.0 Amps	2	\$0.34	SER2915L 652 mm² TRANS_NexFET_Q5A 55 mm²
M2	Infineon Technologies	BSC037N08NS5ATMA1	VdsMax= 80.0 V IdsMax= 100.0 Amps	1	\$1.06	PG-TDSON-8 55 mm ²
Rcomp1	Vishay-Dale	CRCW04022K10FKED Series= CRCWe3	Res= 2.1 kOhm Power= 63.0 mW Tolerance= 1.0%	1	\$0.01	0402 3 mm ²
Rcomp2	Vishay-Dale	CRCW040252R3FKED Series= CRCWe3	Res= 52.3 Ohm Power= 63.0 mW Tolerance= 1.0%	1	\$0.01	0402 3 mm ²
Rfbb	Vishay-Dale	CRCW04021K27FKED Series= CRCWe3	Res= 1.27 kOhm Power= 63.0 mW Tolerance= 1.0%	1	\$0.01	0402 3 mm ²
Rfbt	Yageo	RC0603FR-0718KL Series=?	Res= 18.0 kOhm Power= 100.0 mW Tolerance= 1.0%	1	\$0.01	0603 5 mm ²
Rilim	Vishay-Dale	CRCW08051K13FKEA Series= CRCWe3	Res= 1.13 kOhm Power= 125.0 mW Tolerance= 1.0%	1	\$0.01	0805 7 mm ²
Rpgood	Vishay-Dale	CRCW040220K0FKED Series= CRCWe3	Res= 20.0 kOhm Power= 63.0 mW Tolerance= 1.0%	1	\$0.01	0402 3 mm ²
Rt	Vishay-Dale	CRCW040224K9FKED Series= CRCWe3	Res= 24.9 kOhm Power= 63.0 mW Tolerance= 1.0%	1	\$0.01	0402 3 mm ²
Ruv1	Vishay-Dale	CRCW0603237KFKEA Series= CRCWe3	Res= 237.0 kOhm Power= 100.0 mW Tolerance= 1.0%	1	\$0.01	0603 5 mm ²
Ruv2	Yageo	RC0603FR-077K68L Series= ?	Res= 7.68 kOhm Power= 100.0 mW Tolerance= 1.0%	1	\$0.01	0603 5 mm ²
Rvcc	Vishay-Dale	CRCW040220K0FKED Series= CRCWe3	Res= 20.0 kOhm Power= 63.0 mW Tolerance= 1.0%	1	\$0.01	0402 3 mm ²

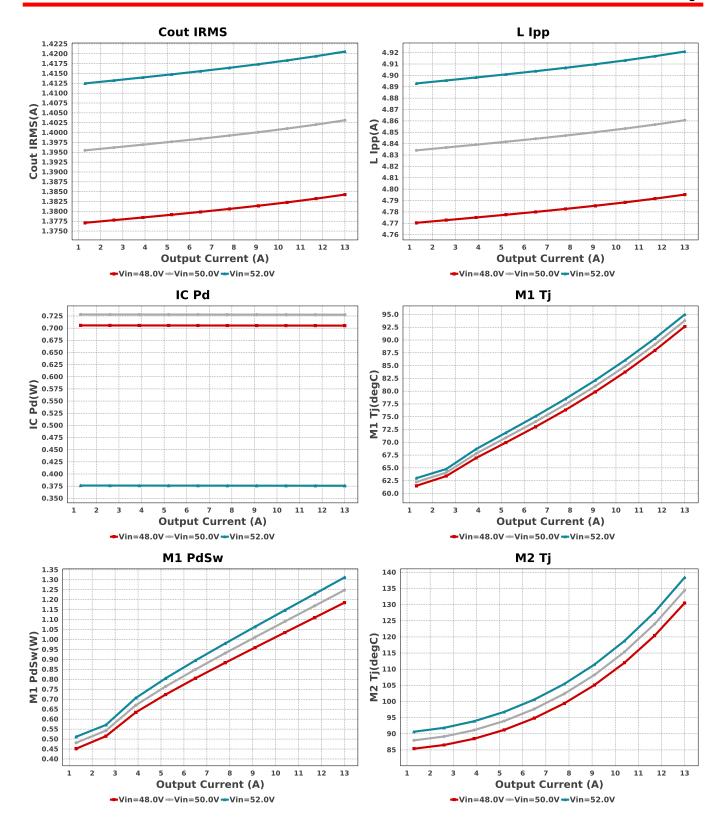
Name	Manufacturer	Part Number	Properties	Qty	Price	Footprint
Rvin	Vishay-Dale	CRCW06032R10FKEA Series= CRCWe3	Res= 2.1 Ohm Power= 100.0 mW Tolerance= 1.0%	1	\$0.01	0603 5 mm ²
U1	Texas Instruments	LM5146RGYR	Switcher	1	\$1.29	DOVEGOOD OF week

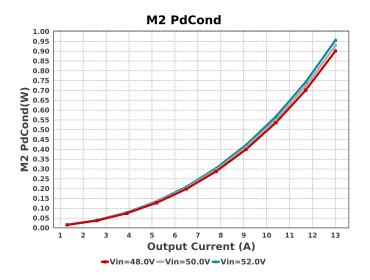


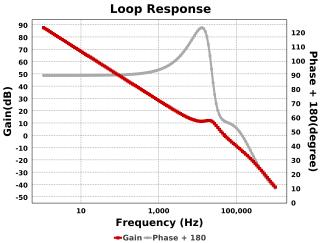












Operating Values

#	Name	Value	Category	Description
1.		5.54 A	Capacitor	Input capacitor RMS ripple current
2.	Cin Pd	71.624 mW	Capacitor	Input capacitor power dissipation
3.	Cout IRMS	1.421 A	Capacitor	Output capacitor RMS ripple current
4.	Cout Pd	4.036 mW	Capacitor	Output capacitor power dissipation
5.	IC lpk	15.46 A	IC	Peak switch current in IC
6.	IC Pd	375.81 mW	IC	IC power dissipation
7.	IC Tj	63.078 degC	IC	IC junction temperature
8.	IC Tolerance	8.0 mV	IC	IC Feedback Tolerance
9.	ICThetaJA	34.8 degC/W	IC	IC junction-to-ambient thermal resistance
10.	lin Avg	3.082 A	IC	Average input current
11.	lpp percentage	37.854 %	Inductor	Inductor ripple current percentage (with respect to average inductor current)
12.	L lpp	4.921 A	Inductor	Peak-to-peak inductor ripple current
	L Pd	256.53 mW	Inductor	Inductor power dissipation
	M1 Pd	1.8 W	Mosfet	M1 MOSFET total power dissipation
15.		487.76 mW	Mosfet	M1 MOSFET conduction losses
16.		1.312 W	Mosfet	M1 MOSFET switching losses
17.		94.989 degC	Mosfet	M1 MOSFET switching losses M1 MOSFET junction temperature
18.	,	1.768 W	Mosfet	·
	M2 PdCond			M2 MOSFET conduction losses
		956.15 mW	Mosfet	M2 MOSFET conduction losses
20.		812.27 mW	Mosfet	M2 MOSFET switching losses
	M2 Tj	138.42 degC	Mosfet	M2 MOSFET junction temperature
	Cin Pd	71.624 mW	Power	Input capacitor power dissipation
-	Cout Pd	4.036 mW	Power	Output capacitor power dissipation
	IC Pd	375.81 mW	Power	IC power dissipation
	L Pd	256.53 mW	Power	Inductor power dissipation
26.		1.8 W	Power	M1 MOSFET total power dissipation
27.	M1 PdCond	487.76 mW	Power	M1 MOSFET conduction losses
28.		1.312 W	Power	M1 MOSFET switching losses
29.		1.768 W	Power	M2 MOSFET total power dissipation
30.	M2 PdCond	956.15 mW	Power	M2 MOSFET conduction losses
31.	M2 PdSw	812.27 mW	Power	M2 MOSFET switching losses
32.	Total Pd	4.283 W	Power	Total Power Dissipation
33.	BOM Count	28	System Information	Total Design BOM count
34.	Duty Cycle	23.325 %	System Information	Duty cycle
35.	Efficiency	97.328 %	System Information	Steady state efficiency
36.	FootPrint	973.0 mm ²	System Information	Total Foot Print Area of BOM components
37.	Frequency	401.606 kHz	System Information	Switching frequency
38.	lout	13.0 A	System Information	lout operating point
39.	Mode	FCCM	System Information	Conduction Mode
40.	Pout	156.0 W	System Information	Total output power
41.	Total BOM	\$7.78	System Information	Total BOM Cost

#	Name	Value	Category	Description
42.	Vin	52.0 V	System Information	Vin operating point
43.	Vin p-p	1.835 V	System Information	Peak-to-peak input voltage
44.	Vout	12.0 V	System Information	Operational Output Voltage
45.	Vout Actual	12.139 V	System Information	Vout Actual calculated based on selected voltage divider resistors
46.	Vout Tolerance	2.906 %	System Information	Vout Tolerance based on IC Tolerance (no load) and voltage divider resistors if applicable
47.	Vout p-p	150.3 mV	System Information	Peak-to-peak output ripple voltage

Design Inputs

Name	Value	Description	
lout	13.0	Maximum Output Current	
SoftStart	4.0 ms	Soft Start Time (ms)	
VinMax	52.0	Maximum input voltage	
VinMin	48.0	Minimum input voltage	
Vout	12.0	Output Voltage	
base_pn	LM5146	Base Product Number	
source	DC	Input Source Type	
Та	50.0	Ambient temperature	
UserFsw	400.0 k	Customer Selected Frequency	

WEBENCH® Assembly

Component Testing

Some published data on components in datasheets such as Capacitor ESR and Inductor DC resistance is based on conservative values that will guarantee that the components always exceed the specification. For design purposes it is usually better to work with typical values. Since this data is not always available it is a good practice to measure the Capacitance and ESR values of Cin and Cout, and the inductance and DC resistance of L1 before assembly of the board. Any large discrepancies in values should be electrically simulated in WEBENCH to check for instabilities and thermally simulated in WebTHERM to make sure critical temperatures are not exceeded.

Soldering Component to Board

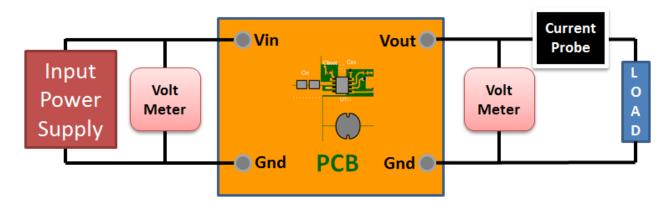
If board assembly is done in house it is best to tack down one terminal of a component on the board then solder the other terminal. For surface mount parts with large tabs, such as the DPAK, the tab on the back of the package should be pre-tinned with solder, then tacked into place by one of the pins. To solder the tab town to the board place the iron down on the board while resting against the tab, heating both surfaces simultaneously. Apply light pressure to the top of the plastic case until the solder flows around the part and the part is flush with the PCB. If the solder is not flowing around the board you may need a higher wattage iron (generally 25W to 30W is enough).

Initial Startup of Circuit

It is best to initially power up the board by setting the input supply voltage to the lowest operating input voltage 48.0V and set the input supply's current limit to zero. With the input supply off connect up the input supply to Vin and GND. Connect a digital volt meter and a load if needed to set the minimum lout of the design from Vout and GND. Turn on the input supply and slowly turn up the current limit on the input supply. If the voltage starts to rise on the input supply continue increasing the input supply current limit while watching the output voltage. If the current increases on the input supply, but the voltage remains near zero, then there may be a short or a component misplaced on the board. Power down the board and visually inspect for solder bridges and recheck the diode and capacitor polarities. Once the power supply circuit is operational then more extensive testing may include full load testing, transient load and line tests to compare with simulation results.

Load Testing

The setup is the same as the initial startup, except that an additional digital voltmeter is connected between Vin and GND, a load is connected between Vout and GND and a current meter is connected in series between Vout and the load. The load must be able to handle at least rated output power + 50% (7.5 watts for this design). Ideally the load is supplied in the form of a variable load test unit. It can also be done in the form of suitably large power resistors. When using an oscilloscope to measure waveforms on the prototype board, the ground leads of the oscilloscope probes should be as short as possible and the area of the loop formed by the ground lead should be kept to a minimum. This will help reduce ground lead inductance and eliminate EMI noise that is not actually present in the circuit.



Design Assistance

- 1. Please note that since parallel FETs have been chosen in this design, schematic and PCB export features will not work
- 2. Master key: E8972043B38D6425[v1]
- 3. LM5146 Product Folder: http://www.ti.com/product/lm5146: contains the data sheet and other resources.

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