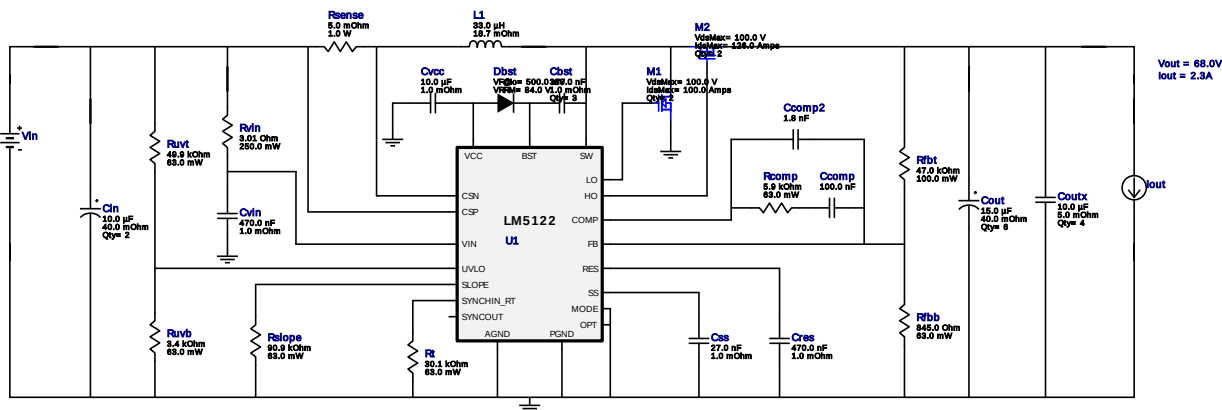


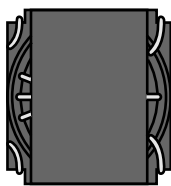
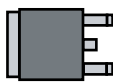
WEBENCH® Design Report

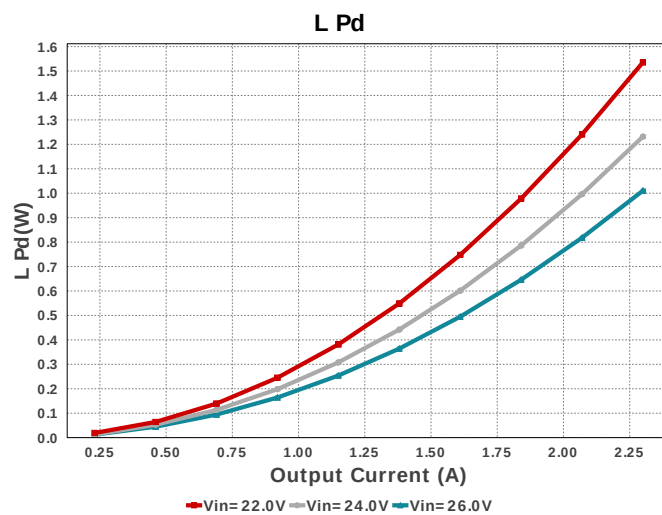
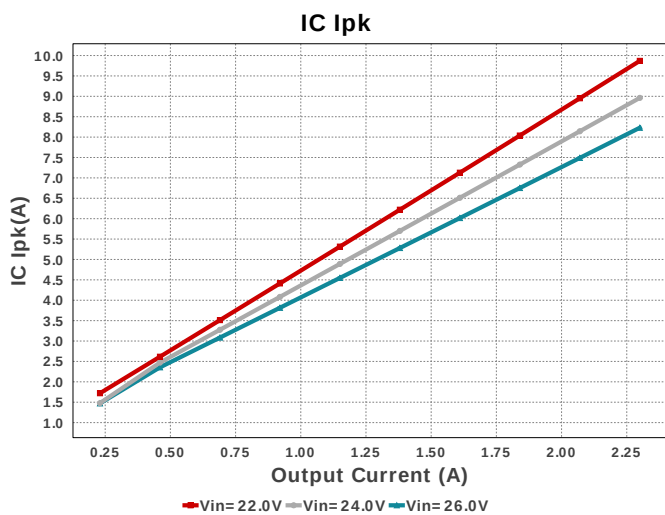
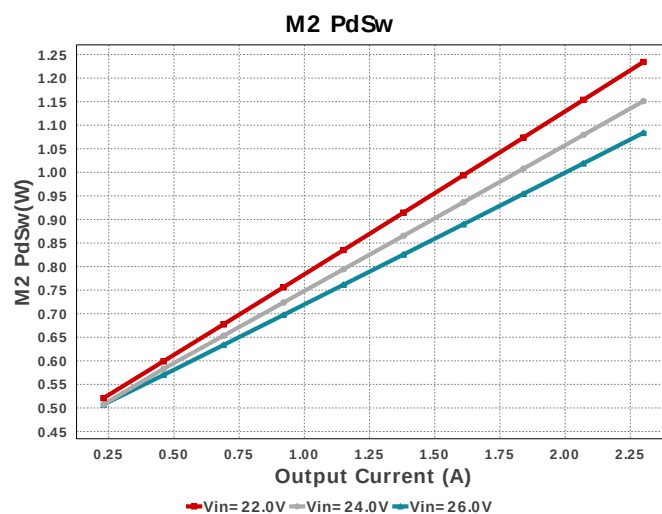
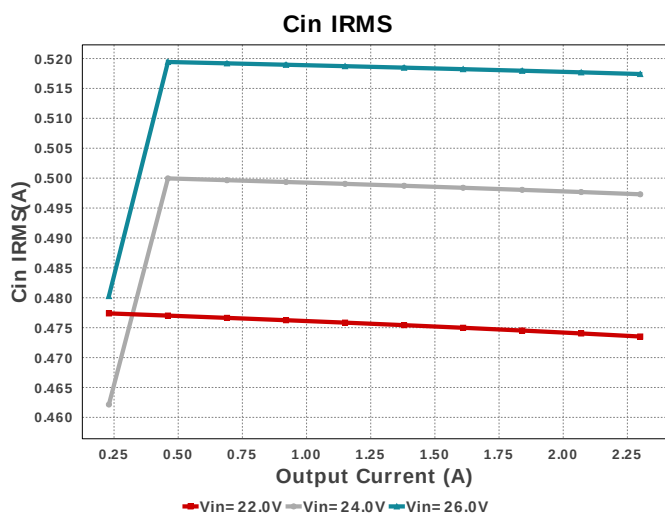
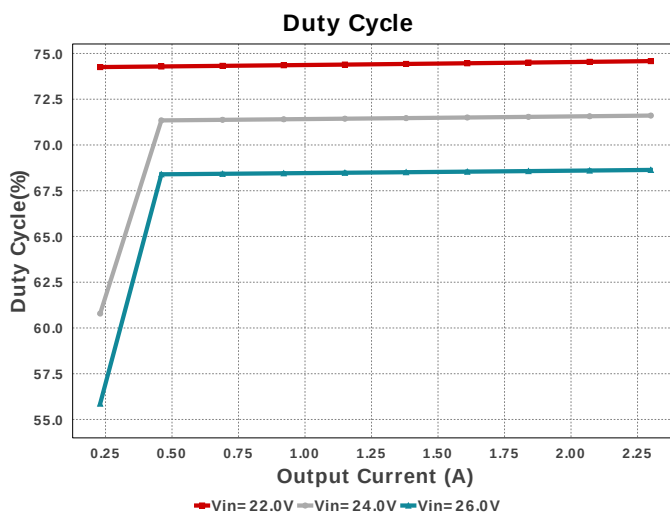
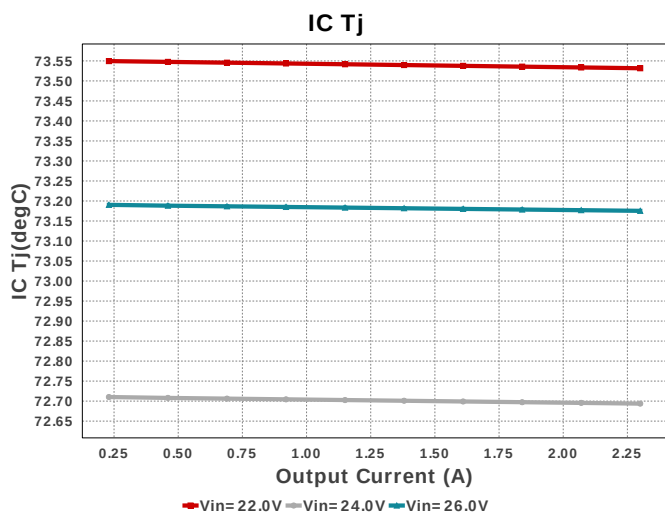
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LM5122MH/NOPB 22V-26V to 68.00V @ 2,3A

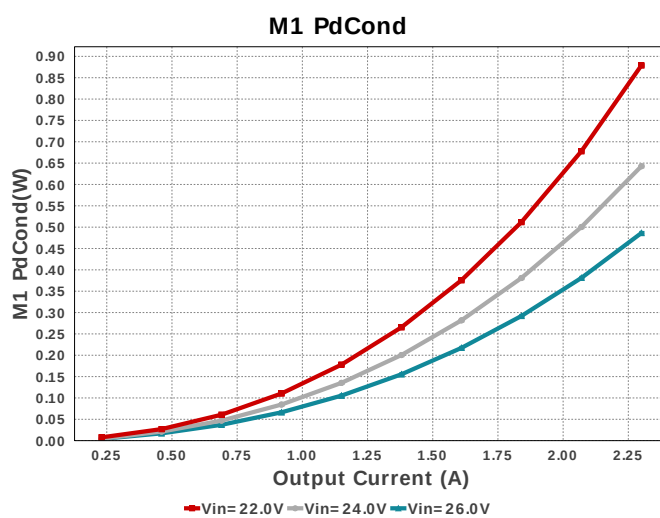
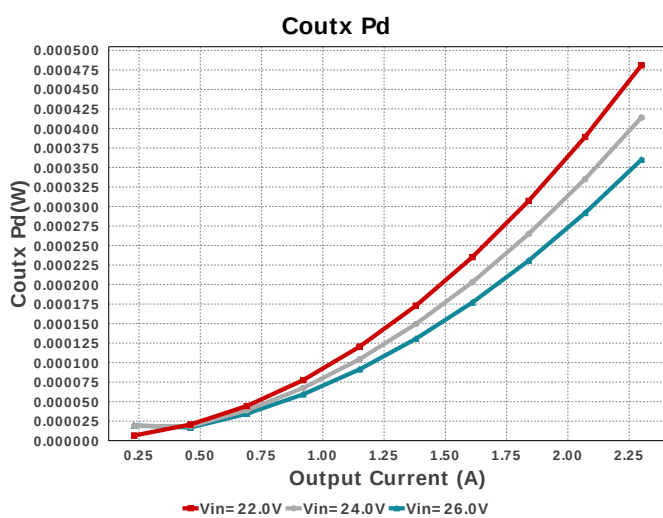
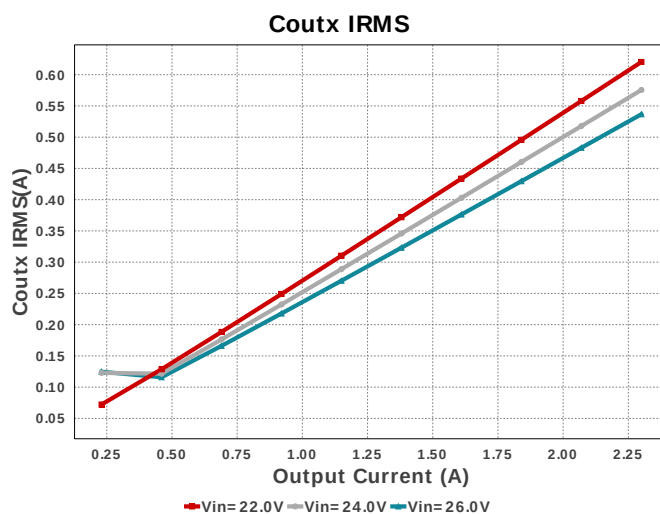
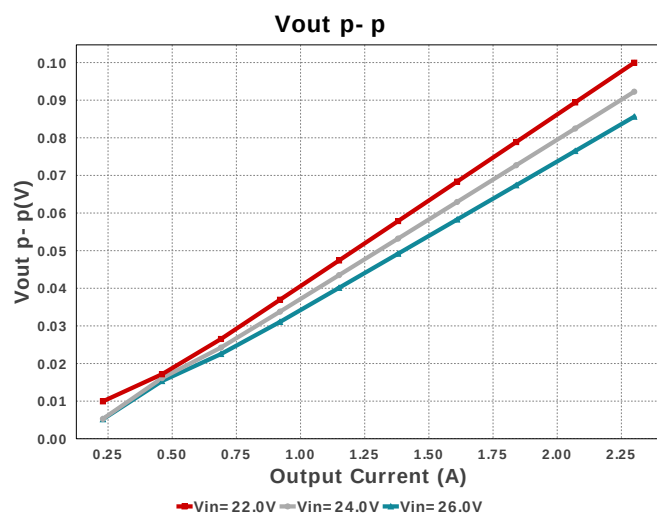
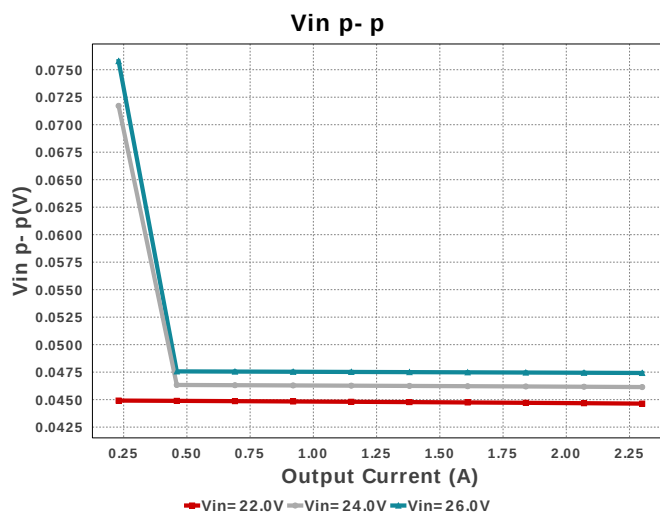
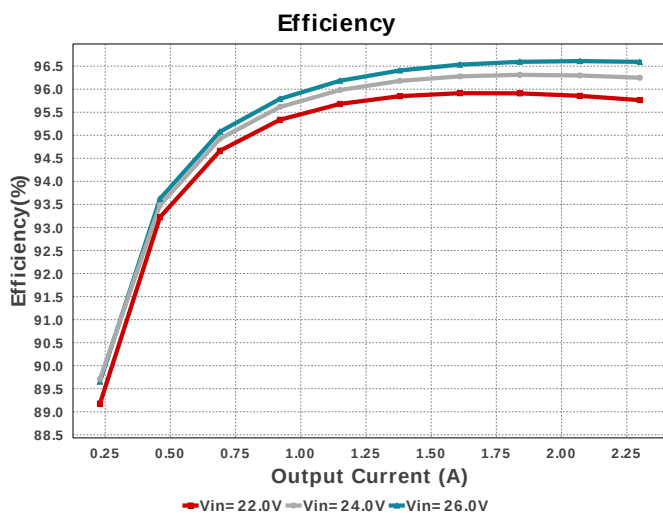


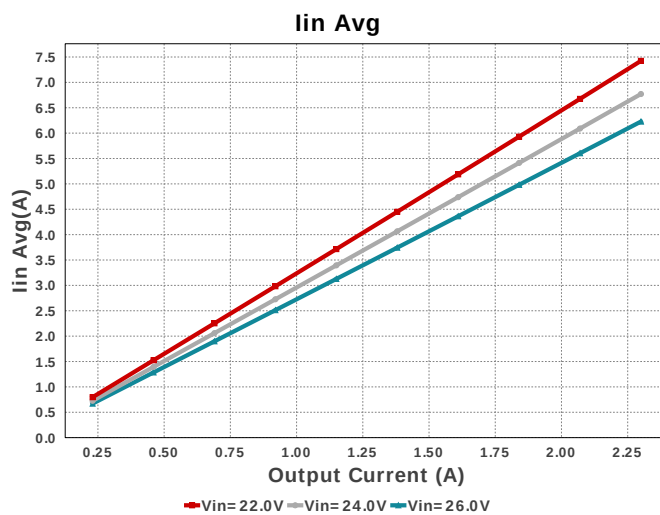
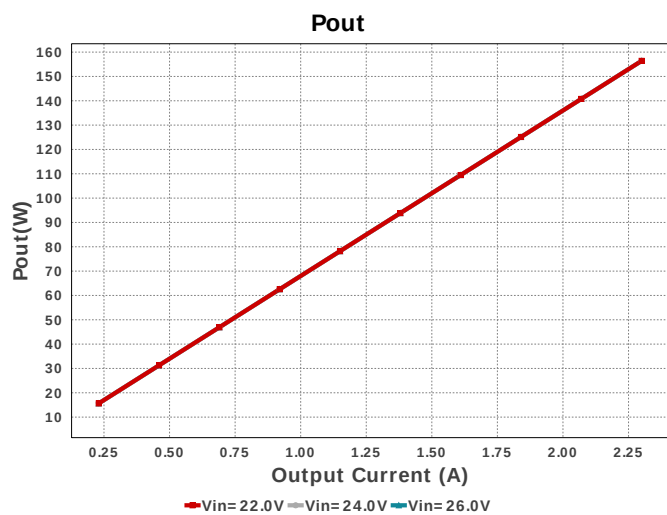
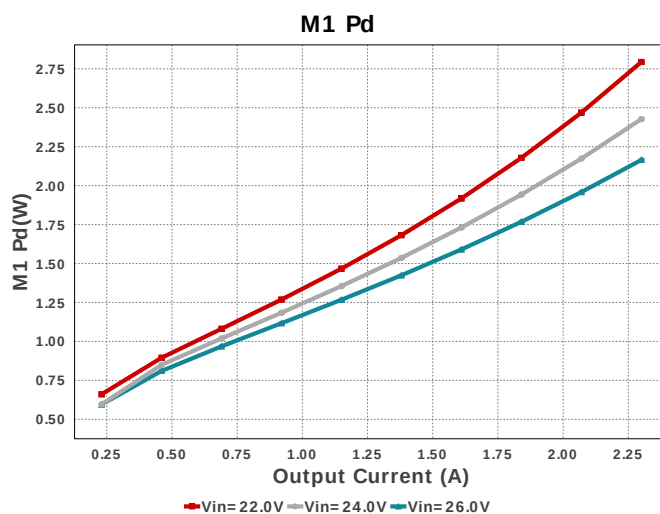
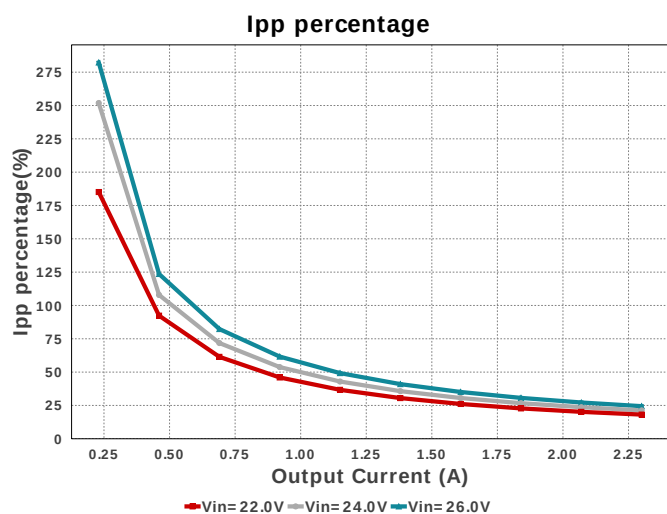
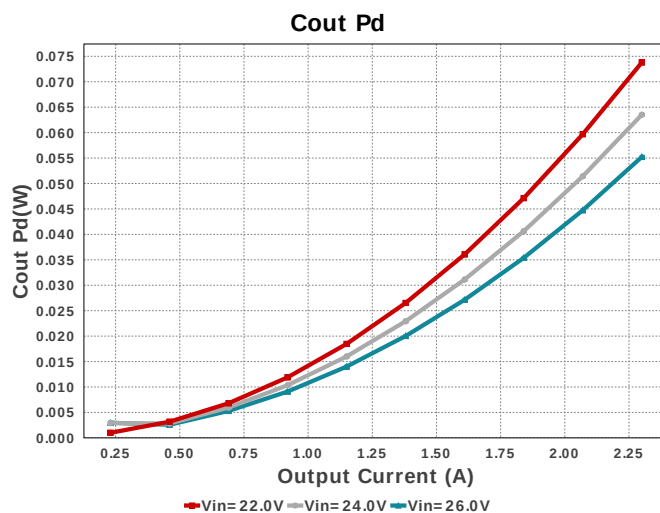
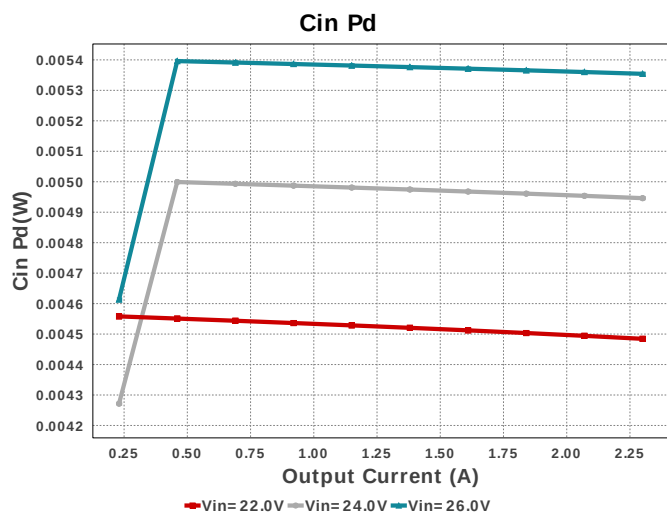
Electrical BOM

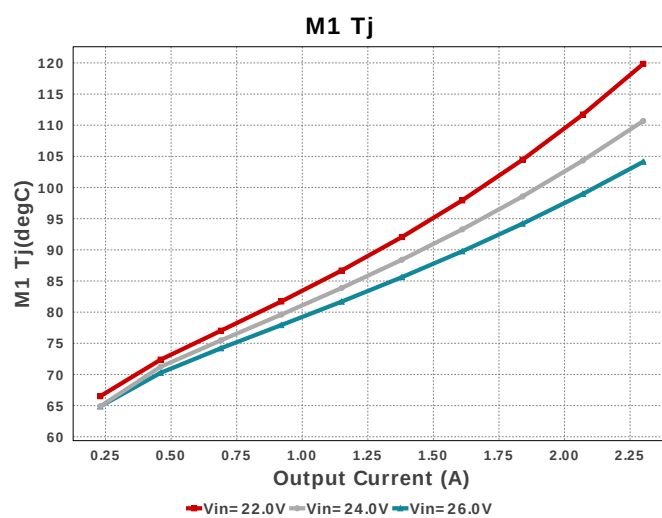
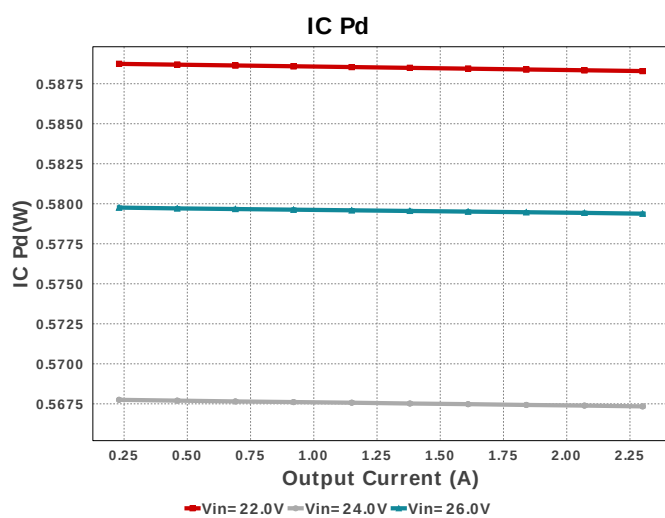
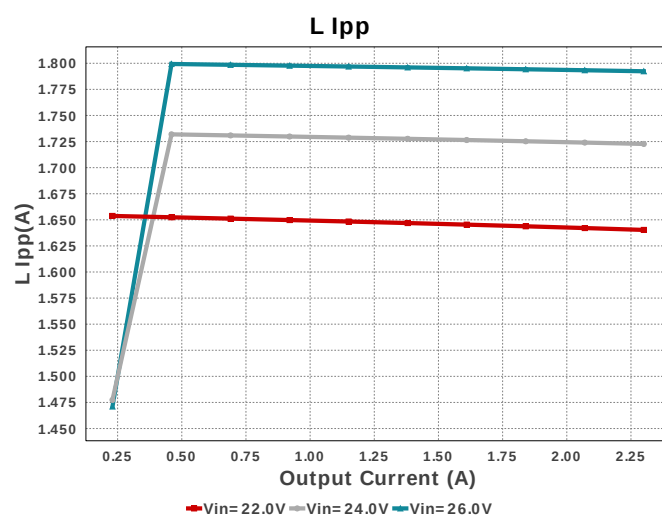
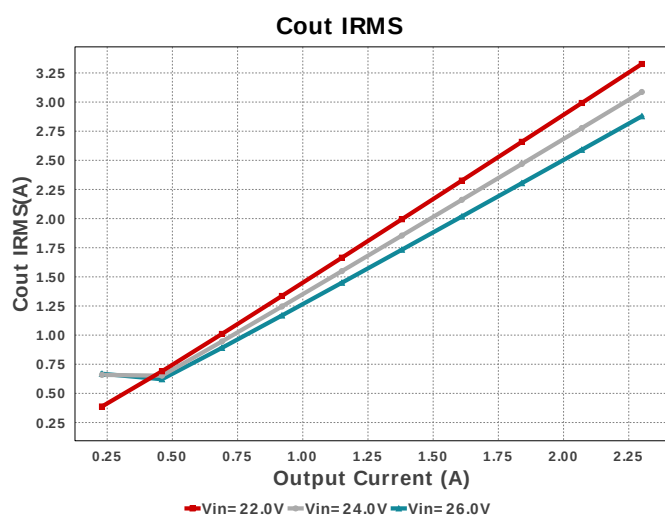
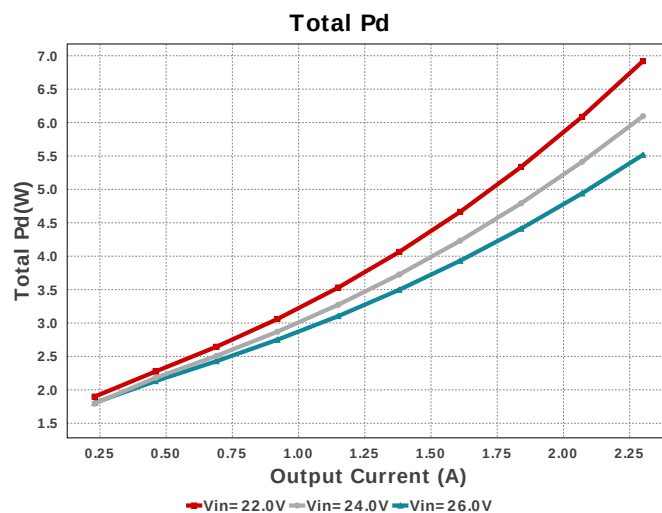
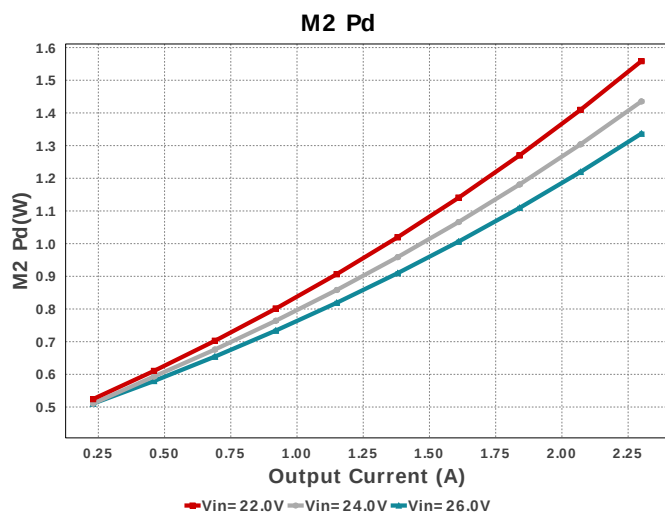
Name	Manufacturer	Part Number	Properties	Qty	Price	Footprint
Cbst	MuRata	GRM21AR72A334KAC5L Series= X7R	Cap= 330.0 nF ESR= 1.0 mOhm VDC= 100.0 V IRMS= 0.0 A	3	\$0.11	 0805 7 mm ²
Ccomp	AVX	08053C104JAZ2A Series= X7R	Cap= 100.0 nF VDC= 25.0 V IRMS= 0.0 A	1	\$0.06	 0805 7 mm ²
Ccomp2	TDK	C2012C0G1H182K060AA Series= C0G/NP0	Cap= 1.8 nF VDC= 50.0 V IRMS= 0.0 A	1	\$0.04	 0805 7 mm ²
Cin	Panasonic	50SVPF10M Series= SVPF	Cap= 10.0 uF ESR= 40.0 mOhm VDC= 50.0 V IRMS= 2.5 A	2	\$0.41	 CAPSMT_62_F61 74 mm ²
Cout	Panasonic	100SXV15M Series= SXV	Cap= 15.0 uF ESR= 40.0 mOhm VDC= 100.0 V IRMS= 2.35 A	6	\$1.18	 CAPSMT_62_E12 106 mm ²
Coutx	TDK	C5750X7S2A106M230KB Series= X7S	Cap= 10.0 uF ESR= 5.0 mOhm VDC= 100.0 V IRMS= 6.45 A	4	\$0.86	 2220 54 mm ²
Cres	Taiyo Yuden	TMK212BJ474KD-T Series= X5R	Cap= 470.0 nF ESR= 1.0 mOhm VDC= 20.0 V IRMS= 0.0 A	1	\$0.02	 0805 7 mm ²
Css	MuRata	GRM155R71A273KA01D Series= X7R	Cap= 27.0 nF ESR= 1.0 mOhm VDC= 10.0 V IRMS= 0.0 A	1	\$0.01	 0402 3 mm ²
Cvcc	Taiyo Yuden	EMK212BJ106KG-T Series= X5R	Cap= 10.0 uF ESR= 1.0 mOhm VDC= 16.0 V IRMS= 0.0 A	1	\$0.03	 0805 7 mm ²

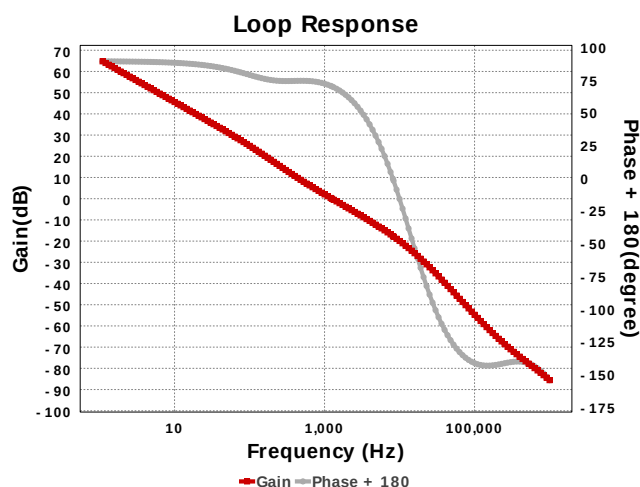
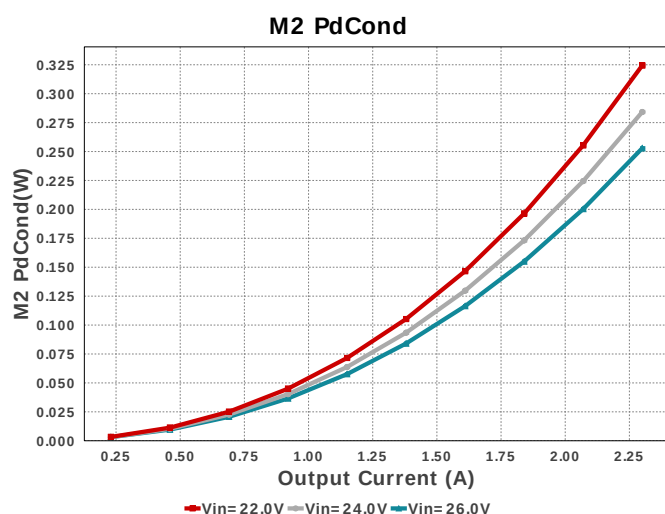
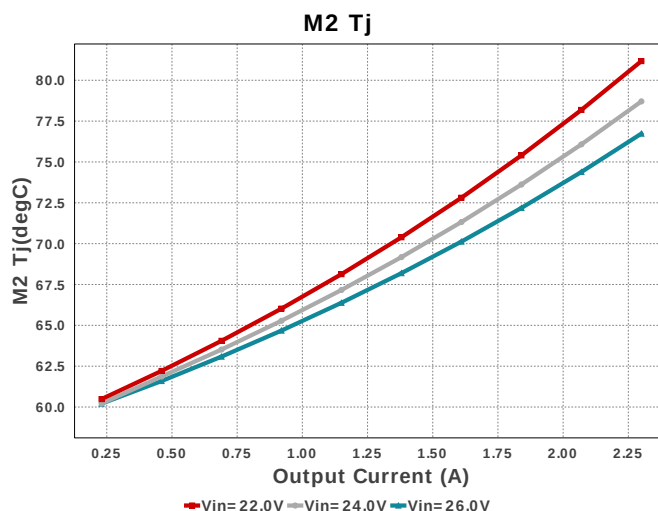
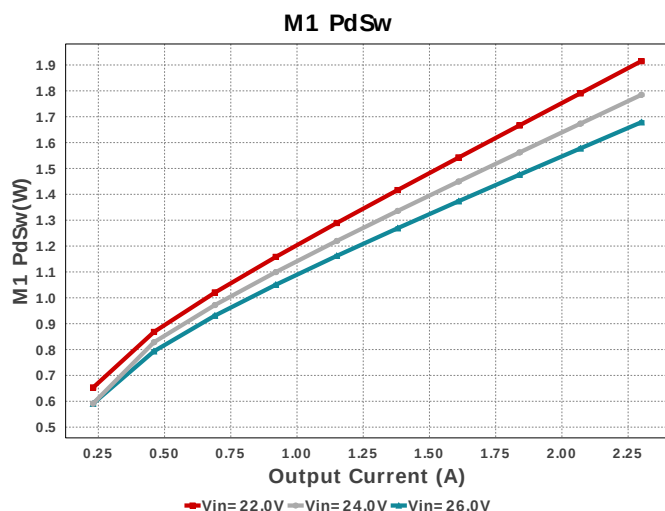
Name	Manufacturer	Part Number	Properties	Qty	Price	Footprint
Cvin	MuRata	GRM21BR71H474KA88L Series= X7R	Cap= 470.0 nF ESR= 1.0 mOhm VDC= 50.0 V IRMS= 0.0 A	1	\$0.08	 0805 7 mm ²
Dbst	CUSTOM	CUSTOM	VF@Io= 500.0 mV VRRM= 84.0 V	1	NA	CUSTOM 0 mm ²
L1	Coilcraft	XAL1510-333MEB	L= 33.0 µH 18.7 mOhm	1	\$2.27	 XAL1510 320 mm ²
M1	Texas Instruments	CSD19534Q5A	VdsMax= 100.0 V IdsMax= 100.0 Amps	2	\$0.34	 TRANS_NexFET_Q5A 55 mm ²
M2	International Rectifier	IRLR3110ZPBF	VdsMax= 100.0 V IdsMax= 126.0 Amps	2	\$0.94	 DPAK 102 mm ²
Rcomp	Vishay-Dale	CRCW04025K90FKED Series= CRCW..e3	Res= 5.9 kOhm Power= 63.0 mW Tolerance= 1.0%	1	\$0.01	 0402 3 mm ²
Rfbb	Vishay-Dale	CRCW0402845RFKED Series= CRCW..e3	Res= 845.0 Ohm Power= 63.0 mW Tolerance= 1.0%	1	\$0.01	 0402 3 mm ²
Rfbt	Susumu Co Ltd	RR1220P-473-D Series= RR12	Res= 47.0 kOhm Power= 100.0 mW Tolerance= 0.5%	1	\$0.01	 0805 7 mm ²
Rsense	Susumu Co Ltd	PRL1632-R005-F-T1 Series= PRL1632	Res= 5.0 mOhm Power= 1.0 W Tolerance= 1.0%	1	\$0.20	 0612 11 mm ²
Rslope	Vishay-Dale	CRCW040290K9FKED Series= CRCW..e3	Res= 90.9 kOhm Power= 63.0 mW Tolerance= 1.0%	1	\$0.01	 0402 3 mm ²
Rt	Vishay-Dale	CRCW040230K1FKED Series= CRCW..e3	Res= 30.1 kOhm Power= 63.0 mW Tolerance= 1.0%	1	\$0.01	 0402 3 mm ²
Ruvb	Vishay-Dale	CRCW04023K40FKED Series= CRCW..e3	Res= 3.4 kOhm Power= 63.0 mW Tolerance= 1.0%	1	\$0.01	 0402 3 mm ²
Rvvt	Vishay-Dale	CRCW040249K9FKED Series= CRCW..e3	Res= 49.9 kOhm Power= 63.0 mW Tolerance= 1.0%	1	\$0.01	 0402 3 mm ²
Rvin	Vishay-Dale	CRCW12063R01FKEA Series= CRCW..e3	Res= 3.01 Ohm Power= 250.0 mW Tolerance= 1.0%	1	\$0.01	 1206 11 mm ²
U1	Texas Instruments	LM5122MH/NOPB	Switcher	1	\$2.09	 MXA20A 71 mm ²











Operating Values

#	Name	Value	Category	Description
1.	BOM Count	37		Total Design BOM count
2.	Total BOM	NA		Total BOM Cost
3.	Cin IRMS	473.52 mA	Capacitor	Input capacitor RMS ripple current
4.	Cin Pd	4.484 mW	Capacitor	Input capacitor power dissipation
5.	Cout IRMS	3.327 A	Capacitor	Output capacitor RMS ripple current
6.	Cout Pd	73.785 mW	Capacitor	Output capacitor power dissipation
7.	Coutx IRMS	620.314 mA	Capacitor	Output capacitor_x RMS ripple current
8.	Coutx Pd	480.99 μ W	Capacitor	Output capacitor_x power loss
9.	IC Ipk	9.869 A	IC	Peak switch current in IC
10.	IC Pd	588.29 mW	IC	IC power dissipation
11.	IC Tj	73.532 degC	IC	IC junction temperature
12.	IC Tolerance	18.0 mV	IC	IC Feedback Tolerance
13.	ICThetaJA	40.0 degC/W	IC	IC junction-to-ambient thermal resistance
14.	Iin Avg	7.424 A	IC	Average input current
15.	Ipp percentage	18.127 %	Inductor	Inductor ripple current percentage (with respect to average inductor current)
16.	L Ipp	1.64 A	Inductor	Peak-to-peak inductor ripple current
17.	L Pd	1.536 W	Inductor	Inductor power dissipation
18.	M1 Pd	2.794 W	Mosfet	M1 MOSFET total power dissipation
19.	M1 PdCond	878.81 mW	Mosfet	M1 MOSFET conduction losses
20.	M1 PdSw	1.915 W	Mosfet	M1 MOSFET switching losses
21.	M1 Tj	119.845 degC	Mosfet	M1 MOSFET junction temperature
22.	M2 Pd	1.559 W	Mosfet	M2 MOSFET total power dissipation
23.	M2 PdCond	324.41 mW	Mosfet	M2 MOSFET conduction losses
24.	M2 PdSw	1.234 W	Mosfet	M2 MOSFET switching losses
25.	M2 Tj	81.173 degC	Mosfet	M2 MOSFET junction temperature
26.	Cin Pd	4.484 mW	Power	Input capacitor power dissipation
27.	Cout Pd	73.785 mW	Power	Output capacitor power dissipation
28.	Coutx Pd	480.99 μ W	Power	Output capacitor_x power loss
29.	IC Pd	588.29 mW	Power	IC power dissipation
30.	L Pd	1.536 W	Power	Inductor power dissipation
31.	M1 Pd	2.794 W	Power	M1 MOSFET total power dissipation

#	Name	Value	Category	Description
32.	M1 PdCond	878.81 mW	Power	M1 MOSFET conduction losses
33.	M1 PdSw	1.915 W	Power	M1 MOSFET switching losses
34.	M2 Pd	1.559 W	Power	M2 MOSFET total power dissipation
35.	M2 PdCond	324.41 mW	Power	M2 MOSFET conduction losses
36.	M2 PdSw	1.234 W	Power	M2 MOSFET switching losses
37.	Total Pd	6.92 W	Power	Total Power Dissipation
38.	Cross Freq	1.028 kHz	System Information	Bode plot crossover frequency
39.	Duty Cycle	74.583 %	System Information	Duty cycle
40.	Efficiency	95.763 %	System Information	Steady state efficiency
41.	FootPrint	1.814 k mm ²	System Information	Total Foot Print Area of BOM components
42.	Frequency	299.003 kHz	System Information	Switching frequency
43.	Gain Marg	-17.031 dB	System Information	Bode Plot Gain Margin
44.	Iout	2.3 A	System Information	Iout operating point
45.	Low Freq Gain	64.838 dB	System Information	Gain at 1Hz
46.	Mode	CCM	System Information	Conduction Mode
47.	Phase Marg	69.305 deg	System Information	Bode Plot Phase Margin
48.	Pout	156.4 W	System Information	Total output power
49.	Vin	22.0 V	System Information	Vin operating point
50.	Vin p-p	44.636 mV	System Information	Peak-to-peak input voltage
51.	Vout	68.0 V	System Information	Operational Output Voltage
52.	Vout Actual	67.946 V	System Information	Vout Actual calculated based on selected voltage divider resistors
53.	Vout Tolerance	3.011 %	System Information	Vout Tolerance based on IC Tolerance (no load) and voltage divider resistors if applicable
54.	Vout p-p	99.966 mV	System Information	Peak-to-peak output ripple voltage

Design Inputs

Name	Value	Description
Iout	2.3	Maximum Output Current
SoftStart	1.0 ms	Soft Start Time (ms)
VinMax	26.0	Maximum input voltage
VinMin	22.0	Minimum input voltage
Vout	68.0	Output Voltage
base_pn	LM5122	Base Product Number
source	DC	Input Source Type
Ta	50.0	Ambient temperature
UserFsw	600.0 k	Customer Selected Frequency

WEBENCH® Assembly

Component Testing

Some published data on components in datasheets such as Capacitor ESR and Inductor DC resistance is based on conservative values that will guarantee that the components always exceed the specification. For design purposes it is usually better to work with typical values. Since this data is not always available it is a good practice to measure the Capacitance and ESR values of C_{in} and C_{out} , and the inductance and DC resistance of $L1$ before assembly of the board. Any large discrepancies in values should be electrically simulated in WEBENCH to check for instabilities and thermally simulated in WebTHERM to make sure critical temperatures are not exceeded.

Soldering Component to Board

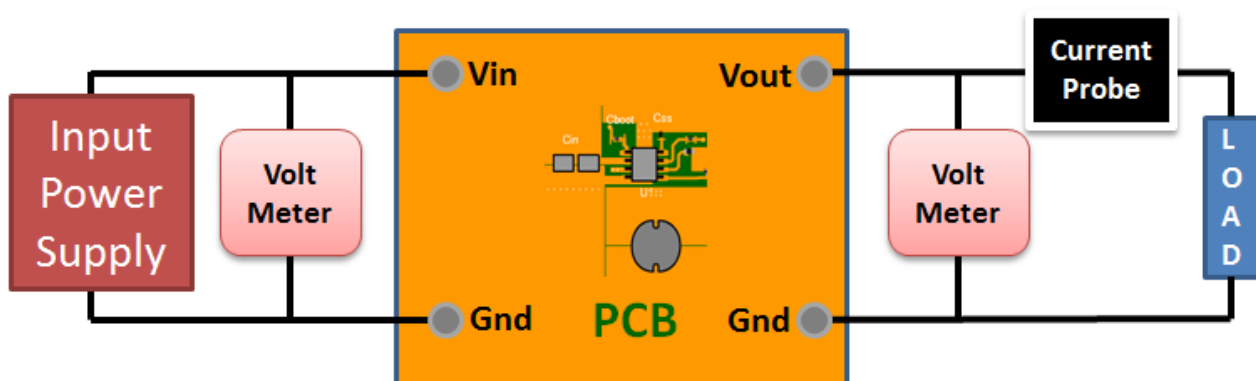
If board assembly is done in house it is best to tack down one terminal of a component on the board then solder the other terminal. For surface mount parts with large tabs, such as the DPAK, the tab on the back of the package should be pre-tinned with solder, then tacked into place by one of the pins. To solder the tab down to the board place the iron down on the board while resting against the tab, heating both surfaces simultaneously. Apply light pressure to the top of the plastic case until the solder flows around the part and the part is flush with the PCB. If the solder is not flowing around the board you may need a higher wattage iron (generally 25W to 30W is enough).

Initial Startup of Circuit

It is best to initially power up the board by setting the input supply voltage to the lowest operating input voltage 22.0V and set the input supply's current limit to zero. With the input supply off connect up the input supply to V_{in} and GND. Connect a digital volt meter and a load if needed to set the minimum load of the design from V_{out} and GND. Turn on the input supply and slowly turn up the current limit on the input supply. If the voltage starts to rise on the input supply continue increasing the input supply current limit while watching the output voltage. If the current increases on the input supply, but the voltage remains near zero, then there may be a short or a component misplaced on the board. Power down the board and visually inspect for solder bridges and recheck the diode and capacitor polarities. Once the power supply circuit is operational then more extensive testing may include full load testing, transient load and line tests to compare with simulation results.

Load Testing

The setup is the same as the initial startup, except that an additional digital voltmeter is connected between V_{in} and GND, a load is connected between V_{out} and GND and a current meter is connected in series between V_{out} and the load. The load must be able to handle at least rated output power + 50% (7.5 watts for this design). Ideally the load is supplied in the form of a variable load test unit. It can also be done in the form of suitably large power resistors. When using an oscilloscope to measure waveforms on the prototype board, the ground leads of the oscilloscope probes should be as short as possible and the area of the loop formed by the ground lead should be kept to a minimum. This will help reduce ground lead inductance and eliminate EMI noise that is not actually present in the circuit.



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