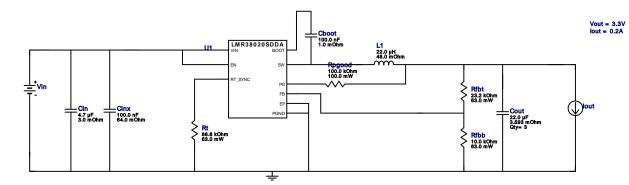
VinMin = 9.0V VinMax = 36.0V Vout = 3.3V Iout = 0.2A Device = LMR38020SDDAR Topology = Buck Created = 2023-11-28 10:35:36.151 BOM Cost = \$2.18 BOM Count = 12 Total Pd = 0.1W

# WEBENCH<sup>®</sup> Design Report

Design : 72 LMR38020SDDAR LMR38020SDDAR 9V-75V to 3.30V @ 0.3A



#### **Design Alerts**

#### **Component Selection Information**

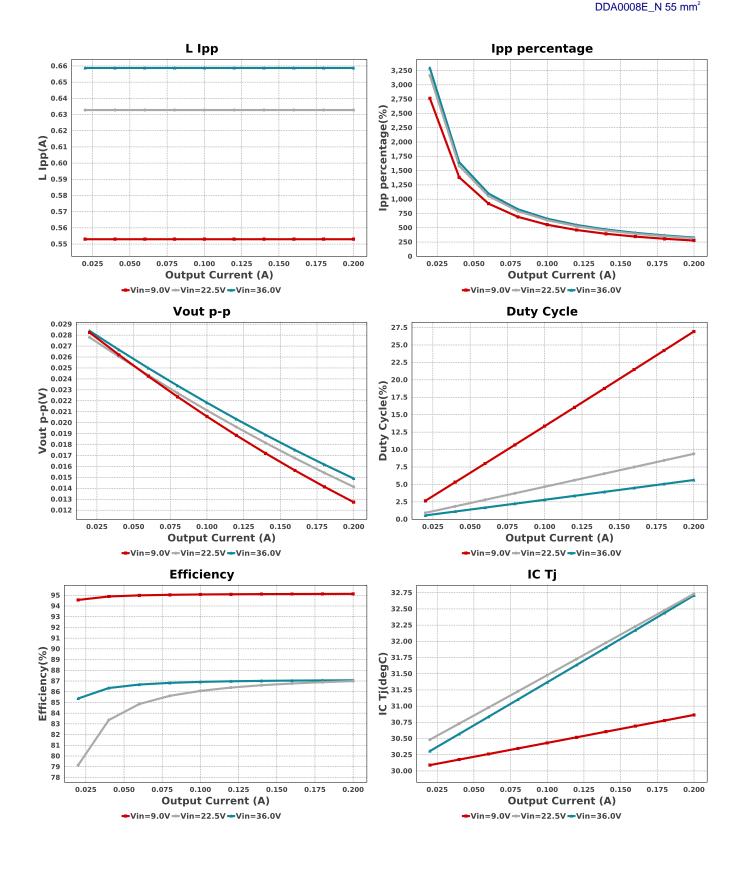
This device support spread spectrum feature which is not modeled on WEBENCH. This device can work in steady state at Vin = 4.2V. However, needs a minimum of 4.5V during start up. See datasheet for details.

#### **Electrical BOM**

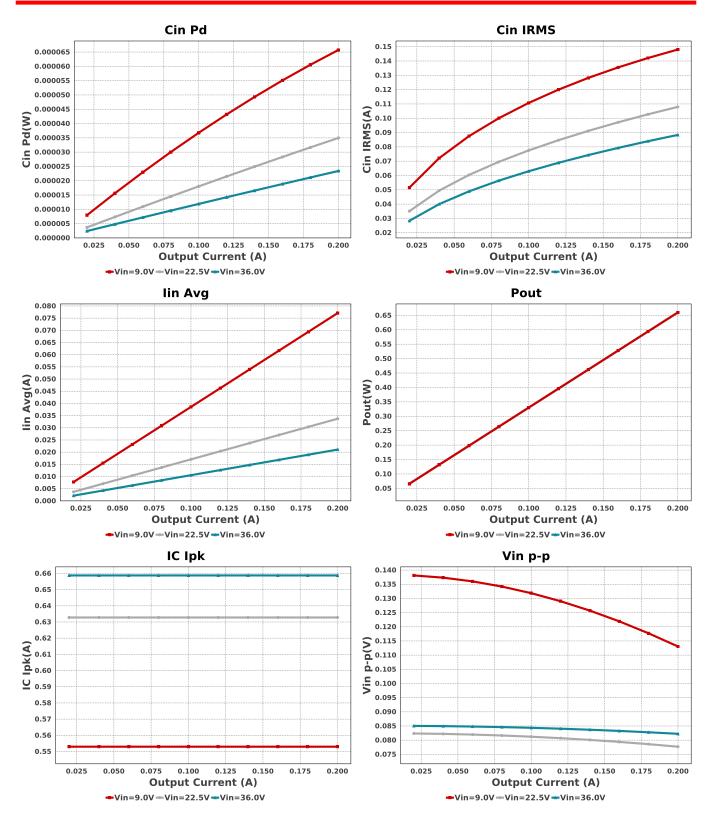
Name	Manufacturer	Part Number	Properties	Qty	Price	Footprint
Cboot	MuRata	GRM155R71C104KA88D Series= X7R	Cap= 100.0 nF ESR= 1.0 mOhm VDC= 16.0 V IRMS= 0.0 A	1	\$0.01	■ 0402 3 mm <sup>2</sup>
Cin	MuRata	GRM31CR71H475KA12L Series= X7R	Cap= 4.7 uF ESR= 3.0 mOhm VDC= 50.0 V IRMS= 4.98 A	1	\$0.10	1206 11 mm <sup>2</sup>
Cinx	Kemet	C0805C104M5RACTU Series= X7R	Cap= 100.0 nF ESR= 64.0 mOhm VDC= 50.0 V IRMS= 1.64 A	1	\$0.01	■ 0805 7 mm <sup>2</sup>
Cout	MuRata	GRM31CR71A226KE15L Series= X7R	Cap= 22.0 uF ESR= 3.593 mOhm VDC= 10.0 V IRMS= 3.5332 A	3	\$0.12	1206_190 11 mm <sup>2</sup>
L1	Bourns	SRR1208-220ML	L= 22.0 µH 48.0 mOhm	1	\$0.56	SRR1208 216 mm <sup>2</sup>
Rfbb	Vishay-Dale	CRCW040210K0FKED Series= CRCWe3	Res= 10.0 kOhm Power= 63.0 mW Tolerance= 1.0%	1	\$0.01	■ 0402 3 mm <sup>2</sup>
Rfbt	Vishay-Dale	CRCW040223K2FKED Series= CRCWe3	Res= 23.2 kOhm Power= 63.0 mW Tolerance= 1.0%	1	\$0.01	■ 0402 3 mm <sup>2</sup>
Rpgood	Vishay-Dale	CRCW0603100KFKEA Series= CRCWe3	Res= 100.0 kOhm Power= 100.0 mW Tolerance= 1.0%	1	\$0.01	■ 0603 5 mm <sup>2</sup>

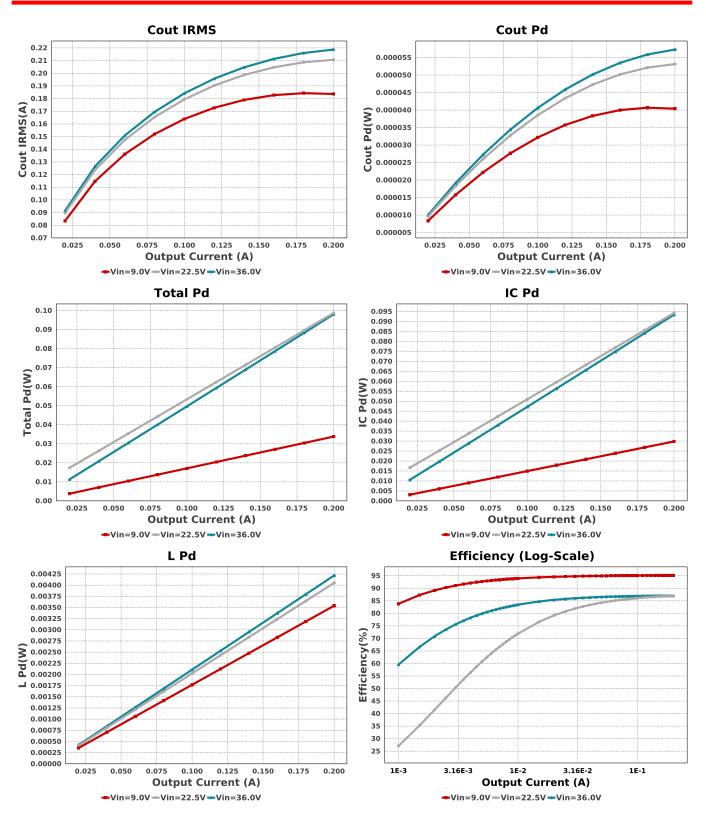
### WEBENCH<sup>®</sup> Design

Name	Manufacturer	Part Number	Properties	Qty	Price	Footprint
Rt	Yageo	AC0402FR-0786K6L Series= ?	Res= 86.6 kOhm Power= 63.0 mW Tolerance= 1.0%	1	\$0.01	■ 0402 3 mm <sup>2</sup>
U1	Texas Instruments	LMR38020SDDAR	Switcher	1	\$1.10	



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### **Operating Values**

#	Name	Value	Category	Description
1.	BOM Count	12		Total Design BOM count
2.	Total BOM	\$2.182		Total BOM Cost
3.	Cin IRMS	88.349 mA	Capacitor	Input capacitor RMS ripple current
4.	Cin Pd	23.417 µW	Capacitor	Input capacitor power dissipation
5.	Cout IRMS	218.709 mA	Capacitor	Output capacitor RMS ripple current
6.	Cout Pd	57.289 µW	Capacitor	Output capacitor power dissipation
7.	IC lpk	658.752 mA	IC	Peak switch current in IC
8.	IC Pd	93.411 mW	IC	IC power dissipation
9.	IC Tj	32.709 degC	IC	IC junction temperature
10.	IC Tolerance	5.0 mV	IC	IC Feedback Tolerance
11.	ICThetaJA Effective	29.0 degC/W	IC	Effective IC Junction-to-Ambient Thermal Resistance

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## WEBENCH<sup>®</sup> Design

#	Name	Value	Category	Description
12.	lin Avg	21.057 mA	IC	Average input current
13.	Ipp percentage	329.376 %	Inductor	Inductor ripple current percentage (with respect to average inductor current)
14	L Ipp	658.752 mA	Inductor	Peak-to-peak inductor ripple current
	L Pd	4.216 mW	Inductor	Inductor power dissipation
	Cin Pd	23.417 µW	Power	Input capacitor power dissipation
17.		57.289 μW	Power	Output capacitor power dissipation
18.	IC Pd	93.411 mW	Power	IC power dissipation
-	L Pd	4.216 mW	Power	Inductor power dissipation
20.	Total Pd	98.039 mW	Power	Total Power Dissipation
21.	Duty Cycle	5.634 %	System	Duty cycle
	- · <b>j</b> - <b>j</b>		Information	
22.	Efficiency	87.067 %	System	Steady state efficiency
	,		Information	
23.	FootPrint	338.0 mm <sup>2</sup>	System	Total Foot Print Area of BOM components
			Information	
24.	Frequency	126.843 kHz	System Information	Switching frequency
25.	Inductor ripple current	40.0 %	System	Custom Inductor ripple current (% of average inductor current)
	requirement used for		Information	requirement used for Inductor selection
	Inductor selection			
26.	lout	200.0 mA	System	lout operating point
			Information	
27.	lout transient step used	100.0 mA	System	Custom Transient current step requirement that was used for Cout
	for Cout calculations		Information	selection (A).
28.	Mode	PFM	System	Conduction Mode
			Information	
29.	Overshoot Value	614.98 µV	System Information	Theoretical Vout Overshoot Value
30.	Pout	660.0 mW	System	Total output power
30.	FUUL	000.0 1110	Information	
31.	Undershoot Value	13.274 mV	System	Theoretical Vout Undershoot Value
01.		10.27 4 111	Information	
32.	Vin	36.0 V	System	Vin operating point
02.	•	00.0 1	Information	
33.	Vin p-p	82.243 mV	System	Peak-to-peak input voltage
	· · · F F		Information	
34.	Vout	3.3 V	System	Operational Output Voltage
-			Information	
35.	Vout Actual	3.32 V	System	Vout Actual calculated based on selected voltage divider resistors
			Information	
36.	Vout Ripple	1.0 %	System	Custom maximum output ripple requirement that was used for Cout
	requirement used for		Information	selection(% of Vout).
	Cout calculations			
37.	Vout Tolerance	1.919 %	System	Vout Tolerance based on IC Tolerance (no load) and voltage divider
			Information	resistors if applicable
38.	Vout p-p	14.897 mV	System	Peak-to-peak output ripple voltage
			Information	
39.	Vout transient	3.0 %	System	Custom Transient voltage change requirement that was used for Cout
	requirement used for		Information	selection (% of Vout).
	Cout calculations			

### **Design Inputs**

Name	Value	Description	
lout	200.0 m	Maximum Output Current	
VinMax	36.0	Maximum input voltage	
VinMin	9.0	Minimum input voltage	
Vout	3.3	Output Voltage	
base_pn	LMR38020S	Base Product Number	
source	DC	Input Source Type	
Та	30.0	Ambient temperature	
UserFsw	300.0 k	Customer Selected Frequency	

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### WEBENCH<sup>®</sup> Assembly

### **Component Testing**

Some published data on components in datasheets such as Capacitor ESR and Inductor DC resistance is based on conservative values that will guarantee that the components always exceed the specification. For design purposes it is usually better to work with typical values. Since this data is not always available it is a good practice to measure the Capacitance and ESR values of Cin and Cout, and the inductance and DC resistance of L1 before assembly of the board. Any large discrepancies in values should be electrically simulated in WEBENCH to check for instabilities and thermally simulated in WebTHERM to make sure critical temperatures are not exceeded.

### Soldering Component to Board

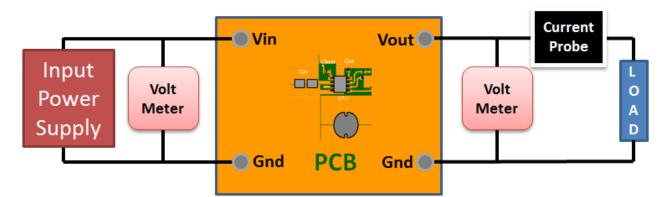
If board assembly is done in house it is best to tack down one terminal of a component on the board then solder the other terminal. For surface mount parts with large tabs, such as the DPAK, the tab on the back of the package should be pre-tinned with solder, then tacked into place by one of the pins. To solder the tab town to the board place the iron down on the board while resting against the tab, heating both surfaces simultaneously. Apply light pressure to the top of the plastic case until the solder flows around the part and the part is flush with the PCB. If the solder is not flowing around the board you may need a higher wattage iron (generally 25W to 30W is enough).

### Initial Startup of Circuit

It is best to initially power up the board by setting the input supply voltage to the lowest operating input voltage 9.0V and set the input supply's current limit to zero. With the input supply off connect up the input supply to Vin and GND. Connect a digital volt meter and a load if needed to set the minimum lout of the design from Vout and GND. Turn on the input supply and slowly turn up the current limit on the input supply. If the voltage starts to rise on the input supply continue increasing the input supply current limit while watching the output voltage. If the current increases on the input supply, but the voltage remains near zero, then there may be a short or a component misplaced on the board. Power down the board and visually inspect for solder bridges and recheck the diode and capacitor polarities. Once the power supply circuit is operational then more extensive testing may include full load testing, transient load and line tests to compare with simulation results.

### Load Testing

The setup is the same as the initial startup, except that an additional digital voltmeter is connected between Vin and GND, a load is connected between Vout and GND and a current meter is connected in series between Vout and the load. The load must be able to handle at least rated output power + 50% (7.5 watts for this design). Ideally the load is supplied in the form of a variable load test unit. It can also be done in the form of suitably large power resistors. When using an oscilloscope to measure waveforms on the prototype board, the ground leads of the oscilloscope probes should be as short as possible and the area of the loop formed by the ground lead should be kept to a minimum. This will help reduce ground lead inductance and eliminate EMI noise that is not actually present in the circuit.



### **Design Assistance**

1. Master key : 2BDF0096E146A26C[v1]

2. LMR38020S Product Folder : http://www.ti.com/product/LMR38020 : contains the data sheet and other resources.

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